

Structural Calculations

Project Title: Kozitza Residence

Address: 09/01 Royal Scot Sub

Location: Donnelly, Idaho

Job #: 2023-4982



Prepared in accordance with 2018 IBC. Calculations expire by: *07/05/2024*

SITE SPECIFIC DESIGN CRITERIA:

Snow Criteria:

Roof Load (P_f)	150 psf	
Ground Load (P_g)	150 psf	
Exposure Factor (C_e)	1.0	Partially
Thermal Factor (C_t)	1.0	Typical
Importance (I_s)	1.0	

Wind Criteria:

Wind Speed (V_3)	115 mph	
Wind Exposure	C	Open Terrain
Wind Importance (I_w)	1.0	
Building Category	II	

Seismic Criteria:

Site Class	D	Stiff Soil
S_s	0.48	F_a 1.42
S_1	0.15	F_v 2.22
S_{D1}	0.45	S_{D1} 0.22
Risk Category	II	Other
Seismic Importance (I_E)	1.0	
Seismic Design Category (SDC)	D	

Seismic Criteria (continued):

Wall Material	Design Base Shear	Response Coeff., R	
OSB	.08Wp	6.5	Typ @ Ext
GYP	.27Wp	2	Typ @ Int
CANT COL	.36Wp	1.5	

Soil Criteria:

Brg. Strength	1500 psf
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STRUCTURE SPECIFIC DESIGN CRITERIA:

Live Loads:

Typ Residential	40 psf
Garage (P.V.)	50 psf
Sleeping Area's	30 psf

Roof Dead Loads:

Deck	1.5
Insulation	2.0
Roofing	3.0
Joist	2.5
Ceiling	3.0
Misc	4.5
TOTAL	17 psf

Exterior Wall Dead Loads:

Studs	2.0
Siding	2.5
Insulation	0.5
Gyp. Board	2.5
Sheathing	1.5
Misc	3.0
TOTAL	12 psf

Floor Dead Loads:

Deck	2.5
Joist	2.0
Ceiling	2.0
Flooring	2.5
Misc	3.0
TOTAL	12 psf

Interior Wall Dead Loads:

Studs	2.0
Gyp. Board	2.5
Misc	3.0
TOTAL	8 psf

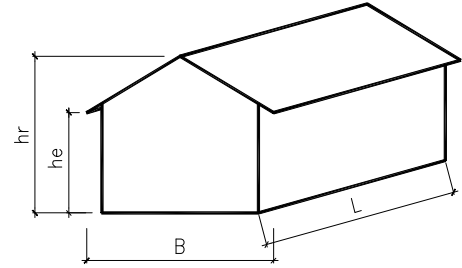
Deck Dead Load

Decking	4.4
Joist	2.0
	0.0
Misc	3.0
TOTAL	10 psf

WIND ANALYSIS: Low-rise Building - Based on IBC / ASCE 7

INPUT DATA

Exposure category (B, C or D, ASCE 7-16 26.7.3)		C			
Importance factor (ASCE 7-16 Table 1.5-2)	$I_w =$	1.00	for all Category		
Basic wind speed (ASCE 7-16 26.5.1 or 2018 IBC)	$V =$	115	mph		
Topographic factor (ASCE 7-16 26.8 & Table 26.8-1)	$K_{zt} =$	1.00	Flat		
Building height to ridge	$h_r =$	26.67	ft		
Building height to eave	$h_e =$	19.16	ft		
Building width	$B =$	40.00	ft		
Building length	$L =$	81.00	ft		
Overhang sloped width	$O_h =$	3.00	ft		
Effective area of components (or Solar Panel area)	$A =$	27.0	ft ² , <== Overhang? (Yes or No):	Yes	
Enclosed? (Y/N)		y			



ANALYSIS

Velocity pressure

$$q_h = 0.00256 K_z K_{zt} K_d K_e V^2 = 26.71 \text{ psf}$$

where: q_h = velocity pressure at mean roof height, h. (Eq. 26.10-1 page 268)

K_z = velocity pressure exposure coefficient evaluated at height, h, (Tab. 26.10-1, pg. 266) = **0.93**

K_d = wind directionality factor. (Tab. 26.6-1, for building, page 266) = **0.85**

h = mean roof height = **22.92 ft**

K_e = ground elevation factor. (**1.0** per Sec. 26.9, page 268)

< 60 ft, [Satisfactory] (ASCE 7-16 26.2.1)

< Min (L, B), [Satisfactory] (ASCE 7-16 26.2.2)

Design pressures for MWFRS

$$p = q_h [(G C_{pf}) - (G C_{pi})]$$

where: p = pressure in appropriate zone. (Eq. 28.3-1, page 311).

$p_{min} = 16 \text{ psf}$ (ASCE 7-16 28.3.4)

$G C_{pf}$ = product of gust effect factor and external pressure coefficient, see table below. (Fig. 28.3-1, page 312 & 313)

$G C_{pi}$ = product of gust effect factor and internal pressure coefficient. (Tab. 26.13-1, Enclosed Building, page 271)

= **0.18** or **-0.18**

a = width of edge strips, Fig 28.3-1, page 312, $\text{MAX}[\text{MIN}(0.1B, 0.1L, 0.4h), \text{MIN}(0.04B, 0.04L), 3] =$

4.00 ft

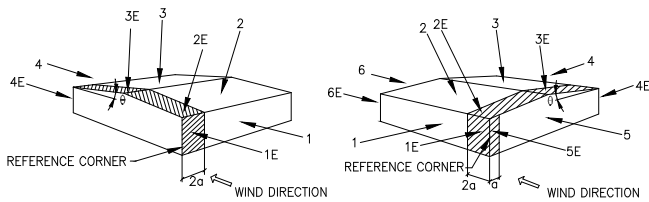
Net Pressures (psf), Basic Load Cases

Surface	Roof angle q = 18.43			Roof angle q = 18.43		
	$G C_{pf}$	Net Press. W/		$G C_{pf}$	Net Press. W/	
		(+ $G C_{pi}$)	(- $G C_{pi}$)		(+ $G C_{pi}$)	(- $G C_{pi}$)
1	0.52	8.99	18.60	-0.45	-16.83	-7.21
2	-0.69	-23.24	-13.62	-0.69	-23.24	-13.62
3	-0.47	-17.32	-7.71	-0.37	-14.69	-5.07
4	-0.42	-15.90	-6.29	-0.45	-16.83	-7.21
5				0.40	5.88	15.49
6				-0.29	-12.55	-2.94
1E	0.78	16.03	25.64	-0.48	-17.63	-8.01
2E	-1.07	-33.39	-23.77	-1.07	-33.39	-23.77
3E	-0.67	-22.79	-13.18	-0.53	-18.96	-9.35
4E	-0.62	-21.32	-11.70	-0.48	-17.63	-8.01
5E				0.61	11.48	21.10
6E				-0.43	-16.29	-6.68

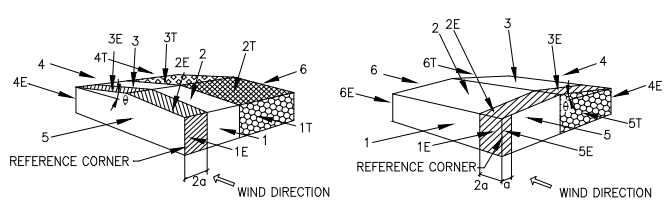
Net Pressures (psf), Torsional Load Cases

Surface	Roof angle q = 18.43		
	$G C_{pf}$	Net Press. W/	
		(+ $G C_{pi}$)	(- $G C_{pi}$)
1T	0.52	2.25	4.65
2T	-0.69	-5.81	-3.41
3T	-0.47	-4.33	-1.93
4T	0.00	-3.98	-1.57
Surface	Roof angle q = 0.00		
	$G C_{pf}$	Net Press. W/	
		(+ $G C_{pi}$)	(- $G C_{pi}$)
5T	0.40	1.47	3.87
6T	-0.29	-3.14	-0.73

+ / - Wind Pressure 64%



Load Case A (Transverse) Load Case B (Longitudinal)
Basic Load Cases



Load Case A (Transverse) Load Case B (Longitudinal)
Torsional Load Cases

Design pressures for components and cladding

$p = q_h [(G C_p) - (G C_{pi})]$

where: p = pressure on component. (Eq. 30.3-1, pg 33)

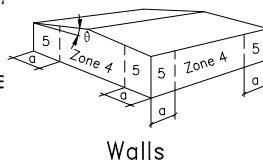
$p_{min} = 16.00$ psf (ASCE 7-16 30.2.2)

$G C_p = 1.00$ external pressure coefficient
see table below. (ASCE 7-16 30.3.2)

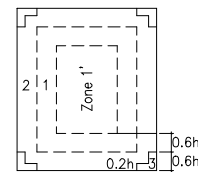
$q = 18.43$ °

$p_{overhang} = -92.14$ psf

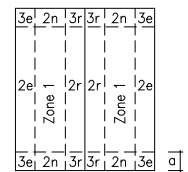
(ASCE 7-16 28.3.3)



Walls



Roof $\theta \leq 7^\circ$



Roof $\theta > 7^\circ$

Comp. & Cladding Coeffs.	Effective Area (ft ²)	Zone 1		Zone 1'		Zone 2		Zone 2e		Zone 2n		Zone 2r	
		GC _p	-GC _p	GC _p	-GC _p	GC _p	-GC _p	GC _p	-GC _p	GC _p	-GC _p	GC _p	-GC _p
	533	0.30	-0.80	0.30	-0.80	0.30	-2.20	0.30	-0.80	0.30	-1.00	0.30	-1.00
Effective Area (ft ²)	Zone 3		Zone 3e		Zone 3r		Zone 4		Zone 5				
	GC _p	-GC _p	GC _p	-GC _p	GC _p	-GC _p	GC _p	-GC _p	GC _p	-GC _p			
27	0.30	-2.50	0.30	-2.50	0.30	-1.80	0.99	-1.09	0.99	-1.38			

Comp. & Cladding Pressures	Zone 1		Zone 1'		Zone 2		Zone 2e		Zone 2n		Zone 2r	
	Positive	Negative	Positive	Negative	Positive	Negative	Positive	Negative	Positive	Negative	Positive	Negative
	3.20	-16.56	3.20	-16.56	3.20	-53.95	3.20	-16.56	3.20	-21.90	3.20	-21.90
	Zone 3		Zone 3e		Zone 3r		Zone 4		Zone 5		(Max Pressure 61.96 psf)	
Positive	Negative	Positive	Negative	Positive	Negative	Positive	Negative	Positive	Negative			
3.20	-61.96	3.20	-61.96	3.20	-43.27	21.62	-24.29	21.62	-32.03			

LOAD CASE 'A' FACTORED LOADS	
$0.6 * W_r = (Z_2 + Z_3) * 0.6 =$	3.5 psf
$0.6 * W_{rE} = (Z_{2E} + Z_{3E}) * 0.6 =$	6.4 psf
$0.6 * W_w = (Z_1 + Z_4) * 0.6 =$	14.9 psf
$0.6 * W_{wE} = (Z_{1E} + Z_{4E}) * 0.6 =$	22.4 psf

LOAD CASE 'B' FACTORED LOADS	
$0.6 * W_r = (Z_2 + Z_3) * 0.6 =$	5.1 psf
$0.6 * W_{rE} = (Z_{2E} + Z_{3E}) * 0.6 =$	8.7 psf
$0.6 * W_w = (Z_5 + Z_6) * 0.6 =$	11.1 psf
$0.6 * W_{wE} = (Z_{5E} + Z_{6E}) * 0.6 =$	16.7 psf

ROOF COMPONENTS FACTORED LOAD	
$0.6 * Z_{r,c\&c} =$	13.1 psf

WALL COMPONENTS FACTORED LOAD	
$0.6 * Z_{w,c\&c} =$	14.6 psf

OSB SEISMIC LOADING ANALYSIS

IBC / ASCE 7: Equivalent Lateral Force (ELF) Procedure:

INPUT DATA

Typical floor height: $h = 9$ ft
 Typical floor weight: $w_x = 55.1$ kips
 Number of floors: $n = 2$
 Importance factor (ASCE 11.5.1): $I_e = 1.00$
 Design spectral response: $S_{DS} = 0.45$ g
 $S_{D1} = 0.22$ g
 Mapped spectral resp.: $S_1 = 0.15$ g
 Period Parameter, C_t :
 (ASCE Tab 12.8-2): $C_t = 0.020$
 Resp. coefficient: (ASCE
 Tab. 12.2.1): $R = 6.5$
 Seismic design category: SDC = D
 $h_n = 26.7$ ft

DESIGN SUMMARY

$C_s = 1.2 * S_{DS} / (R / I_e) = 0.0833$ <= Applicable
 Period Parameter, $x = 0.75$, ASCE Tab 12.8-2
 Period: $T_a = C_t (h_n)^x = 0.23$ sec, ASCE 12.8.2.1
 $C_s < S_{D1} / [(R / I_e) T_a] = 0.1415$, ASCE Tab 12.8.1.1 <= Not Applicable
 $C_s > 0.044 S_{DS} I_e = 0.0199$, ASCE Tab 12.8.1.1 <= Not Applicable
 $C_s > 0.5 S_1 / (R / I_e) = 0.0112$, ASCE Tab 12.8.1.1 <= Not Applicable
 $k = 1.81$, (ASCE 12.8.3, page 91)
 $V = C_s W = 0.0833$ W
 $0.7 * V = 0.0583$ W
 $W = 110$ kips, total

SEISMIC COMPONENT & ANCHORING ANALYSIS

Out-of-plane seismic force for wall design (ASCE 7, Sec.12.11.1)

$$w_{1, seismic} = MAX(0.4 I S_{DS} W_p, 0.1 W_p) = 0.2 W_p = 0.2 \text{ psf} \quad \leq \text{USE FOR DIAPHRAGMS}$$

Where: $W_p = 1.0$ psf , $I_e = 1.00$
 (CBC / IBC Tab. 1604.5 & ASCE 7 Tab. 1.5-2)

Out-of-plane seismic force for anchorage design

For seismic design category A & B, any diaphragm (ASCE 7 Sec. 12.11.2)

$$F_{anch, seismic} = MAX \left[0.4 S_{DS} I W_p \frac{(h+h_p)^2}{2h}, 0.1 W_p \frac{(h+h_p)^2}{2h}, 400 S_{DS} I, F_{min} \right] =$$

Where: $F_{min} = 0.16$ plf, $1.69 W_p = 180$ plf (Horizontal) <= Not Applicable
 (ASCE 7 Sec. 12.11.2 & 11.7.3)

For seismic design category C and above, flexible diaphragm (ASCE 7 Sec. 12.11.2.1)

$$F_{anch, seismic} = MAX \left[0.8 S_{DS} I W_p \frac{(h+h_p)^2}{2h}, 0.1 W_p \frac{(h+h_p)^2}{2h}, 400 S_{DS} I, F_{min} \right] =$$

= **3.39** $W_p = 180$ plf (Horizontal) <= Applicable

For connections (ASCE 7 Sec. 12.11.2.1)

$$F_{conn, seismic} = MAX [0.133 S_{DS} w_p, 0.5 w_p] = 0.5 W_p = 0.5 \text{ plf (Horizontal)}$$

GYP SEISMIC LOADING ANALYSIS

IBC / ASCE 7: Equivalent Lateral Force (ELF) Procedure:

INPUT DATA

Typical floor height: $h = 9$ ft
 Typical floor weight: $w_x = 55.1$ kips
 Number of floors: $n = 2$
 Importance factor (ASCE 11.5.1): $I_e = 1.00$
 Design spectral response: $S_{DS} = 0.45$ g
 $S_{D1} = 0.22$ g
 Mapped spectral resp.: $S_1 = 0.15$ g
 Period Parameter, C_t :
 (ASCE Tab 12.8-2): $C_t = 0.020$
 Resp. coefficient: (ASCE
 Tab. 12.2.1): $R = 2$
 Seismic design category: SDC = D
 $h_n = 26.7$ ft

DESIGN SUMMARY

$C_s = 1.2 * S_{DS} / (R / I_e) = 0.2707$ <= Applicable
 Period Parameter, $x = 0.75$, ASCE Tab 12.8-2
 Period: $T_a = C_t (h_n)^x = 0.23$ sec, ASCE 12.8.2.1
 $C_s < S_{D1} / [(R / I_e) T_a] = 0.4599$, ASCE Tab 12.8.1.1 <= Not Applicable
 $C_s > 0.044 S_{DS} I_e = 0.0199$, ASCE Tab 12.8.1.1 <= Not Applicable
 $C_s > 0.5 S_1 / (R / I_e) = 0.0365$, ASCE Tab 12.8.1.1 <= Not Applicable
 $k = 1.81$, (ASCE 12.8.3, page 91)
 $V = C_s W = 0.2707$ W
 $0.7 * V = 0.1895$ W
 $W = 110$ kips, total

SEISMIC COMPONENT & ANCHORING ANALYSIS

Out-of-plane seismic force for wall design (ASCE 7, Sec.12.11.1)

$$w_{1, seismic} = MAX(0.4 I S_{DS} W_p, 0.1 W_p) = 0.2 W_p = 0.2 \text{ psf} \quad \leq \text{USE FOR DIAPHRAGMS}$$

Where: $W_p = 1.0$ psf, $I_e = 1.00$
 (CBC / IBC Tab. 1604.5 & ASCE 7 Tab. 1.5-2)

Out-of-plane seismic force for anchorage design

For seismic design category A & B, any diaphragm (ASCE 7 Sec. 12.11.2)

$$F_{anch, seismic} = MAX \left[0.4 S_{DS} I W_p \frac{(h+h_p)^2}{2h}, 0.1 W_p \frac{(h+h_p)^2}{2h}, 400 S_{DS} I, F_{min} \right] =$$

Where: $F_{min} = 0.16$ plf, $1.69 W_p = 180$ plf (Horizontal) <= Not Applicable
 (ASCE 7 Sec. 12.11.2 & 11.7.3)

For seismic design category C and above, flexible diaphragm (ASCE 7 Sec. 12.11.2.1)

$$F_{anch, seismic} = MAX \left[0.8 S_{DS} I W_p \frac{(h+h_p)^2}{2h}, 0.1 W_p \frac{(h+h_p)^2}{2h}, 400 S_{DS} I, F_{min} \right] =$$

= **3.39** $W_p = 180$ plf (Horizontal) <= Applicable

For connections (ASCE 7 Sec. 12.11.2.1)

$$F_{conn, seismic} = MAX [0.133 S_{DS} w_p, 0.5 w_p] = 0.5 W_p = 0.5 \text{ plf (Horizontal)}$$

WIND / SEISMIC SHEAR FORCE CALCULATIONS:

