

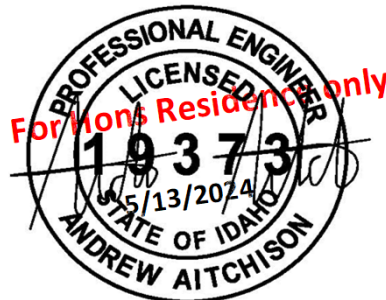
Structural Calculations

Project Title: Hons Residence

Address: Boulder Lake Est. Lot #2

Location: Valley County, Idaho

Job #: 2024-7378



Prepared in accordance with 2018 IBC. Calculations expire by: 5/13/2025

SITE SPECIFIC DESIGN CRITERIA:

Snow Criteria:

Roof Load (P_f)	150 psf	
Ground Load (P_g)	150 psf	
Exposure Factor (C_e)	1.0	Partially
Thermal Factor (C_t)	1.0	Typical
Importance (I_s)	1.0	

Wind Criteria:

Wind Speed (V_3)	115 mph	
Wind Exposure	C	Open Terrain
Wind Importance (I_w)	1.0	
Building Category	II	

Seismic Criteria:

Site Class	D	Stiff Soil
S_s	0.51	F_a 1.39
S_1	0.15	F_v 2.19
S_{D1}	0.47	S_{D1} 0.22
Risk Category	II	Other
Seismic Importance (I_E)	1.0	
Seismic Design Category (SDC)	D	

Seismic Criteria (continued):

Wall Material	Design Base Shear	Response Coeff., R	
OSB	.09Wp	6.5	Typ @ Ext
GYP	.28Wp	2	Typ @ Int
Cant. Col.	.38Wp	1.5	

Soil Criteria:

Brg. Strength	1500 psf
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STRUCTURE SPECIFIC DESIGN CRITERIA:

Live Loads:

Typ Residential	40 psf
Garage (P.V.)	50 psf
Sleeping Area's	30 psf

Roof Dead Loads:

Deck	1.5
Insulation	2.0
Roofing	3.0
Joist	2.5
Ceiling	3.0
Misc	4.5
TOTAL	17 psf

Roof not engineered for Tile, Slate or Concrete.

Exterior Wall Dead Loads:

Studs	2.0
Siding	2.5
Insulation	0.5
Gyp. Board	2.5
Sheathing	1.5
Misc	3.0
TOTAL	12 psf

Floor Dead Loads:

Deck	2.5
Joist	2.0
Ceiling	2.0
Flooring	2.5
Misc	3.0
TOTAL	12 psf

Floor joists not engineered for concrete overlay.

Interior Wall Dead Loads:

Studs	2.0
Gyp. Board	2.5
Misc	3.0
TOTAL	8 psf

Deck Dead Load

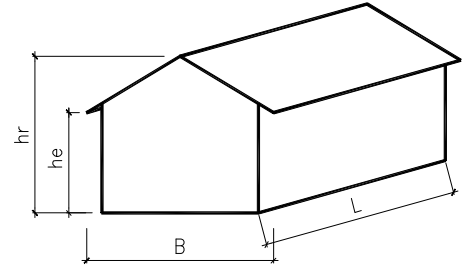
Decking	4.4
Joist	2.0
	0.0
Misc	3.0
TOTAL	10 psf

Deck not engineered for concrete overlay.

WIND ANALYSIS: Low-rise Building - Based on IBC / ASCE 7

INPUT DATA

Exposure category (B, C or D, ASCE 7-16 26.7.3)		C			
Importance factor (ASCE 7-16 Table 1.5-2)	$I_w =$	1.00	for all Category		
Basic wind speed (ASCE 7-16 26.5.1 or 2018 IBC)	$V =$	115	mph		
Topographic factor (ASCE 7-16 26.8 & Table 26.8-1)	$K_{zt} =$	1.00	Flat		
Building height to ridge	$h_r =$	25.58	ft		
Building height to eave	$h_e =$	9.00	ft		
Building width	$B =$	68.00	ft		
Building length	$L =$	81.00	ft		
Overhang sloped width	$O_h =$	3.00	ft		
Effective area of components (or Solar Panel area)	$A =$	27.0	ft ² , <== Overhang? (Yes or No):	Yes	
Enclosed? (Y/N)		y			



ANALYSIS

Velocity pressure

$$q_h = 0.00256 K_z K_{zt} K_d K_e V^2 = 25.17 \text{ psf}$$

where: q_h = velocity pressure at mean roof height, h. (Eq. 26.10-1 page 268)

K_z = velocity pressure exposure coefficient evaluated at height, h, (Tab. 26.10-1, pg. 266) = **0.87**

K_d = wind directionality factor. (Tab. 26.6-1, for building, page 266) = **0.85**

h = mean roof height = **17.29 ft**

K_e = ground elevation factor. (**1.0** per Sec. 26.9, page 268) **< 60 ft, [Satisfactory]** (ASCE 7-16 26.2.1)

< Min (L, B), [Satisfactory] (ASCE 7-16 26.2.2)

Design pressures for MWFRS

$$p = q_h [(G C_{pf}) - (G C_{pi})]$$

where: p = pressure in appropriate zone. (Eq. 28.3-1, page 311).