From ASCE 7-16 Wind & Seismic Loading Analysis

Wall Line	Roof / Floor						Wall					Load above		*C _s (W/p)	=	Loading		
	Wind Force (psf)	Diaph. Weight	Wr, We truss trib (ft)	Area W (ft)	Area L (ft)	Wind Force (psf)	Wall DL (psf)	Wall ht (ft)	wall line dist (ft)	Upr. Flr Wall ht (ft)	Wind (#)	Seismic (#)	Wind Force (kips)			Seismic Force (kips)	Lateral Control	
X1-1	9.6	55	17.7	40.0	78.0	16.4	12.0	9.0	40.0				0.06	=	4.87	5.21	Seismic	
X2-1	9.6	55	17.7	40.0	50.0	16.4	12.0	9.0	40.0				0.06	=	4.87	3.43	Wind	
X3-1	9.6	55	9.0	26.0	29.5	17.2	12.0	10.5	26.0				0.06	=	1.47	0.90	Wind	
Y1-1	9.6	55	17.7	51.5	40.0	16.1	12.0	9.0	51.5				0.06	=	6.23	3.60	Wind	
Y2-1	9.6	55	17.7	51.5	40.0	16.1	12.0	9.0	51.5				0.06	=	8.82	5.69	Wind	
	9.6	55	9.0	29.5	40.0	17.0	12.0	10.5	29.5				0.06	=				
Y3-1	9.6	55	9.0	29.5	40.0	17.0	12.0	10.5	29.5				0.06	=	2.59	2.09	Wind	

SHEAR WALL CALCULATIONS:

		X1-1	X1-1	X2-1	X3-1	Y1-1	Y2-1
Shear Wall Forces							
Total length of wall		60.00 ft	18.00 ft	50.00 ft	29.50 ft	11.00 ft	35.50 ft
Total length of shear wall	L =	60.00 ft	18.00 ft	50.00 ft	29.50 ft	11.00 ft	28.00 ft
Total length of full ht seg.	L _w =	31.50 ft	15.00 ft	24.58 ft	14.50 ft	3.50 ft	21.00 ft
height of shear wall	H =	9.00 ft	10.50 ft	9.00 ft	10.50 ft	9.00 ft	9.00 ft
Maximum opening height	H' =	9.00 ft	2.00 ft	8.00 ft	10.50 ft	8.00 ft	2.00 ft
Total force at top of wall	V ₁ =	3529 lbs	1681 lbs	4871 lbs	1469 lbs	3116 lbs	8821 lbs
Self weight	W _{DL self} =	108 plf	126 plf	108 plf	126 plf	108 plf	108 plf
Applied dead load	W _{DL above} =	40 plf	40 plf	40 plf	40 plf	40 plf	40 plf
Prefered OSB thickness	in	7/16	7/16	7/16	7/16	7/16	7/16
Prefered Gyp thickness	in	1/2	1/2	1/2	1/2	1/2	1/2
Wall Connected to Concrete	y/n =	Y	Y	Y	Y	Y	Y
Shear Wall Segments							
		2.75	7.50	3.50	3.00	1.75	4.75
		2.75	7.50	7.00	3.00	1.75	4.75
		13.00		10.83	5.00		11.50
		4.00		3.25	3.50		
		4.00					
		5.00					
Shear Transfer to Concrete							
	T =	Not Req'd	102 lbs	Not Req'd	Not Req'd	3500 lbs	2125 lbs
1/2 Anchor Bolts @		72 " O.C.	72 " O.C.	72 " O.C.	72 " O.C.		48 " O.C.
Provide:		Code Min.	Code Min.	Code Min.	Code Min.		A4
Min # of 1/2 Anchor Bolts		(4) Min	(2) Min	(5) Min	(2) Min		(9) Min
Load From Above		0.00	0.00	0.00	0.00	0.00	0.00
			Perp. Wall			HD3	HD1
Shear Resisting System							
Force Calculated		218.48	112.04	366.09	204.37	890.41	420.03
		OSB	OSB	OSB	OSB	B.F.	OSB
Min Shear Wall Segment:		2.57 ft	3.00 ft	2.57 ft	3.00 ft	1.33 ft	2.57 ft
Provide:	V _a =	SW1	SW1	SW2	SW1	4400	SW3
Min Shear Wall Segment:							
Provide:	V _a =						
Blocking / Nailing Framing Attachment							
Blocking Unit Shear		59 plf	93 plf	97 plf	50 plf	567 plf	248 plf
Blocking		NONE	NONE	NONE	NONE	B3	B1
Nailing		See SCHED	See SCHED	See SCHED	See SCHED	T3	T1
Unit Base Shear							
% of full height segments	%fh = L _w /L =	0.525	0.833	0.492	0.492	0.318	0.750
% of maximum opening height	%oh = H'/H =	1.000	0.190	0.889	1.000	0.889	0.222
Shear cap adj factor	SCAF =	0.51	1.00	0.54	0.50	0.47	1.00
Unit base shear	vbase V ₁ /L _w =	112 plf	112 plf	198 plf	101 plf	890 plf	420 plf
Effective unit base shear	vreq=v _{base} /SCAF =	218 plf	112 plf	366 plf	204 plf	1902 plf	420 plf
Ovrtrn. mo. Ttl. length of wall	OTM =	61.9 k-ft	17.6 k-ft	81.0 k-ft	31.1 k-ft	14.0 k-ft	79.4 k-ft
Shear wall adjustment factor							
Resist moment total L. of wall	RM =	266.0 k-ft	26.9 k-ft	184.7 k-ft	72.1 k-ft	0.2 k-ft	57.9 k-ft
	r =	0.5250	0.9633	0.5210	0.4915	0.3443	0.9310
	C _o =	0.5128	1.0769	0.5413	0.4958	0.4681	1.0909

SHEAR WALL CALCULATIONS:

Y3-1

Shear Wall Forces

Total length of wall		26.00 ft				
Total length of shear wall	L =	26.00 ft				
Total length of full ht seg.	L _w =	14.50 ft				
height of shear wall	H =	10.50 ft				
Maximum opening height	H' =	6.67 ft				
Total force at top of wall	V ₁ =	2588 lbs				
Self weight	w _{DL self} =	126 plf				
Applied dead load	w _{DL above} =	40 plf				
Prefered OSB thickness	in	7/16				
Prefered Gyp thickness	in	1/2				
Wall Connected to Concrete	y/n =	Y				

Shear Wall Segments

6.50
4.00
4.00

Shear Transfer to Concrete

T =		306 lbs				
1/2 Anchor Bolts @		72 " O.C.				
Provide:		Code Min.				
Min # of 1/2 Anchor Bolts		(3) Min				
Load From Above		0.00				
Holddown		Perp. Wall				

Shear Resisting System

Force Calculated		249.96				
		OSB				
Min Shear Wall Segment:		3.00 ft				
Provide:	V _a =	SW1				
Min Shear Wall Segment:						
Provide:	V _a =					

Blocking / Nailing Framing Attachment

Blocking Unit Shear		100 plf				
Blocking		NONE				
Nailing		See SCHED				

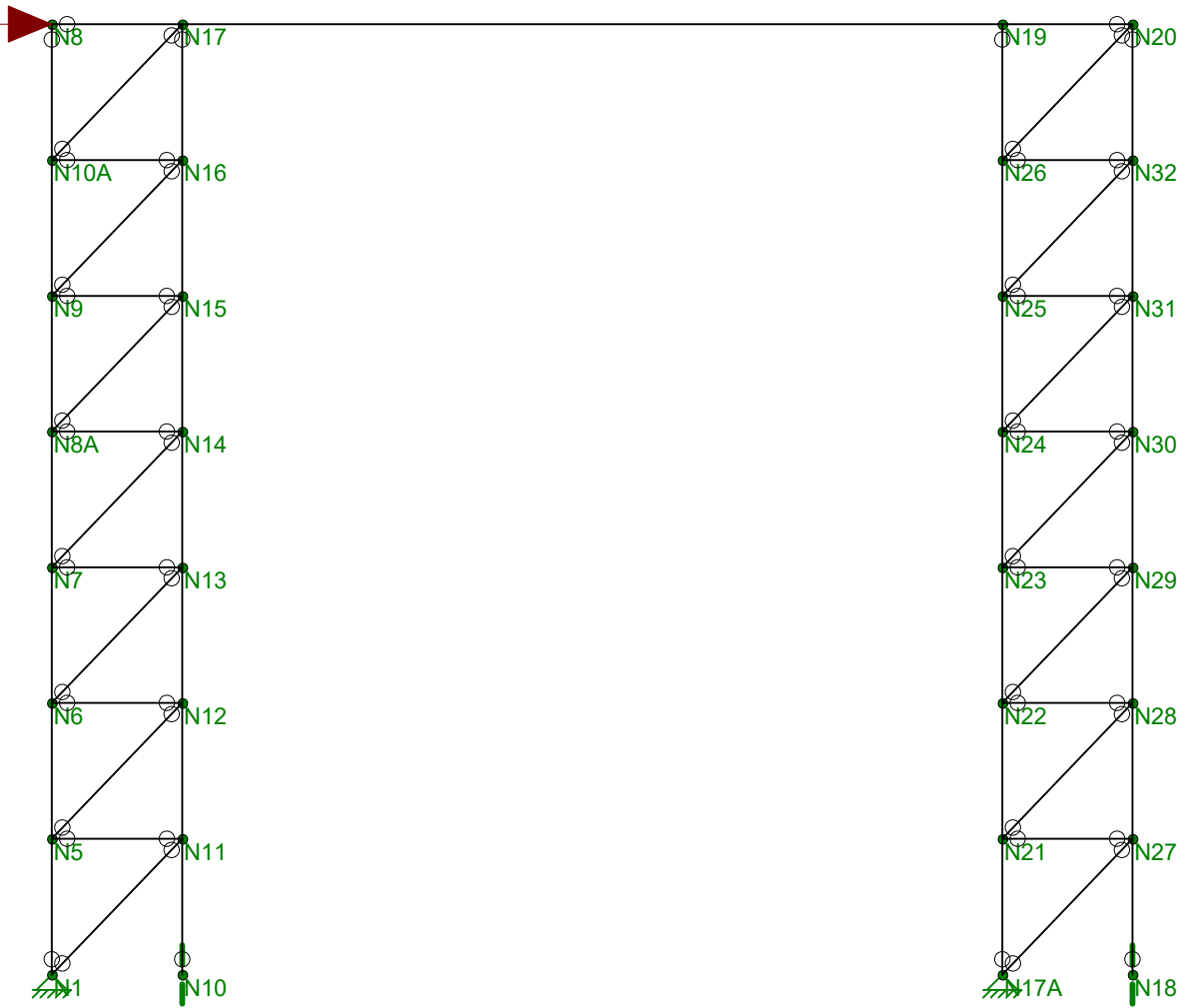
Unit Base Shear

% of full height segments	%fh = L _w /L =	0.558				
% of maximum opening height	%oh = H'/H =	0.635				
Shear cap adj factor	SCAF =	0.71				
Unit base shear	vbase V ₁ /L _w =	178 plf				
Effective unit base shear	vreq=v _{base} /SCAF =	250 plf				
Ovrtrn. mo. Ttl. length of wall	OTM =	38.1 k-ft				

Shear wall adjustment factor

Resist moment total L. of wall	RM =	56.0 k-ft				
	r =	0.6650				
	C ₀ =	0.7140				

4.4k



Loads: BLC 1, Wind Load
Envelope Only Solution

KccX'GYW]cb'GYlg

	Šca^	Ü@^	V^	Ö• a} / Šac	Tæ æ	Ö• a} Ä^	ÖZä Gá	Ö ÉÜ €	Ö ÉÜ €	Ö ÉÜ €
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>c]bh7ccfX]bUHyg'UbX'HYa dYfUi fYg

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F€	þF€	€	FG	€
FF	þFF	FÈG	G	€
FG	þFG	FÈG	I	€
FH	þFH	FÈG	Í	€
FI	þFI	FÈG	Ì	€
FÍ	þFÍ	FÈG	F€	€
FÎ	þFÎ	FÈG	FG	€
FÏ	þFÏ	FI	€	€
FÌ	þFÌ	FÍÈG	€	€
FJ	þFJ	FI	FI	€
F€	þF€	FÍÈG	FI	€
Fƒ	þFƒ	FI	G	€
GG	þGG	FI	I	€
GH	þGH	FI	Í	€
GI	þGI	FI	Ì	€
GÍ	þGÍ	FI	F€	€
GÎ	þGÎ	FI	FG	€
GÏ	þGÏ	FÍÈG	G	€
GÌ	þGÌ	FÍÈG	I	€
GJ	þGJ	FÍÈG	Í	€
G€	þG€	FÍÈG	Ì	€
Gƒ	þGƒ	FÍÈG	€	€
HF	þHF	FÍÈG	F€	€
HG	þHG	FÍÈG	FG	€

>c]bh6ci bXUf m7 cbX]h]cbg

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9bj YcdYAUIja i a 'A Ya Vyf'GWJcb': cfWg'f'cbh'bi YXL

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G	TFĪ	{ ae	FĪĪ H	€	FĪ	€	€	F	€	€	F
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GJ	TFĪ	{ ae	ĪĪĪ	€	FĪ	€	€	F	€	€	F
H€		{ a	ĪĪĪ Ī	€	FĪ	€	€	F	€	€	F
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9bj YcdYA UI ja i a 'A Ya Vyf'GYWjcb': cfWg'f' cbi YXL

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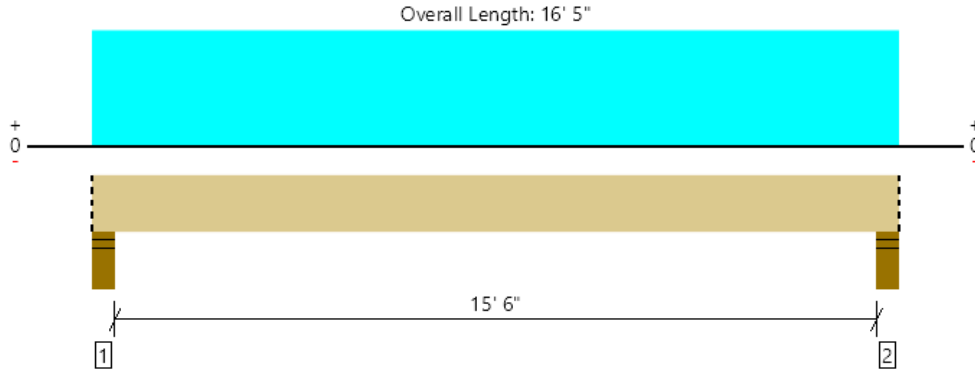
9bj YcdYA Ya Vyf'9bX'FYUWjcbg

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9bj YcdYA Ya Vyf 9bX'FYUW]cbg'f' c b h i YXL

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Roof Framing , RB1
1 piece(s) 6 3/4" x 18" 24F-V4 DF Glulam



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	18748 @ 4"	23203 (5.50")	Passed (81%)	--	1.0 D + 1.0 S (All Spans)
Shear (lbs)	14275 @ 1' 11 1/2"	24685	Passed (58%)	1.15	1.0 D + 1.0 S (All Spans)
Pos Moment (Ft-lbs)	70823 @ 8' 2 1/2"	80603	Passed (88%)	1.15	1.0 D + 1.0 S (All Spans)
Live Load Defl. (in)	0.475 @ 8' 2 1/2"	0.788	Passed (L/398)	--	1.0 D + 1.0 S (All Spans)
Total Load Defl. (in)	0.536 @ 8' 2 1/2"	1.050	Passed (L/353)	--	1.0 D + 1.0 S (All Spans)

System : Roof
Member Type : Drop Beam
Building Use : Residential
Building Code : IBC 2018
Design Methodology : ASD
Member Pitch : 0/12

- Deflection criteria: LL (L/240) and TL (L/180).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Critical positive moment adjusted by a volume factor of 0.96 that was calculated using length L = 15' 9".
- The effects of positive or negative camber have not been accounted for when calculating deflection.
- The specified glulam is assumed to have its strong laminations at the bottom of the beam. Install with proper side up as indicated by the manufacturer.
- Applicable calculations are based on NDS.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Snow	Factored	
1 - Stud wall - DF	5.50"	5.50"	4.44"	2126	16622	18748	Blocking
2 - Stud wall - DF	5.50"	5.50"	4.44"	2126	16622	18748	Blocking

• Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	16' 5" o/c	
Bottom Edge (Lu)	16' 5" o/c	

•Maximum allowable bracing intervals based on applied load.

Vertical Loads	Location (Side)	Tributary Width	Dead (0.90)	Snow (1.15)	Comments
0 - Self Weight (PLF)	0 to 16' 5"	N/A	29.5	--	
1 - Uniform (PSF)	0 to 16' 5" (Front)	13' 6"	17.0	150.0	Default Load

Weyerhaeuser Notes

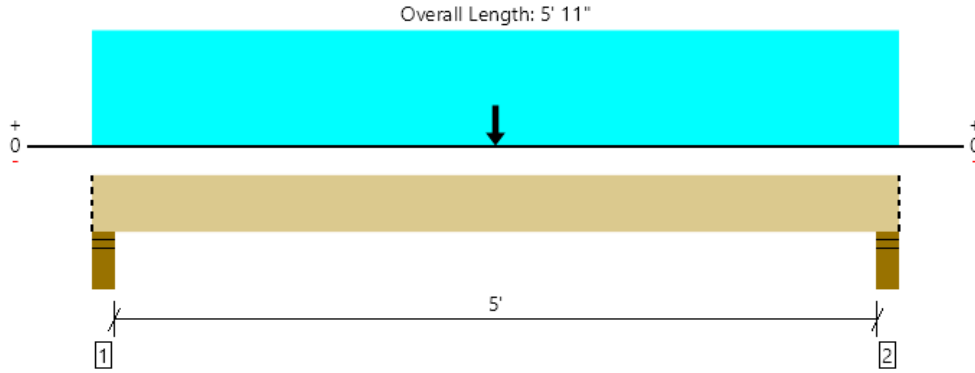
Weyerhaeuser warrants that the sizing of its products will be in accordance with Weyerhaeuser product design criteria and published design values. Weyerhaeuser expressly disclaims any other warranties related to the software. Use of this software is not intended to circumvent the need for a design professional as determined by the authority having jurisdiction. The designer of record, builder or framer is responsible to assure that this calculation is compatible with the overall project. Accessories (Rim Board, Blocking Panels and Squash Blocks) are not designed by this software. Products manufactured at Weyerhaeuser facilities are third-party certified to sustainable forestry standards. Weyerhaeuser Engineered Lumber Products have been evaluated by ICC-ES under evaluation reports ESR-1153 and ESR-1387 and/or tested in accordance with applicable ASTM standards. For current code evaluation reports, Weyerhaeuser product literature and installation details refer to www.eyerhaeuser.com/woodproducts/document-library.

The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

ForteWEB Software Operator	Job Notes
Trevor Steelsmith Snake River Engineering (208) 453-6512 trevor@snakeriverengineering.com	



Roof Framing , RB2
1 piece(s) 5 1/8" x 12" 24F-V4 DF Glulam



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	10653 @ 4"	17617 (5.50")	Passed (60%)	--	1.0 D + 1.0 S (All Spans)
Shear (lbs)	10023 @ 1' 5 1/2"	12495	Passed (80%)	1.15	1.0 D + 1.0 S (All Spans)
Pos Moment (Ft-lbs)	26097 @ 2' 11 1/2"	28290	Passed (92%)	1.15	1.0 D + 1.0 S (All Spans)
Live Load Defl. (in)	0.070 @ 2' 11 1/2"	0.262	Passed (L/900)	--	1.0 D + 1.0 S (All Spans)
Total Load Defl. (in)	0.079 @ 2' 11 1/2"	0.350	Passed (L/797)	--	1.0 D + 1.0 S (All Spans)

System : Roof
Member Type : Drop Beam
Building Use : Residential
Building Code : IBC 2018
Design Methodology : ASD
Member Pitch : 0/12

- Deflection criteria: LL (L/240) and TL (L/180).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Critical positive moment adjusted by a volume factor of 1.00 that was calculated using length L = 5' 3".
- The effects of positive or negative camber have not been accounted for when calculating deflection.
- The specified glulam is assumed to have its strong laminations at the bottom of the beam. Install with proper side up as indicated by the manufacturer.
- Applicable calculations are based on NDS.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Snow	Factored	
1 - Stud wall - DF	5.50"	5.50"	3.33"	1233	9420	10653	Blocking
2 - Stud wall - DF	5.50"	5.50"	3.33"	1233	9420	10653	Blocking

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	5' 11" o/c	
Bottom Edge (Lu)	5' 11" o/c	

- Maximum allowable bracing intervals based on applied load.

Vertical Loads	Location (Side)	Tributary Width	Dead (0.90)	Snow (1.15)	Comments
0 - Self Weight (PLF)	0 to 5' 11"	N/A	14.9	--	
1 - Uniform (PSF)	0 to 5' 11" (Front)	2' 6"	17.0	150.0	Default Load
2 - Point (lb)	2' 11 1/2" (Front)	N/A	2126	16622	Linked from: RB1, Support 1

Weyerhaeuser Notes

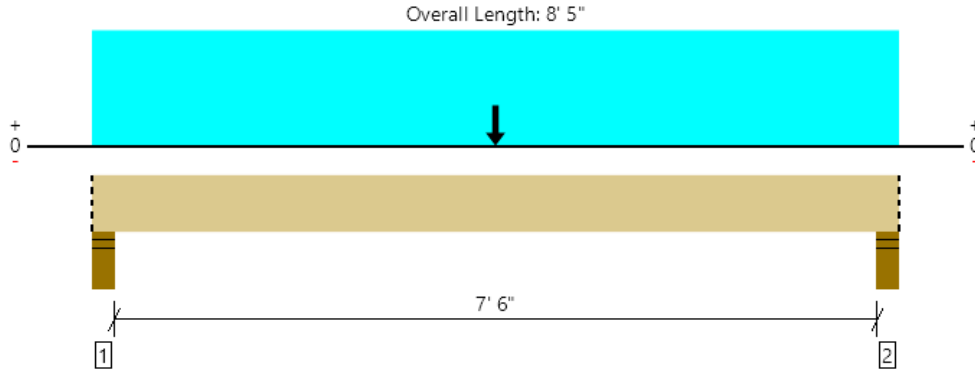
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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

ForteWEB Software Operator	Job Notes
Trevor Steelsmith Snake River Engineering (208) 453-6512 trevor@snakeriverengineering.com	



Roof Framing , RB3
1 piece(s) 5 1/8" x 15" 24F-V4 DF Glulam



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	11210 @ 4"	17617 (5.50")	Passed (64%)	--	1.0 D + 1.0 S (All Spans)
Shear (lbs)	10464 @ 1' 8 1/2"	15618	Passed (67%)	1.15	1.0 D + 1.0 S (All Spans)
Pos Moment (Ft-lbs)	39599 @ 4' 2 1/2"	44203	Passed (90%)	1.15	1.0 D + 1.0 S (All Spans)
Live Load Defl. (in)	0.119 @ 4' 2 1/2"	0.387	Passed (L/781)	--	1.0 D + 1.0 S (All Spans)
Total Load Defl. (in)	0.135 @ 4' 2 1/2"	0.517	Passed (L/690)	--	1.0 D + 1.0 S (All Spans)

System : Roof
Member Type : Drop Beam
Building Use : Residential
Building Code : IBC 2018
Design Methodology : ASD
Member Pitch : 0/12

- Deflection criteria: LL (L/240) and TL (L/180).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Critical positive moment adjusted by a volume factor of 1.00 that was calculated using length L = 7' 9".
- The effects of positive or negative camber have not been accounted for when calculating deflection.
- The specified glulam is assumed to have its strong laminations at the bottom of the beam. Install with proper side up as indicated by the manufacturer.
- Applicable calculations are based on NDS.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Snow	Factored	
1 - Stud wall - DF	5.50"	5.50"	3.50"	1320	9889	11210	Blocking
2 - Stud wall - DF	5.50"	5.50"	3.50"	1320	9889	11210	Blocking

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	8' 5" o/c	
Bottom Edge (Lu)	8' 5" o/c	

- Maximum allowable bracing intervals based on applied load.

Vertical Loads	Location (Side)	Tributary Width	Dead (0.90)	Snow (1.15)	Comments
0 - Self Weight (PLF)	0 to 8' 5"	N/A	18.7	--	
1 - Uniform (PSF)	0 to 8' 5" (Front)	2' 6"	17.0	150.0	Default Load
2 - Point (lb)	4' 2 1/2" (Front)	N/A	2126	16622	Linked from: RB1, Support 1

Weyerhaeuser Notes

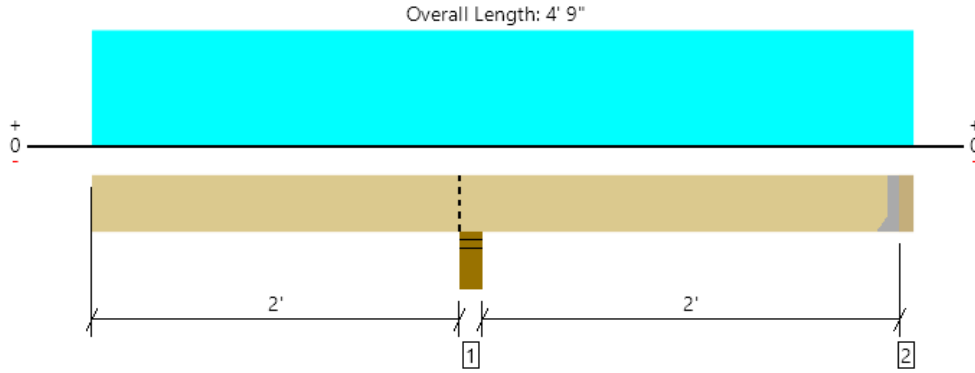
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ForteWEB Software Operator	Job Notes
Trevor Steelsmith Snake River Engineering (208) 453-6512 trevor@snakeriverengineering.com	



Roof Framing , Outlookers
1 piece(s) 2 x 6 DF No.2 @ 24" OC



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	1489 @ 2' 2 3/4"	5156 (5.50")	Passed (29%)	--	1.0 D + 1.0 S (All Spans)
Shear (lbs)	515 @ 1' 6 1/2"	1139	Passed (45%)	1.15	1.0 D + 1.0 S (All Spans)
Moment (Ft-lbs)	-830 @ 2' 2 3/4"	975	Passed (85%)	1.15	1.0 D + 1.0 S (All Spans)
Live Load Defl. (in)	0.104 @ 0	0.223	Passed (2L/514)	--	1.0 D + 1.0 S (Alt Spans)
Total Load Defl. (in)	0.115 @ 0	0.297	Passed (2L/464)	--	1.0 D + 1.0 S (Alt Spans)

System : Roof
Member Type : Joist
Building Use : Residential
Building Code : IBC 2018
Design Methodology : ASD
Member Pitch : 0/12

- Deflection criteria: LL (L/240) and TL (L/180).
- Overhang deflection criteria: LL (2L/240) and TL (2L/180).
- Left cantilever length exceeds 1/3 member length or 1/2 back span length. Additional bracing should be considered.
- Allowed moment does not reflect the adjustment for the beam stability factor.
- A 15% increase in the moment capacity has been added to account for repetitive member usage.
- Applicable calculations are based on NDS.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Snow	Factored	
1 - Stud wall - DF	5.50"	5.50"	1.59"	152	1338	1489	Blocking
2 - Hanger on 5 1/2" DF beam	3.50"	Hanger ¹	1.50"	10	255/-80	265/-70	See note ¹

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.
- At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger
- ¹ See Connector grid below for additional information and/or requirements.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	4' 6" o/c	
Bottom Edge (Lu)	4' 6" o/c	

- Maximum allowable bracing intervals based on applied load.

Connector: Simpson Strong-Tie							
Support	Model	Seat Length	Top Fasteners	Face Fasteners	Member Fasteners	Accessories	
2 - Face Mount Hanger	LU26	1.50"	N/A	6-10dx1.5	4-10dx1.5		

- Refer to manufacturer notes and instructions for proper installation and use of all connectors.

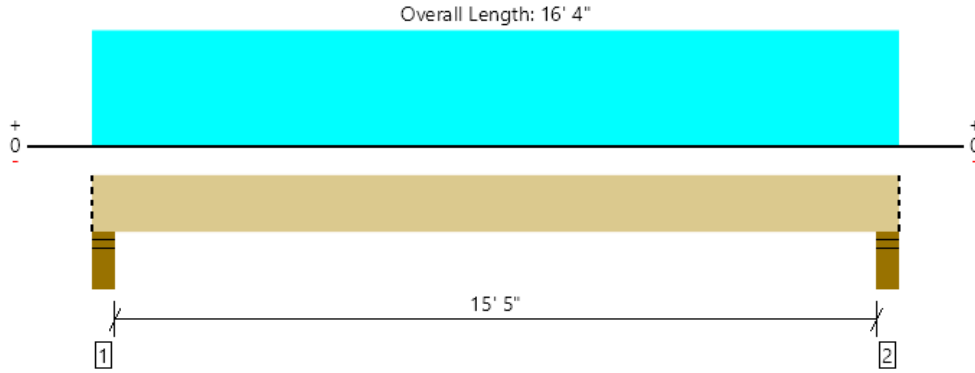
Vertical Load	Location (Side)	Spacing	Dead (0.90)	Snow (1.15)	Comments
1 - Uniform (PSF)	0 to 4' 9"	24"	17.0	150.0	Default Load

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ForteWEB Software Operator	Job Notes
Trevor Steelsmith Snake River Engineering (208) 453-6512 trevor@snakeriverengineering.com	



Roof Framing , Deck Beam Worst Case
1 piece(s) 6 3/4" x 13 1/2" 24F-V4 DF Glulam



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	9728 @ 4"	23203 (5.50")	Passed (42%)	--	1.0 D + 1.0 S (All Spans)
Shear (lbs)	7842 @ 1' 7"	18514	Passed (42%)	1.15	1.0 D + 1.0 S (All Spans)
Pos Moment (Ft-lbs)	36545 @ 8' 2"	46687	Passed (78%)	1.15	1.0 D + 1.0 S (All Spans)
Live Load Defl. (in)	0.571 @ 8' 2"	0.783	Passed (L/329)	--	1.0 D + 1.0 S (All Spans)
Total Load Defl. (in)	0.648 @ 8' 2"	1.044	Passed (L/290)	--	1.0 D + 1.0 S (All Spans)

System : Roof
Member Type : Drop Beam
Building Use : Residential
Building Code : IBC 2018
Design Methodology : ASD
Member Pitch : 0/12

- Deflection criteria: LL (L/240) and TL (L/180).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Critical positive moment adjusted by a volume factor of 0.99 that was calculated using length L = 15' 8".
- The effects of positive or negative camber have not been accounted for when calculating deflection.
- The specified glulam is assumed to have its strong laminations at the bottom of the beam. Install with proper side up as indicated by the manufacturer.
- Applicable calculations are based on NDS.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Snow	Factored	
1 - Stud wall - DF	5.50"	5.50"	2.31"	1153	8575	9728	Blocking
2 - Stud wall - DF	5.50"	5.50"	2.31"	1153	8575	9728	Blocking

• Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	16' 4" o/c	
Bottom Edge (Lu)	16' 4" o/c	

•Maximum allowable bracing intervals based on applied load.

Vertical Loads	Location (Side)	Tributary Width	Dead (0.90)	Snow (1.15)	Comments
0 - Self Weight (PLF)	0 to 16' 4"	N/A	22.1	--	
1 - Uniform (PSF)	0 to 16' 4" (Front)	7'	17.0	150.0	Default Load

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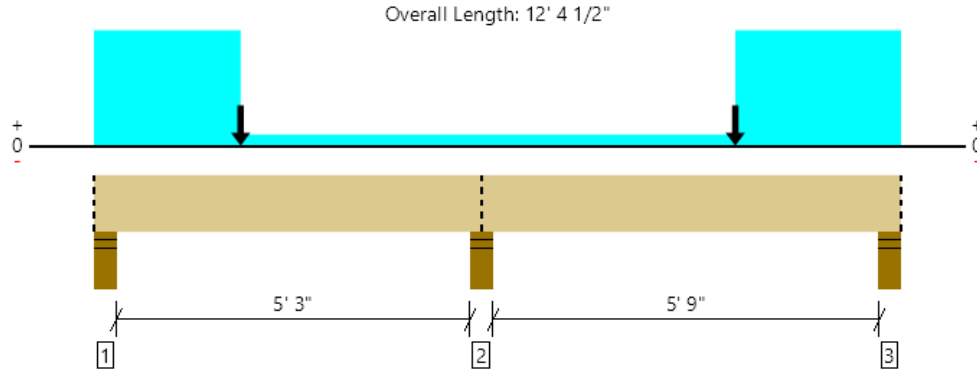
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ForteWEB Software Operator	Job Notes
Trevor Steelsmith Snake River Engineering (208) 453-6512 trevor@snakeriverengineering.com	



Floor Framing, FB3
2 piece(s) 1 3/4" x 11 7/8" 2.0E Microllam® LVL



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	12064 @ 5' 11 1/4"	12031 (5.50")	Passed (100%)	--	1.0 D + 1.0 S (All Spans)
Shear (lbs)	6192 @ 1' 5 3/8"	9081	Passed (68%)	1.15	1.0 D + 1.0 S (Alt Spans)
Moment (Ft-lbs)	13529 @ 9' 10"	20525	Passed (66%)	1.15	1.0 D + 1.0 S (Alt Spans)
Live Load Defl. (in)	0.089 @ 9' 10"	0.153	Passed (L/820)	--	1.0 D + 1.0 S (Alt Spans)
Total Load Defl. (in)	0.102 @ 9' 10"	0.305	Passed (L/722)	--	1.0 D + 1.0 S (Alt Spans)

System : Floor
Member Type : Drop Beam
Building Use : Residential
Building Code : IBC 2018
Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.

Supports	Bearing Length			Loads to Supports (lbs)				Accessories
	Total	Available	Required	Dead	Floor Live	Snow	Factored	
1 - Stud wall - DF	5.50"	5.50"	3.17"	912	112/-17	6024	6936	Blocking
2 - Stud wall - DF	5.50"	5.50"	5.51"	1638	293	10426	12064	Blocking
3 - Stud wall - DF	5.50"	5.50"	3.14"	938	120/-12	5927	6865	Blocking

• Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	10' o/c	
Bottom Edge (Lu)	12' 5" o/c	

•Maximum allowable bracing intervals based on applied load.

Vertical Loads	Location (Side)	Tributary Width	Dead (0.90)	Floor Live (1.00)	Snow (1.15)	Comments
0 - Self Weight (PLF)	0 to 12' 4 1/2"	N/A	12.1	--	--	
1 - Uniform (PSF)	0 to 2' 3" (Front)	2' 6"	17.0	-	150.0	Default Load
2 - Point (lb)	2' 3" (Front)	N/A	1320	-	9889	Linked from: RB3, Support 1
3 - Uniform (PSF)	0 to 12' 4 1/2" (Front)	1'	12.0	40.0	-	Default Load
4 - Uniform (PSF)	9' 10" to 12' 4 1/2" (Front)	2' 6"	17.0	-	150.0	Default Load
5 - Uniform (PSF)	0 to 2' 3" (Front)	9'	8.0	-	-	Default Load
6 - Uniform (PSF)	9' 10" to 12' 4 1/2" (Front)	9'	8.0	-	-	Default Load
7 - Point (lb)	9' 10" (Front)	N/A	1320	-	9889	Linked from: RB3, Support 1

Weyerhaeuser Notes

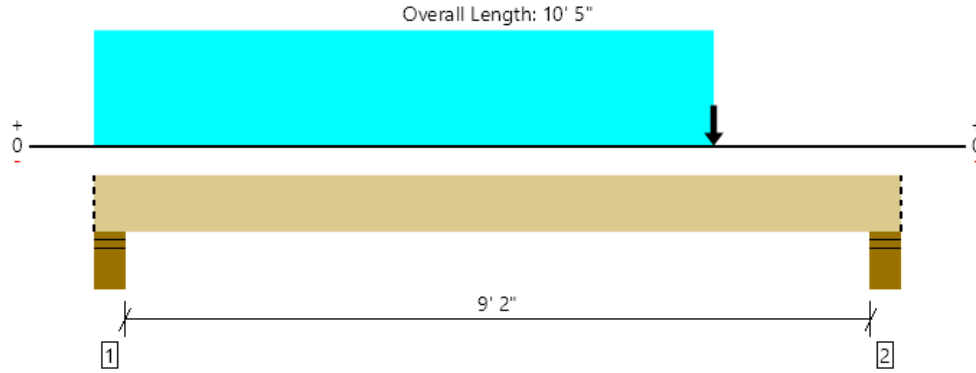
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ForteWEB Software Operator	Job Notes
Trevor Steelsmith Snake River Engineering (208) 453-6512 trevor@snakeriverengineering.com	



Floor Framing, FB4
1 piece(s) 8 3/4" x 18" 24F-V4 DF Glulam



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	27393 @ 9' 11"	41016 (7.50")	Passed (67%)	--	1.0 D + 1.0 S (All Spans)
Shear (lbs)	27311 @ 8' 3 1/2"	31999	Passed (85%)	1.15	1.0 D + 1.0 S (All Spans)
Pos Moment (Ft-lbs)	52396 @ 8'	107182	Passed (49%)	1.15	1.0 D + 1.0 S (All Spans)
Live Load Defl. (in)	0.073 @ 5' 8 7/16"	0.235	Passed (L/999+)	--	1.0 D + 1.0 S (All Spans)
Total Load Defl. (in)	0.086 @ 5' 8 3/16"	0.471	Passed (L/999+)	--	1.0 D + 1.0 S (All Spans)

System : Floor
Member Type : Drop Beam
Building Use : Residential
Building Code : IBC 2018
Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Critical positive moment adjusted by a volume factor of 0.99 that was calculated using length L = 9' 5".
- The effects of positive or negative camber have not been accounted for when calculating deflection.
- The specified glulam is assumed to have its strong laminations at the bottom of the beam. Install with proper side up as indicated by the manufacturer.
- Applicable calculations are based on NDS.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Snow	Factored	
1 - Stud wall - DF	7.50"	7.50"	1.72"	1755	7627	9382	Blocking
2 - Stud wall - DF	7.50"	7.50"	5.01"	3785	23607	27393	Blocking

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	10' 5" o/c	
Bottom Edge (Lu)	10' 5" o/c	

- Maximum allowable bracing intervals based on applied load.

Vertical Loads	Location (Side)	Tributary Width	Dead (0.90)	Snow (1.15)	Comments
0 - Self Weight (PLF)	0 to 10' 5"	N/A	38.3	--	
1 - Uniform (PSF)	0 to 8' (Front)	2' 6"	17.0	150.0	Default Load
2 - Uniform (PSF)	0 to 8' (Front)	9'	12.0	-	Default Load
3 - Point (lb)	8' (Front)	N/A	2163	14054	Linked from: FB6, Support 1
4 - Point (lb)	8' (Front)	N/A	1775	14180	Linked from: FB5, Support 2

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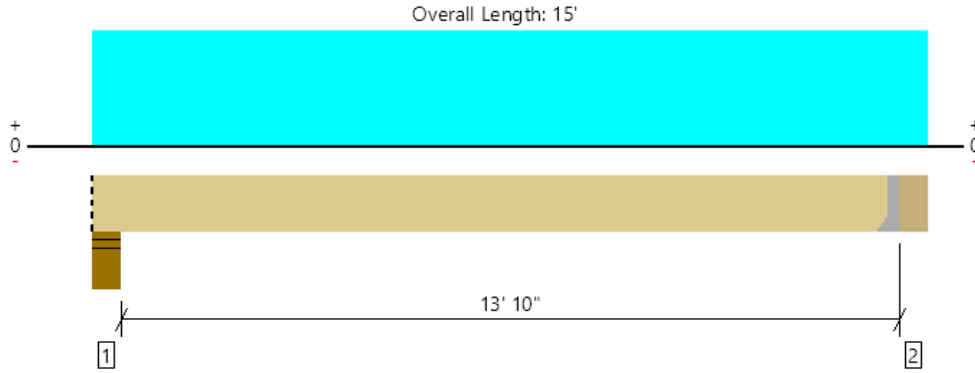
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ForteWEB Software Operator	Job Notes
Trevor Steelsmith Snake River Engineering (208) 453-6512 trevor@snakeriverengineering.com	



Floor Framing, FB5
1 piece(s) 5 1/2" x 18" 24F-V4 DF Glulam



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	14737 @ 14' 5"	14737 (4.12")	Passed (100%)	--	1.0 D + 1.0 S (All Spans)
Shear (lbs)	11570 @ 12' 11"	20114	Passed (58%)	1.15	1.0 D + 1.0 S (All Spans)
Pos Moment (Ft-lbs)	51426 @ 7' 5 1/4"	67850	Passed (76%)	1.15	1.0 D + 1.0 S (All Spans)
Live Load Defl. (in)	0.333 @ 7' 5 1/4"	0.349	Passed (L/503)	--	1.0 D + 1.0 S (All Spans)
Total Load Defl. (in)	0.375 @ 7' 5 1/4"	0.698	Passed (L/447)	--	1.0 D + 1.0 S (All Spans)

System : Floor
Member Type : Drop Beam
Building Use : Residential
Building Code : IBC 2018
Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Critical positive moment adjusted by a volume factor of 0.99 that was calculated using length L = 13' 11 1/2".
- The effects of positive or negative camber have not been accounted for when calculating deflection.
- The specified glulam is assumed to have its strong laminations at the bottom of the beam. Install with proper side up as indicated by the manufacturer.
- Applicable calculations are based on NDS.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Snow	Factored	
1 - Stud wall - DF	7.00"	7.00"	4.57"	1759	13945	15705	Blocking
2 - Hanger on 18" DF beam	7.00"	Hanger ¹	4.12"	1775	14180	15955	See note ¹

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.
- At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger
- ¹ See Connector grid below for additional information and/or requirements.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	14' 5" o/c	
Bottom Edge (Lu)	14' 5" o/c	

- Maximum allowable bracing intervals based on applied load.

Connector: Simpson Strong-Tie						
Support	Model	Seat Length	Top Fasteners	Face Fasteners	Member Fasteners	Accessories
2 - Face Mount Hanger	HHGU5.50-SDS H=18	5.25"	N/A	44-SDS25212	28-SDS25212	

- Refer to manufacturer notes and instructions for proper installation and use of all connectors.

Vertical Loads	Location (Side)	Tributary Width	Dead (0.90)	Snow (1.15)	Comments
0 - Self Weight (PLF)	0 to 14' 5"	N/A	24.1	--	
1 - Uniform (PSF)	0 to 15' (Front)	12' 6"	17.0	150.0	Default Load

Weyerhaeuser Notes

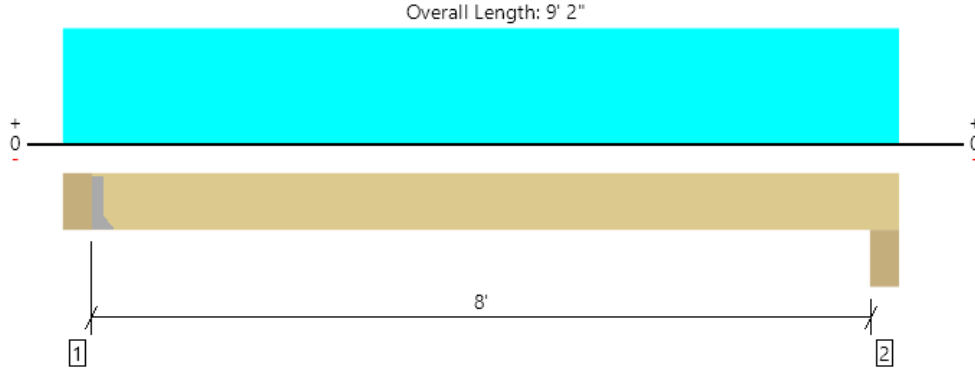
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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

ForteWEB Software Operator	Job Notes
Trevor Steelsmith Snake River Engineering (208) 453-6512 trevor@snakeriverengineering.com	



Floor Framing, FB6
1 piece(s) 5 1/8" x 13 1/2" 24F-V4 DF Glulam



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	14189 @ 7"	14189 (4.26")	Passed (100%)	--	1.0 D + 1.0 S (All Spans)
Shear (lbs)	10260 @ 1' 8 1/2"	14057	Passed (73%)	1.15	1.0 D + 1.0 S (All Spans)
Pos Moment (Ft-lbs)	28821 @ 4' 7 3/4"	35805	Passed (80%)	1.15	1.0 D + 1.0 S (All Spans)
Live Load Defl. (in)	0.157 @ 4' 7 3/4"	0.203	Passed (L/622)	--	1.0 D + 1.0 S (All Spans)
Total Load Defl. (in)	0.181 @ 4' 7 3/4"	0.406	Passed (L/538)	--	1.0 D + 1.0 S (All Spans)

System : Floor
Member Type : Drop Beam
Building Use : Residential
Building Code : IBC 2018
Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Critical positive moment adjusted by a volume factor of 1.00 that was calculated using length L = 8' 1 1/2".
- The effects of positive or negative camber have not been accounted for when calculating deflection.
- The specified glulam is assumed to have its strong laminations at the bottom of the beam. Install with proper side up as indicated by the manufacturer.
- Applicable calculations are based on NDS.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Snow	Factored	
1 - Hanger on 13 1/2" DF beam	7.00"	Hanger ¹	4.26"	2163	14054	16216	See note ¹
2 - Beam - DF	7.00"	7.00"	4.93"	2114	13676	15790	None

- At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger
- ¹ See Connector grid below for additional information and/or requirements.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	8' 7" o/c	
Bottom Edge (Lu)	8' 7" o/c	

- Maximum allowable bracing intervals based on applied load.

Connector: Simpson Strong-Tie						
Support	Model	Seat Length	Top Fasteners	Face Fasteners	Member Fasteners	Accessories
1 - Face Mount Hanger	HHGU5.25-SDS H=13.5	5.25"	N/A	44-SDS25212	28-SDS25212	

- Refer to manufacturer notes and instructions for proper installation and use of all connectors.

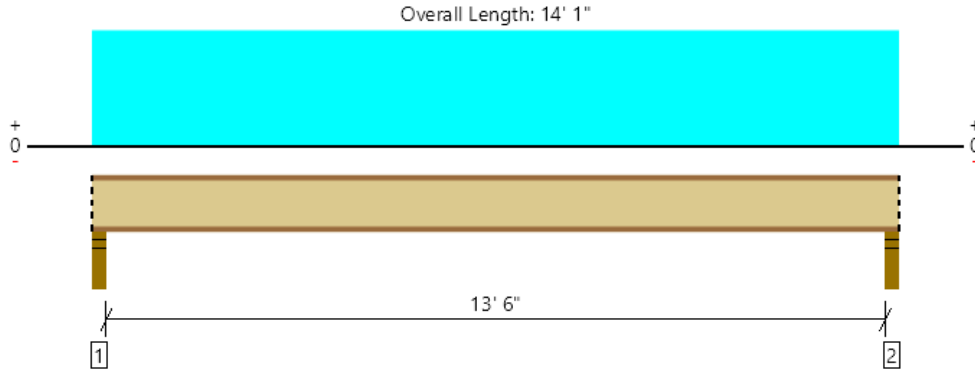
Vertical Loads	Location (Side)	Tributary Width	Dead (0.90)	Snow (1.15)	Comments
0 - Self Weight (PLF)	7" to 9' 2"	N/A	16.8	--	
1 - Uniform (PSF)	0 to 9' 2" (Front)	20' 2"	17.0	150.0	Default Load
2 - Uniform (PSF)	0 to 9' 2" (Front)	9'	12.0	-	Default Load

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ForteWEB Software Operator	Job Notes
Trevor Steelsmith Snake River Engineering (208) 453-6512 trevor@snakeriverengineering.com	



Floor Framing, Upper Floor Joists
1 piece(s) 11 7/8" TJI @ 110 @ 24" OC



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	732 @ 2 1/2"	1375 (3.50")	Passed (53%)	1.00	1.0 D + 1.0 L (All Spans)
Shear (lbs)	702 @ 3 1/2"	1560	Passed (45%)	1.00	1.0 D + 1.0 L (All Spans)
Moment (Ft-lbs)	2428 @ 7' 1/2"	3160	Passed (77%)	1.00	1.0 D + 1.0 L (All Spans)
Live Load Defl. (in)	0.211 @ 7' 1/2"	0.342	Passed (L/779)	--	1.0 D + 1.0 L (All Spans)
Total Load Defl. (in)	0.274 @ 7' 1/2"	0.683	Passed (L/599)	--	1.0 D + 1.0 L (All Spans)
TJ-Pro™ Rating	43	40	Passed	--	--

System : Floor
Member Type : Joist
Building Use : Residential
Building Code : IBC 2018
Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- A structural analysis of the deck has not been performed.
- Deflection analysis is based on composite action with a single layer of 23/32" Weyerhaeuser Edge™ Panel (24" Span Rating) that is glued and nailed down.
- Additional considerations for the TJ-Pro™ Rating include: None.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Floor Live	Factored	
1 - Stud wall - DF	3.50"	3.50"	1.75"	169	563	732	Blocking
2 - Stud wall - DF	3.50"	3.50"	1.75"	169	563	732	Blocking

• Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	3' 7" o/c	
Bottom Edge (Lu)	14' 1" o/c	

- TJI joists are only analyzed using Maximum Allowable bracing solutions.
- Maximum allowable bracing intervals based on applied load.

Vertical Load	Location	Spacing	Dead (0.90)	Floor Live (1.00)	Comments
1 - Uniform (PSF)	0 to 14' 1"	24"	12.0	40.0	Default Load

Weyerhaeuser Notes

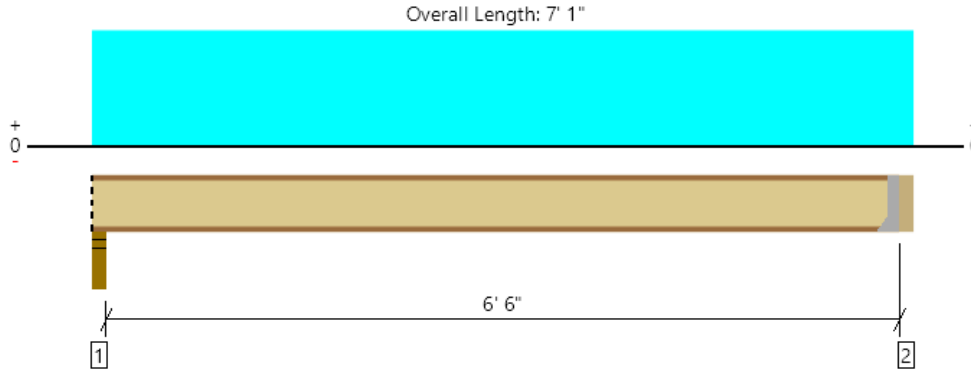
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ForteWEB Software Operator	Job Notes
Trevor Steelsmith Snake River Engineering (208) 453-6512 trevor@snakeriverengineering.com	



Floor Framing, Upper Floor Joists 2
1 piece(s) 11 7/8" TJI @ 110 @ 24" OC



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	342 @ 6' 9 1/2"	910 (1.75")	Passed (38%)	1.00	1.0 D + 1.0 L (All Spans)
Shear (lbs)	342 @ 6' 9 1/2"	1560	Passed (22%)	1.00	1.0 D + 1.0 L (All Spans)
Moment (Ft-lbs)	563 @ 3' 6"	3160	Passed (18%)	1.00	1.0 D + 1.0 L (All Spans)
Live Load Defl. (in)	0.017 @ 3' 6"	0.165	Passed (L/999+)	--	1.0 D + 1.0 L (All Spans)
Total Load Defl. (in)	0.023 @ 3' 6"	0.329	Passed (L/999+)	--	1.0 D + 1.0 L (All Spans)
TJ-Pro™ Rating	63	40	Passed	--	--

System : Floor
Member Type : Joist
Building Use : Residential
Building Code : IBC 2018
Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- A structural analysis of the deck has not been performed.
- Deflection analysis is based on composite action with a single layer of 23/32" Weyerhaeuser Edge™ Panel (24" Span Rating) that is glued and nailed down.
- Additional considerations for the TJ-Pro™ Rating include: None.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Floor Live	Factored	
1 - Stud wall - DF	3.50"	3.50"	1.75"	84	280	364	Blocking
2 - Hanger on 11 7/8" DF beam	3.50"	Hanger ¹	1.75" / - ²	86	287	373	See note ¹

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.
- At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger
- ¹ See Connector grid below for additional information and/or requirements.
- ² Required Bearing Length / Required Bearing Length with Web Stiffeners

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	6' 10" o/c	
Bottom Edge (Lu)	6' 10" o/c	

- TJI joists are only analyzed using Maximum Allowable bracing solutions.
- Maximum allowable bracing intervals based on applied load.

Connector: Simpson Strong-Tie

Support	Model	Seat Length	Top Fasteners	Face Fasteners	Member Fasteners	Accessories
2 - Face Mount Hanger	IUS1.81/11.88	2.00"	N/A	10-10dx1.5	2-Strong-Grip	

- Refer to manufacturer notes and instructions for proper installation and use of all connectors.

Vertical Load	Location	Spacing	Dead (0.90)	Floor Live (1.00)	Comments
1 - Uniform (PSF)	0 to 7' 1"	24"	12.0	40.0	Default Load

Weyerhaeuser Notes

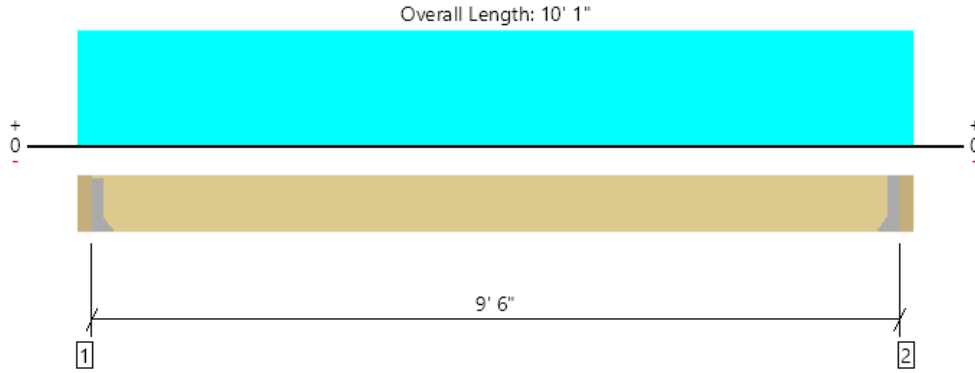
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ForteWEB Software Operator	Job Notes
Trevor Steelsmith Snake River Engineering (208) 453-6512 trevor@snakeriverengineering.com	



Floor Framing, Deck Floor Joists
1 piece(s) 2 x 10 DF No.2 @ 12" OC



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	770 @ 3' 1/2"	1406 (1.50")	Passed (55%)	--	1.0 D + 1.0 S (All Spans)
Shear (lbs)	645 @ 1' 3/4"	1915	Passed (34%)	1.15	1.0 D + 1.0 S (All Spans)
Moment (Ft-lbs)	1828 @ 5' 1/2"	2334	Passed (78%)	1.15	1.0 D + 1.0 S (All Spans)
Live Load Defl. (in)	0.174 @ 5' 1/2"	0.237	Passed (L/656)	--	1.0 D + 1.0 S (All Spans)
Total Load Defl. (in)	0.188 @ 5' 1/2"	0.475	Passed (L/608)	--	1.0 D + 1.0 S (All Spans)
TJ-Pro™ Rating	N/A	N/A	N/A	--	N/A

System : Floor
Member Type : Joist
Building Use : Residential
Building Code : IBC 2018
Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- A 15% increase in the moment capacity has been added to account for repetitive member usage.
- Applicable calculations are based on NDS.
- No composite action between deck and joist was considered in analysis.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Snow	Factored	
1 - Hanger on 9 1/4" DF beam	3.50"	Hanger ¹	1.50"	61	756	817	See note ¹
2 - Hanger on 9 1/4" DF beam	3.50"	Hanger ¹	1.50"	61	756	817	See note ¹

- At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger
- ¹ See Connector grid below for additional information and/or requirements.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	5' 9" o/c	
Bottom Edge (Lu)	9' 6" o/c	

- Maximum allowable bracing intervals based on applied load.

Connector: Simpson Strong-Tie							
Support	Model	Seat Length	Top Fasteners	Face Fasteners	Member Fasteners	Accessories	
1 - Face Mount Hanger	LU28	1.50"	N/A	8-10dx1.5	6-10dx1.5		
2 - Face Mount Hanger	LU28	1.50"	N/A	8-10dx1.5	6-10dx1.5		

- Refer to manufacturer notes and instructions for proper installation and use of all connectors.

Vertical Load	Location (Side)	Spacing	Dead (0.90)	Snow (1.15)	Comments
1 - Uniform (PSF)	0 to 10' 1"	12"	12.0	150.0	Default Load

Weyerhaeuser Notes

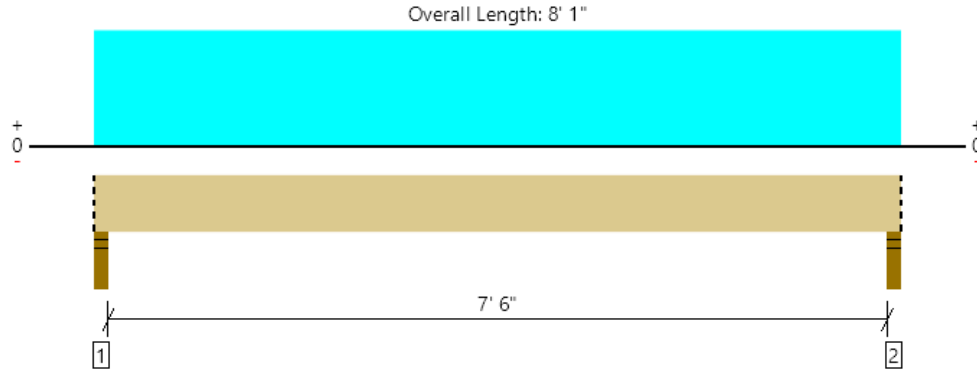
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ForteWEB Software Operator	Job Notes
Trevor Steelsmith Snake River Engineering (208) 453-6512 trevor@snakeriverengineering.com	



Floor Framing, Worst Case Deck Beam
1 piece(s) 6 x 10 DF No.2



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	3327 @ 2"	12031 (3.50")	Passed (28%)	--	1.0 D + 1.0 S (All Spans)
Shear (lbs)	2435 @ 1' 1"	6810	Passed (36%)	1.15	1.0 D + 1.0 S (All Spans)
Moment (Ft-lbs)	6181 @ 4' 1/2"	6937	Passed (89%)	1.15	1.0 D + 1.0 S (All Spans)
Live Load Defl. (in)	0.119 @ 4' 1/2"	0.194	Passed (L/780)	--	1.0 D + 1.0 S (All Spans)
Total Load Defl. (in)	0.131 @ 4' 1/2"	0.387	Passed (L/711)	--	1.0 D + 1.0 S (All Spans)

System : Floor
Member Type : Drop Beam
Building Use : Residential
Building Code : IBC 2018
Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Lumber grading provisions must be extended over the length of the member per NDS 4.2.5.5.
- Applicable calculations are based on NDS.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Snow	Factored	
1 - Stud wall - DF	3.50"	3.50"	1.50"	296	3031	3327	Blocking
2 - Stud wall - DF	3.50"	3.50"	1.50"	296	3031	3327	Blocking

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	8' 1" o/c	
Bottom Edge (Lu)	8' 1" o/c	

- Maximum allowable bracing intervals based on applied load.

Vertical Loads	Location (Side)	Tributary Width	Dead (0.90)	Snow (1.15)	Comments
0 - Self Weight (PLF)	0 to 8' 1"	N/A	13.2	--	
1 - Uniform (PSF)	0 to 8' 1" (Front)	5'	12.0	150.0	Default Load

Weyerhaeuser Notes

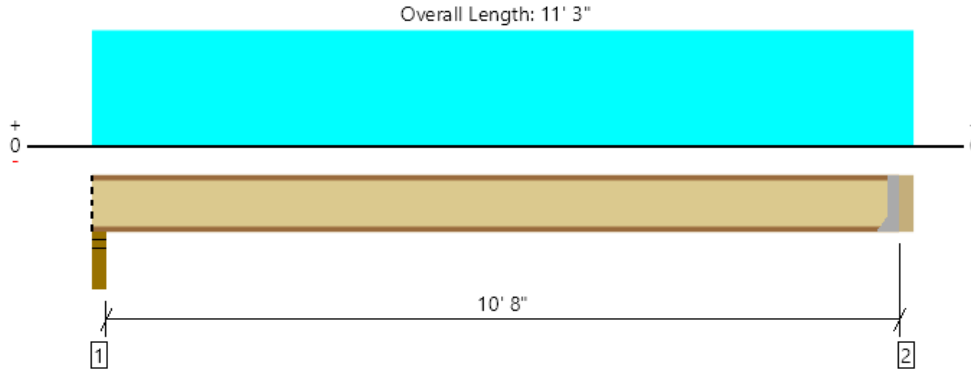
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ForteWEB Software Operator	Job Notes
Trevor Steelsmith Snake River Engineering (208) 453-6512 trevor@snakeriverengineering.com	



Floor Framing, Main Floor Framing
1 piece(s) 9 1/2" TJI® 110 @ 24" OC



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	559 @ 10' 11 1/2"	910 (1.75")	Passed (61%)	1.00	1.0 D + 1.0 L (All Spans)
Shear (lbs)	559 @ 10' 11 1/2"	1220	Passed (46%)	1.00	1.0 D + 1.0 L (All Spans)
Moment (Ft-lbs)	1502 @ 5' 7"	2500	Passed (60%)	1.00	1.0 D + 1.0 L (All Spans)
Live Load Defl. (in)	0.139 @ 5' 7"	0.269	Passed (L/930)	--	1.0 D + 1.0 L (All Spans)
Total Load Defl. (in)	0.180 @ 5' 7"	0.538	Passed (L/715)	--	1.0 D + 1.0 L (All Spans)
TJ-Pro™ Rating	41	40	Passed	--	--

System : Floor
Member Type : Joist
Building Use : Residential
Building Code : IBC 2018
Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- A structural analysis of the deck has not been performed.
- Deflection analysis is based on composite action with a single layer of 23/32" Weyerhaeuser Edge™ Panel (24" Span Rating) that is glued and nailed down.
- Additional considerations for the TJ-Pro™ Rating include: None.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Floor Live	Factored	
1 - Stud wall - DF	3.50"	3.50"	1.75"	134	447	581	Blocking
2 - Hanger on 9 1/2" DF beam	3.50"	Hanger ¹	1.75" / - ²	136	453	589	See note ¹

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.
- At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger
- ¹ See Connector grid below for additional information and/or requirements.
- ² Required Bearing Length / Required Bearing Length with Web Stiffeners

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	4' o/c	
Bottom Edge (Lu)	11' o/c	

- TJI joists are only analyzed using Maximum Allowable bracing solutions.
- Maximum allowable bracing intervals based on applied load.

Connector: Simpson Strong-Tie

Support	Model	Seat Length	Top Fasteners	Face Fasteners	Member Fasteners	Accessories
2 - Face Mount Hanger	IUS1.81/9.5	2.00"	N/A	8-10dx1.5	2-Strong-Grip	

- Refer to manufacturer notes and instructions for proper installation and use of all connectors.

Vertical Load	Location	Spacing	Dead (0.90)	Floor Live (1.00)	Comments
1 - Uniform (PSF)	0 to 11' 3"	24"	12.0	40.0	Default Load

Weyerhaeuser Notes

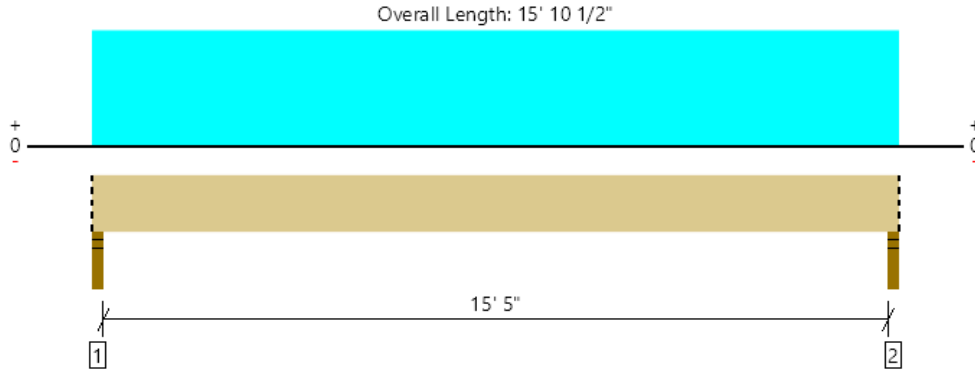
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Trevor Steelsmith Snake River Engineering (208) 453-6512 trevor@snakeriverengineering.com	



Deck Framing Update 7.5.2023, Roof: Drop Beam
 1 piece(s) 6 3/4" x 13 1/2" 24F-V4 DF Glulam



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	9455 @ 1' 1/4"	11602 (2.75")	Passed (81%)	--	1.0 D + 1.0 S (All Spans)
Shear (lbs)	7842 @ 7' 4 1/4"	18514	Passed (42%)	1.15	1.0 D + 1.0 S (All Spans)
Pos Moment (Ft-lbs)	36545 @ 7' 11 1/4"	46687	Passed (78%)	1.15	1.0 D + 1.0 S (All Spans)
Live Load Defl. (in)	0.571 @ 7' 11 1/4"	0.783	Passed (L/329)	--	1.0 D + 1.0 S (All Spans)
Total Load Defl. (in)	0.648 @ 7' 11 1/4"	1.044	Passed (L/290)	--	1.0 D + 1.0 S (All Spans)

System : Roof
 Member Type : Drop Beam
 Building Use : Residential
 Building Code : IBC 2018
 Design Methodology : ASD
 Member Pitch : 0/12

- Deflection criteria: LL (L/240) and TL (L/180).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Critical positive moment adjusted by a volume/size factor of 0.99 that was calculated using length L = 15' 8".
- The effects of positive or negative camber have not been accounted for when calculating deflection.
- The specified glulam is assumed to have its strong laminations at the bottom of the beam. Install with proper side up as indicated by the manufacturer.
- Applicable calculations are based on NDS.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Snow	Factored	
1 - Stud wall - DF	2.75"	2.75"	2.24"	1120	8334	9455	Blocking
2 - Stud wall - DF	2.75"	2.75"	2.24"	1120	8334	9455	Blocking

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	15' 11" o/c	
Bottom Edge (Lu)	15' 11" o/c	

- Maximum allowable bracing intervals based on applied load.

Vertical Loads	Location (Side)	Tributary Width	Dead (0.90)	Snow (1.15)	Comments
0 - Self Weight (PLF)	0 to 15' 10 1/2"	N/A	22.1	--	
1 - Uniform (PSF)	0 to 15' 10 1/2" (Front)	7'	17.0	150.0	Default Load

Weyerhaeuser Notes

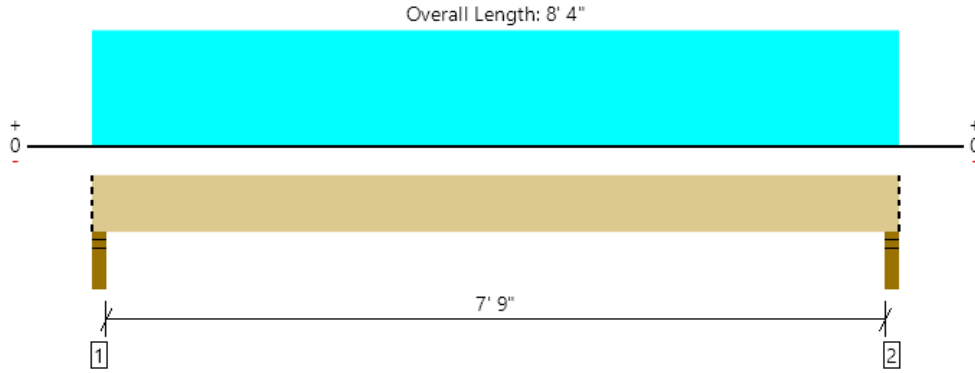
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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

ForteWEB Software Operator	Job Notes
Trevor Steelsmith 07/05/23 Snake River Engineering (208) 453-6512 trevor@snakeriverengineering.com	



Deck Framing Update 7.5.2023, floor beam
1 piece(s) 6 x 10 DF No.2



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	1868 @ 2"	12031 (3.50")	Passed (16%)	--	1.0 D + 1.0 S (All Spans)
Shear (lbs)	1382 @ 1' 1"	6810	Passed (20%)	1.15	1.0 D + 1.0 S (All Spans)
Moment (Ft-lbs)	3586 @ 4' 2"	6937	Passed (52%)	1.15	1.0 D + 1.0 S (All Spans)
Live Load Defl. (in)	0.068 @ 4' 2"	0.200	Passed (L/999+)	--	1.0 D + 1.0 S (All Spans)
Total Load Defl. (in)	0.081 @ 4' 2"	0.400	Passed (L/999+)	--	1.0 D + 1.0 S (All Spans)

System : Floor
Member Type : Drop Beam
Building Use : Residential
Building Code : IBC 2018
Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Lumber grading provisions must be extended over the length of the member per NDS 4.2.5.5.
- Applicable calculations are based on NDS.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Snow	Factored	
1 - Stud wall - DF	3.50"	3.50"	1.50"	305	1562	1868	Blocking
2 - Stud wall - DF	3.50"	3.50"	1.50"	305	1562	1868	Blocking

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	8' 4" o/c	
Bottom Edge (Lu)	8' 4" o/c	

- Maximum allowable bracing intervals based on applied load.

Vertical Loads	Location (Side)	Tributary Width	Dead (0.90)	Snow (1.15)	Comments
0 - Self Weight (PLF)	0 to 8' 4"	N/A	13.2	--	
1 - Uniform (PSF)	0 to 8' 4" (Front)	5'	12.0	75.0	Default Load

Weyerhaeuser Notes

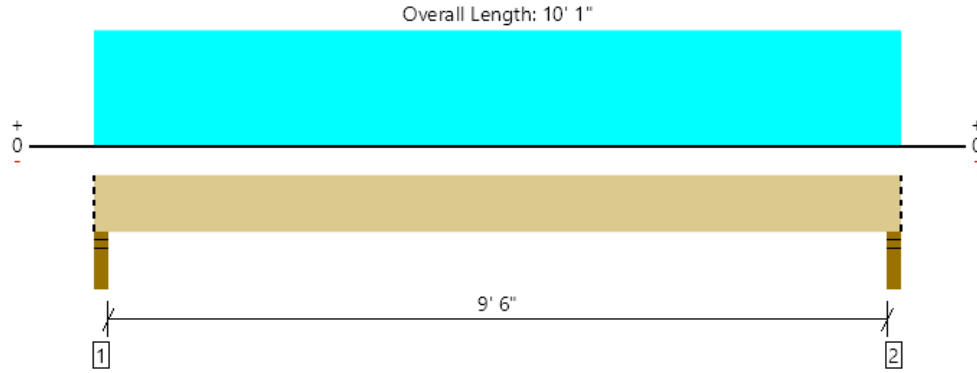
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ForteWEB Software Operator	Job Notes
Trevor Steelsmith Snake River Engineering (208) 453-6512 trevor@snakeriverengineering.com	



Deck Framing Update 7.5.2023, Copy of floor beam
1 piece(s) 4 x 10 DF No.2



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	919 @ 2"	7656 (3.50")	Passed (12%)	--	1.0 D + 1.0 S (All Spans)
Shear (lbs)	725 @ 1' 3/4"	4468	Passed (16%)	1.15	1.0 D + 1.0 S (All Spans)
Moment (Ft-lbs)	2165 @ 5' 1/2"	5166	Passed (42%)	1.15	1.0 D + 1.0 S (All Spans)
Live Load Defl. (in)	0.083 @ 5' 1/2"	0.244	Passed (L/999+)	--	1.0 D + 1.0 S (All Spans)
Total Load Defl. (in)	0.100 @ 5' 1/2"	0.488	Passed (L/999+)	--	1.0 D + 1.0 S (All Spans)

System : Floor
Member Type : Drop Beam
Building Use : Residential
Building Code : IBC 2018
Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Applicable calculations are based on NDS.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Snow	Factored	
1 - Stud wall - DF	3.50"	3.50"	1.50"	162	756	919	Blocking
2 - Stud wall - DF	3.50"	3.50"	1.50"	162	756	919	Blocking

• Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	10' 1" o/c	
Bottom Edge (Lu)	10' 1" o/c	

•Maximum allowable bracing intervals based on applied load.

Vertical Loads	Location (Side)	Tributary Width	Dead (0.90)	Snow (1.15)	Comments
0 - Self Weight (PLF)	0 to 10' 1"	N/A	8.2	--	
1 - Uniform (PSF)	0 to 10' 1" (Front)	2'	12.0	75.0	Default Load

Weyerhaeuser Notes

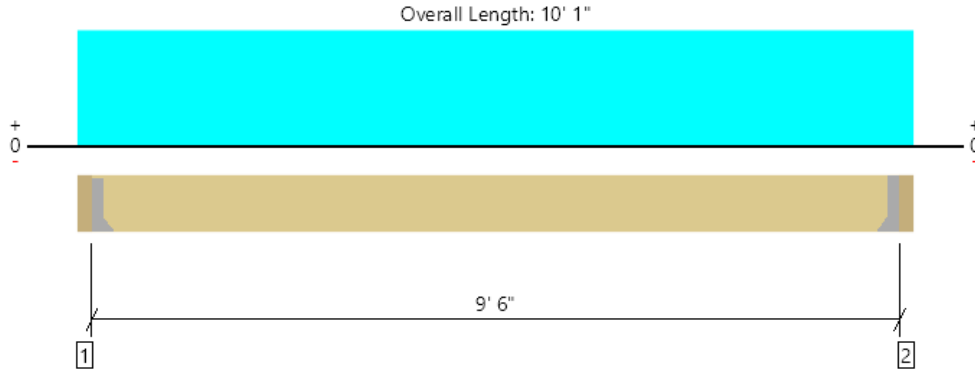
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ForteWEB Software Operator	Job Notes
Trevor Steelsmith Snake River Engineering (208) 453-6512 trevor@snakeriverengineering.com	



Deck Framing Update 7.5.2023, Floor: Joist
1 piece(s) 2 x 10 DF No.2 @ 12" OC



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	413 @ 3 1/2"	1406 (1.50")	Passed (29%)	--	1.0 D + 1.0 S (All Spans)
Shear (lbs)	346 @ 1' 3/4"	1915	Passed (18%)	1.15	1.0 D + 1.0 S (All Spans)
Moment (Ft-lbs)	981 @ 5' 1/2"	2334	Passed (42%)	1.15	1.0 D + 1.0 S (All Spans)
Live Load Defl. (in)	0.087 @ 5' 1/2"	0.237	Passed (L/999+)	--	1.0 D + 1.0 S (All Spans)
Total Load Defl. (in)	0.101 @ 5' 1/2"	0.475	Passed (L/999+)	--	1.0 D + 1.0 S (All Spans)
TJ-Pro™ Rating	N/A	N/A	N/A	--	N/A

System : Floor
Member Type : Joist
Building Use : Residential
Building Code : IBC 2018
Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- A 15% increase in the moment capacity has been added to account for repetitive member usage.
- Applicable calculations are based on NDS.
- No composite action between deck and joist was considered in analysis.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Snow	Factored	
1 - Hanger on 9 1/4" DF beam	3.50"	Hanger ¹	1.50"	61	378	439	See note ¹
2 - Hanger on 9 1/4" DF beam	3.50"	Hanger ¹	1.50"	61	378	439	See note ¹

- At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger
- ¹ See Connector grid below for additional information and/or requirements.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	9' 6" o/c	
Bottom Edge (Lu)	9' 6" o/c	

- Maximum allowable bracing intervals based on applied load.

Connector: Simpson Strong-Tie							
Support	Model	Seat Length	Top Fasteners	Face Fasteners	Member Fasteners	Accessories	
1 - Face Mount Hanger	LU28	1.50"	N/A	8-10dx1.5	6-10dx1.5		
2 - Face Mount Hanger	LU28	1.50"	N/A	8-10dx1.5	6-10dx1.5		

- Refer to manufacturer notes and instructions for proper installation and use of all connectors.

Vertical Load	Location (Side)	Spacing	Dead (0.90)	Snow (1.15)	Comments
1 - Uniform (PSF)	0 to 10' 1"	12"	12.0	75.0	Default Load

Weyerhaeuser Notes

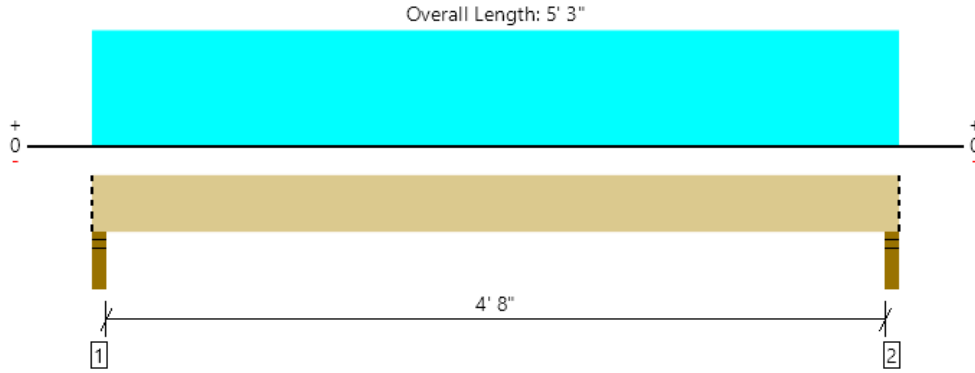
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ForteWEB Software Operator	Job Notes
Trevor Steelsmith Snake River Engineering (208) 453-6512 trevor@snakeriverengineering.com	



Deck Framing Update 7.5.2023, Copy of floor beam
1 piece(s) 6 x 8 DF No.2



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	1398 @ 2"	12031 (3.50")	Passed (12%)	--	1.0 D + 1.0 S (All Spans)
Shear (lbs)	910 @ 11"	5376	Passed (17%)	1.15	1.0 D + 1.0 S (All Spans)
Moment (Ft-lbs)	1609 @ 2' 7 1/2"	3706	Passed (43%)	1.15	1.0 D + 1.0 S (All Spans)
Live Load Defl. (in)	0.024 @ 2' 7 1/2"	0.123	Passed (L/999+)	--	1.0 D + 1.0 S (All Spans)
Total Load Defl. (in)	0.028 @ 2' 7 1/2"	0.246	Passed (L/999+)	--	1.0 D + 1.0 S (All Spans)

System : Floor
Member Type : Drop Beam
Building Use : Residential
Building Code : IBC 2018
Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Applicable calculations are based on NDS.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Snow	Factored	
1 - Stud wall - DF	3.50"	3.50"	1.50"	216	1181	1398	Blocking
2 - Stud wall - DF	3.50"	3.50"	1.50"	216	1181	1398	Blocking

• Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	5' 3" o/c	
Bottom Edge (Lu)	5' 3" o/c	

•Maximum allowable bracing intervals based on applied load.

Vertical Loads	Location (Side)	Tributary Width	Dead (0.90)	Snow (1.15)	Comments
0 - Self Weight (PLF)	0 to 5' 3"	N/A	10.4	--	
1 - Uniform (PSF)	0 to 5' 3" (Front)	6'	12.0	75.0	Default Load

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Trevor Steelsmith Snake River Engineering (208) 453-6512 trevor@snakeriverengineering.com	



WOOD HEADER ALLOWABLE LOADS (kips/ft)

Load Duration Factor: 1.15

LVL Grade: 2.0E

Top Chord Bracing: 2'-0" O.C.

Max TL Deflection: L/240, 0.75in

Repetitive Stress Increase: No

Header Type	Header Span										
	2'	3'	4'	5'	6'	8'	10'	12'	14'	16'	18'
(2) 2x4 DF Stud	1.15	0.69	0.29	0.22	0.12	NA	NA	NA	NA	NA	NA
(3) 2x4 DF Stud	1.84	1.04	0.46	0.35	0.18	NA	NA	NA	NA	NA	NA
(2) 2x6 DF #2	3.34	1.44	0.83	0.48	0.36	0.20	0.12	NA	NA	NA	NA
(3) 2x6 DF #2	5.06	2.19	1.27	0.72	0.55	0.30	0.18	0.13	NA	NA	NA
(2) 2x8 DF #2	5.41	2.30	1.27	0.80	0.59	0.32	0.20	0.14	0.09	NA	NA
(3) 2x8 DF #2	8.74	3.39	2.19	1.18	0.97	0.53	0.33	0.23	0.16	0.12	NA
(2) 2x10 DF #2	8.05	3.39	1.96	1.18	0.89	0.48	0.31	0.21	0.15	0.10	NA
(3) 2x10 DF #2	13.23	5.18	3.22	1.80	1.38	0.82	0.52	0.36	0.25	0.20	0.15
(2) 2x12 DF #2	10.81	4.83	2.65	1.60	1.15	0.67	0.41	0.29	0.21	0.15	0.12
(3) 2x12 DF #2	17.94	7.02	4.49	2.40	1.96	1.10	0.70	0.48	0.35	0.26	0.21
(2) 1-3/4x7-1/4 LVL	13.80	6.79	3.80	2.40	1.61	0.94	0.52	0.30	0.18	0.12	NA
(3) 1-3/4x7-1/4 LVL	20.70	10.47	5.64	3.50	2.53	1.38	0.79	0.45	0.28	0.17	NA
(2) 1-3/4x9-1/2 LVL	24.73	10.47	5.64	3.75	2.65	1.50	0.92	0.63	0.39	0.24	0.15
(3) 1-3/4x9-1/2 LVL	37.15	17.25	8.51	6.00	4.03	2.30	1.38	0.95	0.60	0.37	0.22
(2) 1-3/4x11-7/8 LVL	40.71	17.25	8.86	6.00	4.49	2.53	1.61	1.12	0.82	0.53	0.32
(3) 1-3/4x11-7/8 LVL	61.30	24.15	13.23	8.75	6.67	3.80	2.42	1.61	1.15	0.79	0.48
(2) 1-3/4x14 LVL	56.47	24.15	12.54	8.00	5.75	3.45	2.19	1.50	1.13	0.86	0.54
(3) 1-3/4x14 LVL	85.10	28.75	18.86	12.00	8.63	5.29	3.34	2.30	1.61	1.27	0.81

Beam Calculations

	Additional Drift	Roof	Floor	Deck	Wall	Total Load	Total Load
Trib	0.0	21	7	0	3.33		3,911.0 plf
Dead Load	-	357.0	84.0	0.0	40.0	481.0 plf	
Live / Snow Load	0	3150.0	280.0	0.0	-	3,430.0 plf	

Description:	3.0 ft Opening	9.5 ft Opening	2.3 ft Opening				
Header Callout	(2)9'-1/2" LVL 2.0E	5.25x18 DF/DF 24F - V4	(2)2x12 DF-L No. 2				
Trimmers	(2) 2x6 DF-L No. 2	(4) 2x6 DF-L No. 2	(2) 2x6 DF-L No. 2				
King Studs	(1) 2x6 DF-L No. 2	(1) 2x6 DF-L No. 2	(1) 2x6 DF-L No. 2				

Wood Design							
Species	LVL	DF/DF	DF-L				
Grade	2.0E	24F - V4	No. 2				
Width	3.50 in	5.25 in	3.00 in				
Depth	9.50 in	18.00 in	11.25 in				

Reaction							
Dead Load	721 lbs	2,285 lbs	541 lbs				
Live Load	5,145 lbs	16,293 lbs	3,859 lbs				

Load							
lu	3.0 ft	9.5 ft	2.3 ft				
le	6.2 ft	19.6 ft	4.6 ft				

Adjustment Factors							
Cd	1.15	1.15	1.15				
CF	1.1	1	1				

Material Properties							
Fb	2,900 psi	2,400 psi	900 psi				
Fv	285 psi	265 psi	180 psi				
E	2,000,000 psi	1,850,000 psi	1,600,000 psi				
Emin	1,016,535 psi	950,000 psi	580,000 psi				

Calculated Prop.							
A	33.25 in^2	94.50 in^2	33.75 in^2				
I	250.07 in^4	2,551.50 in^4	355.96 in^4				
S	52.65 in^3	283.50 in^3	63.28 in^3				
RB	7.58	12.38	8.34				
Emin'	1,016,535 psi	950,000 psi	580,000 psi				
FbE	21,210 psi	7,433 psi	10,011 psi				
Fb*	3,669 psi	2,760 psi	1,035 psi				
CL	1	1	1				

Shear and Moment							
M	52,798 lb-in	529,446 lb-in	29,699 lb-in				
V	5,866 lbs	18,577 lbs	4,400 lbs				

Stress							
fb	1,003 psi	1,868 psi	469 psi				
Fb'	3,631 psi	2,684 psi	1,029 psi				
fb/Fb'	0.28	0.70	0.46				
fv	265 psi	295 psi	196 psi				
Fv'	328 psi	305 psi	207 psi				
fv/Fv'	0.81	0.97	0.94				
Max Ratio	0.81	0.97	0.94				
	Pass	Pass	Pass				

Deflection							
ΔL	0.01 in	0.15 in	0.00 in				
	L/2,526	L/751	L/6,818				
ΔU	0.01 in	0.13 in	0.00 in				
	L/2,880	L/856	L/7,775				
	Pass	Pass	Pass				

Beam Calculations

	Additional Drift	Roof	Floor	Deck	Wall	Total Load	Total Load
Trib	0.0	7	0	0	3.33		1,209.0 plf
Dead Load	-	119.0	0.0	0.0	40.0	159.0 plf	
Live / Snow Load	0	1050.0	0.0	0.0	-	1,050.0 plf	

Description:	4.0 ft Opening	8.0 ft Opening	7.0 ft Opening				
Header Callout	(2)2x8 DF-L No. 2	(2)9-1/2" LVL 2.0E	(2)9-1/2" LVL 2.0E				
Trimmers	(1) 2x6 DF-L No. 2	(2) 2x6 DF-L No. 2	(2) 2x6 DF-L No. 2				
King Studs	(1) 2x6 DF-L No. 2	(1) 2x6 DF-L No. 2	(1) 2x6 DF-L No. 2				

Wood Design							
Species	DF-L	LVL	LVL				
Grade	No. 2	2.0E	2.0E				
Width	3.00 in	3.50 in	3.50 in				
Depth	7.25 in	9.50 in	9.50 in				

Reaction							
Dead Load	318 lbs	636 lbs	556 lbs				
Live Load	2,100 lbs	4,200 lbs	3,675 lbs				

Load							
lu	4.0 ft	8.0 ft	7.0 ft				
le	8.2 ft	15.4 ft	13.8 ft				

Adjustment Factors							
Cd	1.15	1.15	1.15				
CF	1.2	1.1	1.1				

Material Properties							
Fb	900 psi	2,900 psi	2,900 psi				
Fv	180 psi	285 psi	285 psi				
E	1,600,000 psi	2,000,000 psi	2,000,000 psi				
Emin	580,000 psi	1,016,535 psi	1,016,535 psi				

Calculated Prop.							
A	21.75 in^2	33.25 in^2	33.25 in^2				
I	95.27 in^4	250.07 in^4	250.07 in^4				
S	26.28 in^3	52.65 in^3	52.65 in^3				
RB	8.92	11.98	11.33				
Emin'	580,000 psi	1,016,535 psi	1,016,535 psi				
FbE	8,738 psi	8,503 psi	9,509 psi				
Fb*	1,242 psi	3,669 psi	3,669 psi				
CL	1	1	1				

Shear and Moment							
M	29,015 lb-in	116,060 lb-in	88,859 lb-in				
V	2,418 lbs	4,836 lbs	4,231 lbs				

Stress							
fb	1,104 psi	2,205 psi	1,688 psi				
Fb'	1,232 psi	3,542 psi	3,562 psi				
fb/Fb'	0.90	0.62	0.47				
fv	167 psi	218 psi	191 psi				
Fv'	207 psi	328 psi	328 psi				
fv/Fv'	0.81	0.67	0.58				
Max Ratio	0.90	0.67	0.58				
	Pass	Pass	Pass				

Deflection							
Δ _L	0.05 in	0.22 in	0.13 in				
	L/1,051	L/431	L/643				
Δ _{LL}	0.04 in	0.19 in	0.11 in				
	L/1,210	L/496	L/741				
	Pass	Pass	Pass				

Beam Calculations

	Additional Drift	Roof	Floor	Deck	Wall	Total Load	Total Load
Trib	0.0	7	0	0	3.33		
Dead Load	-	119.0	0.0	0.0	40.0	159.0 plf	1,209.0 plf
Live / Snow Load	0	1050.0	0.0	0.0	-	1,050.0 plf	

Description:	9.5 ft Opening						
---------------------	----------------	--	--	--	--	--	--

Header Callout	(2) 11-7/8" LVL 2.0E						
Trimmers	(2) 2x6 DF-L No. 2						
King Studs	(1) 2x6 DF-L No. 2						

Wood Design							
Species	LVL						
Grade	2.0E						
Width	3.50 in						
Depth	11.88 in						

Reaction							
Dead Load	755 lbs						
Live Load	4,988 lbs						

Load							
l _u	9.5 ft						
l _e	18.5 ft						

Adjustment Factors							
C _d	1.15						
C _F	1						

Material Properties							
F _b	2,900 psi						
F _v	285 psi						
E	2,000,000 psi						
E _{min}	1,016,535 psi						

Calculated Prop.							
A	41.56 in ²						
I	488.41 in ⁴						
S	82.26 in ³						
RB	14.65						
E _{min} '	1,016,535 psi						
F _{bE}	5,683 psi						
F _b *	3,335 psi						
C _L	1						

Shear and Moment							
M	163,663 lb-in						
V	5,743 lbs						

Stress							
f _b	1,990 psi						
F _b '	3,141 psi						
f _b /F _b '	0.63						
f _v	207 psi						
F _v '	328 psi						
f _v /F _v '	0.63						
Max Ratio	0.63						
	Pass						

Deflection							
Δ _{T_L}	0.23 in						
	L/503						
Δ _{L_L}	0.20 in						
	L/579						
	Pass						

Beam Calculations

	Additional Drift	Roof	Floor	Deck	Wall	Total Load	Total Load
Trib	0.0	15.5	0	0	3.33		2,628.5 plf
Dead Load	-	263.5	0.0	0.0	40.0	303.5 plf	
Live / Snow Load	0	2325.0	0.0	0.0	-	2,325.0 plf	

Description:	9.5 ft Opening						
Header Callout	5.25x13.5 DF/DF 24F - V4						
Trimmers	(3) 2x6 DF-L No. 2						
King Studs	(1) 2x6 DF-L No. 2						

Wood Design							
Species	DF/DF						
Grade	24F - V4						
Width	5.25 in						
Depth	13.50 in						

Reaction							
Dead Load	1,441 lbs						
Live Load	11,044 lbs						

Load							
l _u	9.5 ft						
l _e	18.9 ft						

Adjustment Factors							
C _d	1.15						
C _F	1						

Material Properties							
F _b	2,400 psi						
F _v	265 psi						
E	1,850,000 psi						
E _{min}	950,000 psi						

Calculated Prop.							
A	70.88 in ²						
I	1,076.41 in ⁴						
S	159.47 in ³						
RB	10.53						
E _{min} '	950,000 psi						
F _{bE}	10,284 psi						
F _b *	2,760 psi						
C _L	1						

Shear and Moment							
M	355,828 lb-in						
V	12,485 lbs						

Stress							
f _b	2,231 psi						
F _b '	2,711 psi						
f _b /F _b '	0.82						
f _v	264 psi						
F _v '	305 psi						
f _v /F _v '	0.87						
Max Ratio	0.87						
	Pass						

Deflection							
Δ _L	0.24 in						
	L/471						
Δ _{LL}	0.21 in						
	L/533						
	Pass						

Beam Calculations

	Additional Drift	Roof	Floor	Deck	Wall	Total Load	Total Load
Trib	0.0	12.165	0	0	3.33		2,071.5 plf
Dead Load	-	206.8	0.0	0.0	40.0	246.8 plf	
Live / Snow Load	0	1824.8	0.0	0.0	-	1,824.8 plf	

Description:	3.0 ft Opening						
Header Callout	(2)2x10 DF-L No. 2						
Trimmers	(2) 2x6 DF-L No. 2						
King Studs	(1) 2x6 DF-L No. 2						

Wood Design							
Species	DF-L						
Grade	No. 2						
Width	3.00 in						
Depth	9.25 in						

Reaction							
Dead Load	370 lbs						
Live Load	2,737 lbs						

Load							
l _u	3.0 ft						
l _e	6.2 ft						

Adjustment Factors							
C _d	1.15						
CF	1.1						

Material Properties							
F _b	900 psi						
F _v	180 psi						
E	1,600,000 psi						
E _{min}	580,000 psi						

Calculated Prop.							
A	27.75 in ²						
I	197.86 in ⁴						
S	42.78 in ³						
RB	8.73						
E _{min'}	580,000 psi						
F _{bE}	9,131 psi						
F _{b*}	1,139 psi						
CL	1						

Shear and Moment							
M	27,965 lb-in						
V	3,107 lbs						

Stress							
fb	654 psi						
Fb'	1,131 psi						
fb/Fb'	0.58						
fv	168 psi						
Fv'	207 psi						
fv/Fv'	0.81						
Max Ratio	0.81						
	Pass						

Deflection							
Δ _L	0.01 in						
	L/3,019						
Δ _{LL}	0.01 in						
	L/3,427						
	Pass						

Beam Calculations

	Additional Drift	Roof	Floor	Deck	Wall	Total Load	Total Load
Trib	0.0	11.5	0	0	3.33		1,960.5 plf
Dead Load	-	195.5	0.0	0.0	40.0	235.5 plf	
Live / Snow Load	0	1725.0	0.0	0.0	-	1,725.0 plf	

Description:	3.0 ft Opening						
Header Callout	(2)2x8 DF-L No. 2						
Trimmers	(2) 2x6 DF-L No. 2						
King Studs	(1) 2x6 DF-L No. 2						

Wood Design							
Species	DF-L						
Grade	No. 2						
Width	3.00 in						
Depth	7.25 in						

Reaction							
Dead Load	353 lbs						
Live Load	2,588 lbs						

Load							
lu	3.0 ft						
le	6.2 ft						

Adjustment Factors							
Cd	1.15						
CF	1.2						

Material Properties							
Fb	900 psi						
Fv	180 psi						
E	1,600,000 psi						
Emin	580,000 psi						

Calculated Prop.							
A	21.75 in^2						
I	95.27 in^4						
S	26.28 in^3						
RB	7.73						
Emin'	580,000 psi						
FbE	11,650 psi						
Fb*	1,242 psi						
CL	1						

Shear and Moment							
M	26,466 lb-in						
V	2,941 lbs						

Stress							
fb	1,007 psi						
Fb'	1,235 psi						
fb/Fb'	0.82						
fv	203 psi						
Fv'	207 psi						
fv/Fv'	0.98						
Max Ratio	0.98						
	Pass						

Deflection							
ΔTL	0.02 in						
	L/1,536						
ΔLL	0.02 in						
	L/1,746						
	Pass						

Beam Calculations

	Additional Drift	Roof	Floor	Deck	Wall	Total Load	Total Load
Trib	0.0	3	0	0	3.33		541.0 plf
Dead Load	-	51.0	0.0	0.0	40.0	91.0 plf	
Live / Snow Load	0	450.0	0.0	0.0	-	450.0 plf	

Description:	12.0 ft Opening	3.0 ft Opening					
Header Callout	(2)11-7/8" LVL 2.0E	(2)2x6 DF-L No. 2					
Trimmers	(1) 2x6 DF-L No. 2	(1) 2x6 DF-L No. 2					
King Studs	(2) 2x6 DF-L No. 2	(1) 2x6 DF-L No. 2					

Wood Design							
Species	LVL	DF-L					
Grade	2.0E	No. 2					
Width	3.50 in	3.00 in					
Depth	11.88 in	5.50 in					

Reaction							
Dead Load	546 lbs	136 lbs					
Live Load	2,700 lbs	675 lbs					

Load							
lu	12.0 ft	3.0 ft					
le	22.5 ft	6.2 ft					

Adjustment Factors							
Cd	1.15	1.15					
CF	1	1.3					

Material Properties							
Fb	2,900 psi	900 psi					
Fv	285 psi	180 psi					
E	2,000,000 psi	1,600,000 psi					
Emin	1,016,535 psi	580,000 psi					

Calculated Prop.							
A	41.56 in ²	16.50 in ²					
I	488.41 in ⁴	41.59 in ⁴					
S	82.26 in ³	15.13 in ³					
RB	16.19	6.73					
Emin'	1,016,535 psi	580,000 psi					
FbE	4,655 psi	15,357 psi					
Fb*	3,335 psi	1,346 psi					
CL	1	1					

Shear and Moment							
M	116,847 lb-in	7,303 lb-in					
V	3,246 lbs	811 lbs					

Stress							
fb	1,420 psi	483 psi					
Fb'	3,046 psi	1,339 psi					
fb/Fb'	0.47	0.36					
fv	117 psi	74 psi					
Fv'	328 psi	207 psi					
fv/Fv'	0.36	0.36					
Max Ratio	0.47	0.36					
	Pass	Pass					

Deflection							
Δ _L	0.26 in	0.01 in					
	L/557	L/2,430					
Δ _{LL}	0.21 in	0.01 in					
	L/670	L/2,921					
	Pass	Pass					

Beam Calculations

	Additional Drift	Roof	Floor	Deck	Wall	Total Load	Total Load
Trib	0.0	15.995	0	0	3.33		2,711.1 plf
Dead Load	-	271.9	0.0	0.0	40.0	311.9 plf	
Live / Snow Load	0	2399.3	0.0	0.0	-	2,399.3 plf	

Description:	3.0 ft Opening						
Header Callout	(3)2x8 DF-L No. 2						
Trimmers	(1) 2x6 DF-L No. 2						
King Studs	(1) 2x6 DF-L No. 2						

Wood Design							
Species	DF-L						
Grade	No. 2						
Width	4.50 in						
Depth	7.25 in						

Reaction							
Dead Load	468 lbs						
Live Load	3,599 lbs						

Load							
lu	3.0 ft						
le	6.2 ft						

Adjustment Factors							
Cd	1.15						
CF	1.2						

Material Properties							
Fb	900 psi						
Fv	180 psi						
E	1,600,000 psi						
Emin	580,000 psi						

Calculated Prop.							
A	32.63 in ²						
I	142.90 in ⁴						
S	39.42 in ³						
RB	5.15						
Emin'	580,000 psi						
FbE	26,214 psi						
Fb*	1,242 psi						
CL	1						

Shear and Moment							
M	36,600 lb-in						
V	4,067 lbs						

Stress							
fb	928 psi						
Fb'	1,239 psi						
fb/Fb'	0.75						
fv	187 psi						
Fv'	207 psi						
fv/Fv'	0.90						
Max Ratio	0.90						
	Pass						

Deflection							
ΔTL	0.02 in						
	L/1,666						
ΔLL	0.02 in						
	L/1,882						
	Pass						

WOOD TALL WALL & KING STUD ALLOWABLE LOADS (plf):

Load Duration Factor: 1.6
Max Vert. Load: 50 lbs

Max Deflection: $L/180$

King Stud	Height						
	12'	14'	16'	18'	20'	22'	24'
(1) 2x4 Stud	12.8	NA	NA	NA	NA	NA	NA
(2) 2x4 Stud	25.6	NA	NA	NA	NA	NA	NA
(3) 2x4 Stud	38.4	NA	NA	NA	NA	NA	NA
(1) 2x6 DF #2	57.0	35.8	24.1	16.9	NA	NA	NA
(2) 2x6 DF #2	114.0	71.6	48.2	33.8	NA	NA	NA
(3) 2x6 DF #2	171.0	107.4	72.3	50.7	NA	NA	NA
(1) 2x8 DF #2	130.0	81.7	55.0	38.7	28.2	21.2	16.3
(2) 2x8 DF #2	260.0	163.4	110.0	77.4	56.4	42.4	32.6
(3) 2x8 DF #2	390.0	245.1	165.0	116.1	84.6	63.6	48.9
(1) 2x6 LSL	67.8	42.7	28.5	20.0	14.7	NA	NA
(2) 2x6 LSL	135.6	85.4	57.0	40.0	29.4	NA	NA
(3) 2x6 LSL	203.4	128.1	85.5	60.0	44.1	NA	NA
(1) 2x8 LSL	155.0	98.3	65.5	46.0	33.5	25.2	19.5
(2) 2x8 LSL	310.0	196.6	131.0	92.0	67.0	50.4	39.0
(3) 2x8 LSL	465.0	294.9	196.5	138.0	100.5	75.6	58.5

*NOTE 1: this table combined with trimmer table to determine combined stress on each common wall stud.
*NOTE 2: allowable loads are interpolated at heights not in 2' increments.

WOOD TRIMMER ALLOWABLE LOADS (kips):

Load Duration Factor: 1.0
Eccentricity: 0"

Weak Axis Braced: Y

Trimmer Type	Height						
	8'	10'	12'	14'	16'	18'	20'
(1) 2x4 Stud	2.4	1.7	1.2	NA	NA	NA	NA
(2) 2x4 Stud	4.9	3.4	2.4	NA	NA	NA	NA
(3) 2x4 Stud	7.1	5.0	3.6	NA	NA	NA	NA
(1) 2x6 DF #2	5.1	5.1	5.0	3.8	3.0	NA	NA
(2) 2x6 DF #2	10.3	10.3	10.1	7.7	6.0	NA	NA
(3) 2x6 DF #2	15.4	15.4	15.1	11.6	9.1	NA	NA
(1) 2x8 DF #2	6.7	6.7	6.7	6.7	6.4	5.3	4.4
(2) 2x8 DF #2	13.5	13.5	13.5	13.5	12.9	10.6	8.8
(3) 2x8 DF #2	20.3	20.3	20.3	20.3	19.4	15.9	13.2

*NOTE 1: this table combined with king stud table to determine combined stress on each common wall stud.
*NOTE 2: allowable loads are interpolated at heights not in 2' increments.

TALL WALL CALCULATIONS:

This spreadsheet is used for designing a stud wall according to the NDS.

Description:	9' Tall Wall	9' Tall Wall	10.5' Tall Wall	King Stud (12' Max Opening)	King Stud (9.5' Max Opening)	
Type:	2x Lumber (2"-4")	2x Lumber (2"-4")	2x Lumber (2"-4")	2x Lumber (2"-4")	2x Lumber (2"-4")	
Species:	DF-L	DF-L	DF-L	DF-L	DF-L	
Grade:	No. 2	No. 2	No. 2	No. 2	No. 2	
Nominal width, t =	(1) 2	(1) 2	(1) 2	(2) 2	(1) 2	
Actual width =	1.50 in	1.50 in	1.50 in	3.00 in	1.50 in	
Nominal depth, d =	6	6	6	6	6	
Actual depth =	5.50 in	5.50 in	5.50 in	5.50 in	5.50 in	
Span, L =	9.000 ft	9.000 ft	10.500 ft	10.500 ft	9.000 ft	
w/o Plates	8.750 ft	8.750 ft	10.250 ft	10.250 ft	8.750 ft	
Stud spacing, s =	12 in	16 in	16 in	82 in	67 in	
Lat. Pressure, w _{wind} =	14.58 psf	14.58 psf	14.58 psf	14.58 psf	14.58 psf	
Axial load, P =	4168 lbs	5335 lbs	2783 lbs	50 lbs	50 lbs	
Eccentricity, e =	0 in	0 in	0 in	0 in	0 in	
K _{cE} =	0.3	0.3	0.3	0.3	0.3	
c =	0.8	0.8	0.8	0.8	0.8	
w =	14.6 plf	19.4 plf	19.4 plf	99.9 plf	81.7 plf	
F _b	900 psi	900 psi	900 psi	900 psi	900 psi	
F _v	180 psi	180 psi	180 psi	180 psi	180 psi	
F _{c-prll}	1,350 psi	1,350 psi	1,350 psi	1,350 psi	1,350 psi	
F _{c-perp}	625 psi	625 psi	625 psi	625 psi	625 psi	
C _d	1.60	1.60	1.60	1.60	1.60	
C _{F,Fb}	1.30	1.30	1.30	1.30	1.30	
C _{F,Fcprll}	1.10	1.10	1.10	1.10	1.10	
C _r	1.15	1.15	1.15	1.00	1.00	
C _p	0.47	0.47	0.36	0.36	0.47	
C _H	1.00	1.00	1.00	1.00	1.00	
C _b	1.07	1.07	1.07	1.07	1.07	
E	1,600,000 psi	1,600,000 psi	1,600,000 psi	1,600,000 psi	1,600,000 psi	
E _{min}	580,000 psi	580,000 psi	580,000 psi	580,000 psi	580,000 psi	
Allowable Stress:						
F' _b = F _b C _d C _F C _r	2153 psi	2153 psi	2153 psi	1872 psi	1872 psi	
F' _v = F _v C _d C _H	288 psi	288 psi	288 psi	288 psi	288 psi	
F' _c = F _c C _d C _F	2376 psi	2376 psi	2376 psi	2376 psi	2376 psi	
F' _{cE} = (K _{cE} E')/(l/d)2	1317 psi	1317 psi	960 psi	960 psi	1317 psi	
F' _c = F _c C _d C _F C _p	1118 psi	1118 psi	862 psi	862 psi	1118 psi	
F' _{c-perp} = F _{c-perp} C _b	668 psi	668 psi	668 psi	668 psi	668 psi	
E' = E	1600000 psi	1600000 psi	1600000 psi	1600000 psi	1600000 psi	
F _{bE} =	2712 psi	2712 psi	2315 psi	9259 psi	2712 psi	
Slenderness Ratio:	< 50 OK	< 50 OK	< 50 OK	< 50 OK	< 50 OK	
R _g =	16	16	17	9	16	
Bending:	< F'_b OK	< F'_b OK	< F'_b OK	< F'_b OK	< F'_b OK	
M = w L ² /8 + P e/12 =	139 ft-lbs	186 ft-lbs	255 ft-lbs	1312 ft-lbs	782 ft-lbs	
f _b = M/S =	221 psi	295 psi	405 psi	1041 psi	1240 psi	
S =	8 in ³	8 in ³	8 in ³	15 in ³	8 in ³	
Shear:	< F'_v OK	< F'_v OK	< F'_v OK	< F'_v OK	< F'_v OK	
V = w L/2 =	64 lbs	85 lbs	100 lbs	512 lbs	357 lbs	
f _v = 1.5 V/A =	12 psi	15 psi	18 psi	47 psi	65 psi	
A =	8 in ²	8 in ²	8 in ²	17 in ²	8 in ²	
Compression:	< F'_c OK	< F'_c OK	< F'_c OK	< F'_c OK	< F'_c OK	
f _c = P/A =	505 psi	647 psi	337 psi	3 psi	6 psi	
Compression (perp.):	< F'_c OK	< F'_c OK	< F'_c OK	< F'_c OK	< F'_c OK	
f _{c-perp} = P/A =	505 psi	647 psi	337 psi	3 psi	6 psi	
Combined:	< 1.0 OK	< 1.0 OK	< 1.0 OK			
(f _c /F _c)2 + (f _b /[F _b (1-(f _c /F _c E))]) =	0.37	0.60	0.44			
Deflection:	> 180 OK	> 180 OK	> 180 OK	> 180 OK	> 180 OK	
D = 22.5 w L ⁴ /E' I =	0.06 in	0.08 in	0.15 in	0.37 in	0.32 in	
I =	21 in ⁴	21 in ⁴	21 in ⁴	42 in ⁴	21 in ⁴	
SPAN /	1817	1363	848	330	324	

UNBRACED WOOD COLUMN ALLOWABLE LOADS (kips)

Column Type	Unbraced Height							Compression Perp. To Grain
	8'	10'	12'	14'	16'	18'	20'	
(2) 2x4 DF #2	4.50	3.00	2.10	SR	SR	SR	SR	6.50
(3) 2x4 DF #2	8.80	5.90	4.20	3.20	SR	SR	SR	9.80
4x4 DF #2	7.00	4.60	3.30	2.40	SR	SR	SR	7.60
(2) 2x6 DF #2	7.20	4.70	3.30	SR	SR	SR	SR	10.30
(3) 2x6 DF #2	20.40	14.70	10.70	8.00	6.20	4.90	SR	15.40
6x6 DF #2	18.00	15.70	13.00	10.50	8.50	6.90	5.70	18.90
6x8 DF #2	24.50	21.40	17.80	14.30	11.60	9.40	7.80	25.70
6x10 DF #2	31.40	27.10	22.50	18.20	14.70	12.00	9.90	32.60
8x8 DF #2	36.60	34.60	31.90	28.50	24.90	21.30	18.20	35.20
8x10 DF #2	46.30	43.90	40.40	36.20	31.50	27.00	23.10	44.50
8x12 DF #2	56.20	53.10	49.00	43.80	38.10	32.70	28.00	53.40
10x10 DF #2	60.50	58.80	56.50	53.40	49.60	45.20	40.50	56.40

Wood Column

Project File: 05 Beams.ec6

LIC# : KW-06013353, Build:20.23.2.14

SNAKE RIVER ENGINEERING

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DESCRIPTION: RB2 BEARING

Code References

Calculations per NDS 2018, IBC 2018, CBC 2019, ASCE 7-16
 Load Combinations Used : IBC 2018

General Information

Analysis Method	Allowable Stress Design	Wood Section Name	6x8
End Fixities	Top & Bottom Pinned	Wood Grading/Manuf.	Graded Lumber
Overall Column Height	21.75 ft	Wood Member Type	Sawn
<i>(Used for non-slender calculations)</i>			
Wood Species	Douglas Fir-Larch	Exact Width	5.50 in
Wood Grade	No.2	Exact Depth	7.50 in
Fb +	750 psi	Fv	170 psi
Fb -	750 psi	Ft	475 psi
Fc - Prll	700 psi	Density	31.21 pcf
Fc - Perp	625 psi		
E : Modulus of Elasticity . . .	x-x Bending	y-y Bending	Axial
	Basic	1300	1300
	Minimum	470	470
			1300 ksi
			Brace condition for deflection (buckling) along columns :
			X-X (width) axis : Fully braced against buckling ABOUT Y-Y Axis
			Y-Y (depth) axis : Unbraced Length for buckling ABOUT X-X Axis = 21.75 ft

Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Column self weight included : 194.453 lbs * Dead Load Factor

AXIAL LOADS . . .

Axial Load at 21.750 ft, D = 1.230, S = 9.420 k

DESIGN SUMMARY

Bending & Shear Check Results

PASS Max. Axial+Bending Stress Ratio = **0.9155 : 1**
 Load Combination +D+S
 Governing NDS Formula Comp Only, f_c/f_c'
 Location of max.above base 0.0 ft
 At maximum location values are .
 Applied Axial 10.844 k
 Applied Mx 0.0 k-ft
 Applied My 0.0 k-ft
 Fc : Allowable 287.166 psi

Maximum SERVICE Lateral Load Reactions . .
 Top along Y-Y 0.0 k Bottom along Y-Y 0.0 k
 Top along X-X 0.0 k Bottom along X-X 0.0 k

Maximum SERVICE Load Lateral Deflections . . .
 Along Y-Y 0.0 in at 0.0 ft above base
 for load combination : n/a
 Along X-X 0.0 in at 0.0 ft above base
 for load combination : n/a

PASS Maximum Shear Stress Ratio = **0.0 : 1**
 Load Combination +0.60D
 Location of max.above base 21.750 ft
 Applied Design Shear 0.0 psi
 Allowable Shear 272.0 psi

Other Factors used to calculate allowable stresses . . .
 Bending Compression Tension

Load Combination Results

Load Combination	C _D	C _P	Maximum Axial + Bending Stress Ratios			Maximum Shear Ratios		
			Stress Ratio	Status	Location	Stress Ratio	Status	Location
D Only	0.900	0.438	0.1251	PASS	0.0 ft	0.0	PASS	21.750 ft
+D+S	1.150	0.357	0.9155	PASS	0.0 ft	0.0	PASS	21.750 ft
+D+0.750S	1.150	0.357	0.7167	PASS	0.0 ft	0.0	PASS	21.750 ft
+0.60D	1.600	0.266	0.06965	PASS	0.0 ft	0.0	PASS	21.750 ft

Maximum Reactions

Note: Only non-zero reactions are listed.

Load Combination	X-X Axis Reaction		Y-Y Axis Reaction		Axial Reaction	My - End Moments		Mx - End Moments	
	@ Base	@ Top	@ Base	@ Top		@ Base	@ Top	@ Base	@ Top
D Only					1.424				
+D+S					10.844				
+D+0.750S					8.489				

Wood Column

Project File: 05 Beams.ec6

LIC# : KW-06013353, Build:20.23.2.14

SNAKE RIVER ENGINEERING

(c) ENERCALC INC 1983-2022

DESCRIPTION: RB2 BEARING

Maximum Reactions

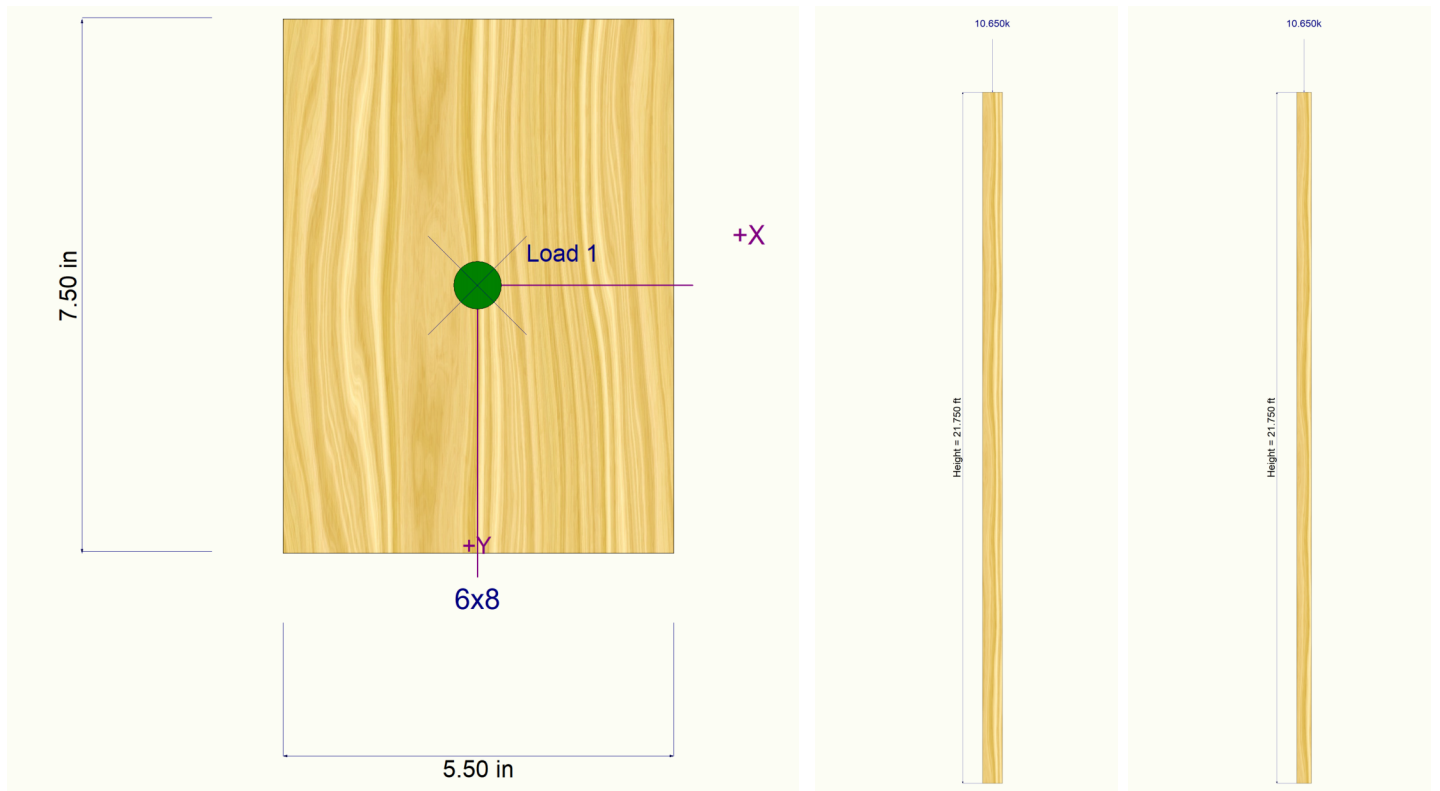
Note: Only non-zero reactions are listed.

Load Combination	X-X Axis Reaction		k	Y-Y Axis Reaction		Axial Reaction	My - End Moments		k-ft	Mx - End Moments	
	@ Base	@ Top		@ Base	@ Top		@ Base	@ Top		@ Base	@ Top
+0.60D						0.855					
S Only						9.420					

Maximum Deflections for Load Combinations

Load Combination	Max. X-X Deflection	Distance	Max. Y-Y Deflection	Distance
D Only	0.0000 in	0.000ft	0.000 in	0.000 ft
+D+S	0.0000 in	0.000ft	0.000 in	0.000 ft
+D+0.750S	0.0000 in	0.000ft	0.000 in	0.000 ft
+0.60D	0.0000 in	0.000ft	0.000 in	0.000 ft
S Only	0.0000 in	0.000ft	0.000 in	0.000 ft

Sketches



Wood Column

Project File: 05 Beams.ec6

LIC# : KW-06013353, Build:20.23.2.14

SNAKE RIVER ENGINEERING

(c) ENERCALC INC 1983-2022

DESCRIPTION: FB4 BEARING

Maximum Reactions

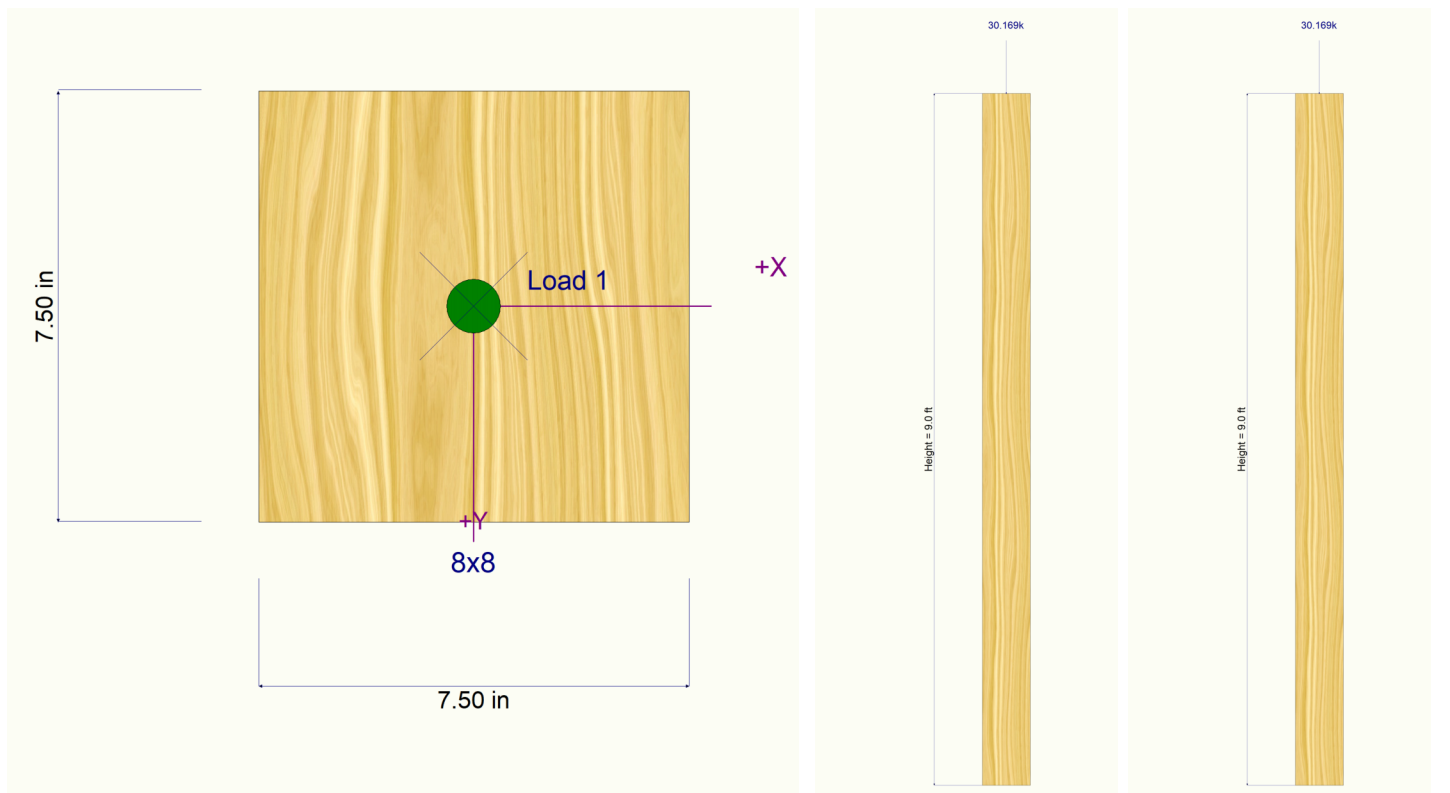
Note: Only non-zero reactions are listed.

Load Combination	X-X Axis Reaction		k	Y-Y Axis Reaction		Axial Reaction	My - End Moments		k-ft Mx - End Moments	
	@ Base	@ Top		@ Base	@ Top		@ Base	@ Top	@ Base	@ Top
+0.60D						2.513				
S Only						26.091				

Maximum Deflections for Load Combinations

Load Combination	Max. X-X Deflection	Distance	Max. Y-Y Deflection	Distance
D Only	0.0000 in	0.000ft	0.000 in	0.000 ft
+D+S	0.0000 in	0.000ft	0.000 in	0.000 ft
+D+0.750S	0.0000 in	0.000ft	0.000 in	0.000 ft
+0.60D	0.0000 in	0.000ft	0.000 in	0.000 ft
S Only	0.0000 in	0.000ft	0.000 in	0.000 ft

Sketches



Pole Soil Bearing Pressure

Axial Load

2600 pounds

Design Soil Bearing Pressure

1500 psf

Skin Friction (Soil to Concrete)

250 psf

Height of Pole Embedment

0 inches

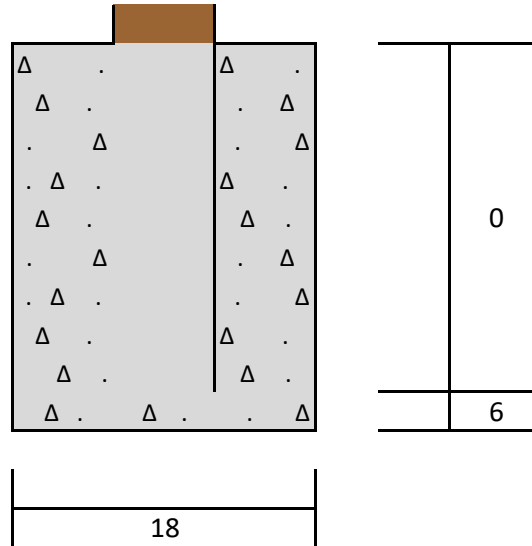
Diameter of Concrete Footing

18 inches

Allowable Axial Load

2651 pounds

2651 > 2600
OK



Individual Footing Design

Program: Continuous Footing

Soil Bearing Pressure: 1500psf

Roof				
Roof Dead	(17psf)	(6.0ft)	=	102plf
Snow Live	(150psf)	(6.0ft)	=	900plf

Upper Floor				
Floor Dead	(12psf)	(.0ft)	=	plf
Floor Live	(40psf)	(.0ft)	=	plf

Main Floor				
Floor Dead	(12psf)	(4.0ft)	=	48plf
Floor Live	(40psf)	(4.0ft)	=	160plf

Deck Cover				
Roof Dead	(17psf)	(.0ft)	=	plf
Snow Live	(150psf)	(.0ft)	=	plf

Deck Floor				
Floor Dead	(12psf)	(.0ft)	=	plf
Snow Live	(150psf)	(.0ft)	=	plf

Misc				
Wall Load:	(12psf)	(10.5ft)	=	126plf
Conc Stem:	(145pcf)	(2 x .5ft)	=	145plf
Misc Load:	(.0ft)	(.0ft)	=	plf

1321plf

Use Footing Width:	12	x	8	in
W/		(2)	#4	Cont.

Individual Footing Design

Program: Continuous Footing

Soil Bearing Pressure: 1500psf

Roof				
Roof Dead	(17psf)	(21.2ft)	=	360plf
Snow Live	(150psf)	(21.2ft)	=	3174plf

Upper Floor				
Floor Dead	(12psf)	(.0ft)	=	plf
Floor Live	(40psf)	(.0ft)	=	plf

Main Floor				
Floor Dead	(12psf)	(7.0ft)	=	84plf
Floor Live	(40psf)	(7.0ft)	=	280plf

Deck Cover				
Roof Dead	(17psf)	(.0ft)	=	plf
Snow Live	(150psf)	(.0ft)	=	plf

Deck Floor				
Floor Dead	(12psf)	(.0ft)	=	plf
Snow Live	(150psf)	(.0ft)	=	plf

Misc				
Wall Load:	(12psf)	(10.5ft)	=	126plf
Conc Stem:	(145pcf)	(2 x .5ft)	=	145plf
Misc Load:	(.0ft)	(.0ft)	=	plf

3889plf

Use Footing Width:	36	x	10	in
W/		(3)	#4	Cont.

Individual Footing Design

Program: Continuous Footing

Soil Bearing Pressure: 1500psf

Roof				
Roof Dead	(17psf)	(22.0ft)	=	374plf
Snow Live	(150psf)	(22.0ft)	=	3300plf

Upper Floor				
Floor Dead	(12psf)	(.0ft)	=	plf
Floor Live	(40psf)	(.0ft)	=	plf

Main Floor				
Floor Dead	(12psf)	(1.0ft)	=	12plf
Floor Live	(40psf)	(1.0ft)	=	40plf

Deck Cover				
Roof Dead	(17psf)	(.0ft)	=	plf
Snow Live	(150psf)	(.0ft)	=	plf

Deck Floor				
Floor Dead	(12psf)	(5.0ft)	=	60plf
Snow Live	(150psf)	(5.0ft)	=	750plf

Misc				
Wall Load:	(12psf)	(10.5ft)	=	126plf
Conc Stem:	(145pcf)	(2 x .5ft)	=	145plf
Misc Load:	(.0ft)	(.0ft)	=	plf

4767plf

Use Footing Width:	48	x	10	in
W/		(4)	#4	Cont.

Individual Footing Design

Program: Continuous Footing

Soil Bearing Pressure: 1500psf

Roof				
Roof Dead	(17psf)	(7.0ft)	=	119plf
Snow Live	(150psf)	(7.0ft)	=	1050plf

Upper Floor				
Floor Dead	(12psf)	(.0ft)	=	plf
Floor Live	(40psf)	(.0ft)	=	plf

Main Floor				
Floor Dead	(12psf)	(1.0ft)	=	12plf
Floor Live	(40psf)	(1.0ft)	=	40plf

Deck Cover				
Roof Dead	(17psf)	(.0ft)	=	plf
Snow Live	(150psf)	(.0ft)	=	plf

Deck Floor				
Floor Dead	(12psf)	(1.0ft)	=	12plf
Snow Live	(150psf)	(1.0ft)	=	150plf

Misc				
Wall Load:	(12psf)	(10.5ft)	=	126plf
Conc Stem:	(145pcf)	(2 x .5ft)	=	145plf
Misc Load:	(.0ft)	(.0ft)	(.0ft)	= plf

1614plf

Use Footing Width:	16	x	8	in
W/		(2)	#4	Cont.

Individual Footing Design

Program: Continuous Footing

Soil Bearing Pressure: 1500psf

Roof				
Roof Dead	(17psf)	(12.2ft)	=	207plf
Snow Live	(150psf)	(12.2ft)	=	1824plf

Upper Floor				
Floor Dead	(12psf)	(.0ft)	=	plf
Floor Live	(40psf)	(.0ft)	=	plf

Main Floor				
Floor Dead	(12psf)	(.0ft)	=	plf
Floor Live	(40psf)	(.0ft)	=	plf

Deck Cover				
Roof Dead	(17psf)	(.0ft)	=	plf
Snow Live	(150psf)	(.0ft)	=	plf

Deck Floor				
Floor Dead	(12psf)	(3.1ft)	=	38plf
Snow Live	(150psf)	(3.1ft)	=	469plf

Misc				
Wall Load:	(12psf)	(10.5ft)	=	126plf
Conc Stem:	(145pcf)	(2 x .5ft)	=	145plf
Misc Load:	(.0ft)	(.0ft)	(.0ft)	= plf

2808plf

Use Footing Width:	30	x	10	in
W/		(3)	#4	Cont.

Individual Footing Design

Program: Continuous Footing

Soil Bearing Pressure: 1500psf

Roof				
Roof Dead	(17psf)	(11.2ft)	=	190plf
Snow Live	(150psf)	(11.2ft)	=	1674plf

Upper Floor				
Floor Dead	(12psf)	(.0ft)	=	plf
Floor Live	(40psf)	(.0ft)	=	plf

Main Floor				
Floor Dead	(12psf)	(.0ft)	=	plf
Floor Live	(40psf)	(.0ft)	=	plf

Deck Floor				
Floor Dead	(12psf)	(.0ft)	=	plf
Snow Live	(150psf)	(.0ft)	=	plf

Misc				
Wall Load:	(12psf)	(10.5ft)	=	126plf
Conc Stem:	(145pcf)	(2 x .5ft)	=	145plf
Misc Load:	(.0ft)	(.0ft)	(.0ft)	= plf

2135plf

Use Footing Width:	24	x	8	in
W/	(2)	#4	Cont.	

Individual Footing Design

Program: Continuous Footing

Soil Bearing Pressure: 1500psf

Roof				
Roof Dead	(17psf)	(3.0ft)	=	51plf
Snow Live	(150psf)	(3.0ft)	=	450plf

Upper Floor				
Floor Dead	(12psf)	(1.0ft)	=	12plf
Floor Live	(40psf)	(1.0ft)	=	40plf

Main Floor				
Floor Dead	(12psf)	(1.0ft)	=	12plf
Floor Live	(40psf)	(1.0ft)	=	40plf

Deck Cover				
Roof Dead	(17psf)	(5.0ft)	=	85plf
Snow Live	(150psf)	(5.0ft)	=	750plf

Deck Floor				
Floor Dead	(30psf)	(5.0ft)	=	150plf
Snow Live	(150psf)	(5.0ft)	=	750plf

Misc				
Wall Load:	(12psf)	(10.5ft)	=	126plf
Conc Stem:	(145pcf)	(2 x .5ft)	=	145plf
Misc Load:	(.0ft)	(.0ft)	(.0ft)	= plf

2531plf

Use Footing Width:	24	x	8	in
W/		(2)	#4	Cont.

PAD FOOTING DESIGN CAPACITIES:

Soil Bearing (1500 psf)							
Dimensions (Inches)			Capacity	# of Bars	Min. Col. Size		
72	x	72	x	12	47,500 lbs	10	3.5 sq.
66	x	66	x	12	39,750 lbs	8	3.5 sq.
60	x	60	x	10	33,450 lbs	6	3.5 sq.
54	x	54	x	10	27,000 lbs	5	3.5 sq.
48	x	48	x	8	21,500 lbs	4	3.5 sq.
42	x	42	x	8	16,500 lbs	4	3.5 sq.
36	x	36	x	8	12,000 lbs	4	3.5 sq.
30	x	30	x	8	8,350 lbs	3	3.5 sq.
24	x	24	x	8	5,300 lbs	2	3.5 sq.
18	x	18	x	8	2,900 lbs	2	3.5 sq.

Bars to be 3 1/2" from bottom of pad. Evenly space in both directions.

CONT. FOOTING DESIGN CAPACITIES:

Soil Bearing (1500 psf)				
Dimensions (Inches)			Capacity	# of Bars
60	x	10	6,850 plf	6
54	x	10	6,200 plf	5
48	x	10	5,500 plf	4
42	x	10	4,750 plf	4
36	x	10	4,000 plf	3
30	x	10	3,400 plf	3
24	x	8	2,800 plf	2
18	x	8	2,100 plf	2
16	x	8	1,850 plf	2
12	x	8	1,350 plf	2

Bars to be 3 1/2" from bottom of footing.