$p_{min} = 16 \text{ psf}$ (ASCE 7-16 28.3.4)

$G C_{pf}$ = product of gust effect factor and external pressure coefficient, see table below. (Fig. 28.3-1, page 312 & 313)

$G C_{pi}$ = product of gust effect factor and internal pressure coefficient. (Tab. 26.13-1, Enclosed Building, page 271)

= **0.18** or **-0.18**

a = width of edge strips, Fig 28.3-1, page 312, $\text{MAX}[\text{MIN}(0.1B, 0.1L, 0.4h), \text{MIN}(0.04B, 0.04L), 3] = 6.80 \text{ ft}$

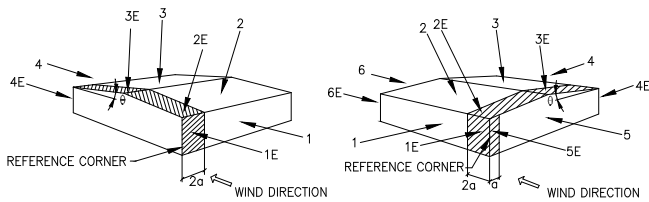
Net Pressures (psf), Basic Load Cases

Surface	Roof angle q = 18.43			Roof angle q = 18.43		
	$G C_{pf}$	Net Press. W/		$G C_{pf}$	Net Press. W/	
		(+ $G C_{pi}$)	(- $G C_{pi}$)		(+ $G C_{pi}$)	(- $G C_{pi}$)
1	0.52	8.47	17.53	-0.45	-15.86	-6.80
2	-0.69	-21.90	-12.84	-0.69	-21.90	-12.84
3	-0.47	-16.32	-7.26	-0.37	-13.84	-4.78
4	-0.42	-14.99	-5.92	-0.45	-15.86	-6.80
5				0.40	5.54	14.60
6				-0.29	-11.83	-2.77
1E	0.78	15.11	24.17	-0.48	-16.61	-7.55
2E	-1.07	-31.46	-22.40	-1.07	-31.46	-22.40
3E	-0.67	-21.48	-12.42	-0.53	-17.87	-8.81
4E	-0.62	-20.09	-11.03	-0.48	-16.61	-7.55
5E				0.61	10.82	19.88
6E				-0.43	-15.35	-6.29

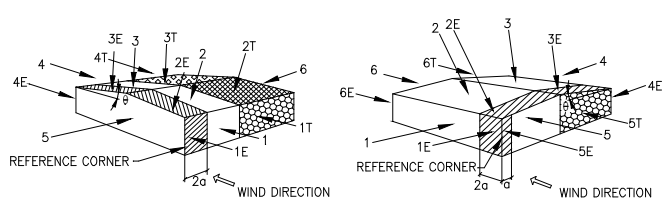
Net Pressures (psf), Torsional Load Cases

Surface	Roof angle q = 18.43		
	$G C_{pf}$	Net Press. W/	
		(+ $G C_{pi}$)	(- $G C_{pi}$)
1T	0.52	2.12	4.38
2T	-0.69	-5.47	-3.21
3T	-0.47	-4.08	-1.82
4T	0.00	-3.75	-1.48
Surface	Roof angle q = 0.00		
	$G C_{pf}$	Net Press. W/	
		(+ $G C_{pi}$)	(- $G C_{pi}$)
5T	0.40	1.38	3.65
6T	-0.29	-2.96	-0.69

+ / - Wind Pressure 64%



Load Case A (Transverse) Load Case B (Longitudinal)
Basic Load Cases



Load Case A (Transverse) Load Case B (Longitudinal)
Torsional Load Cases

Design pressures for components and cladding

$p = q_h [(G C_p) - (G C_{pi})]$

where: p = pressure on component. (Eq. 30.3-1, pg 33)

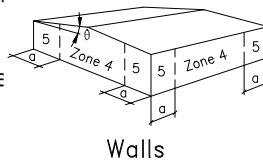
$p_{min} = 16.00$ psf (ASCE 7-16 30.2.2)

$G C_p = 1.00$ external pressure coefficient
 see table below. (ASCE 7-16 30.3.2)

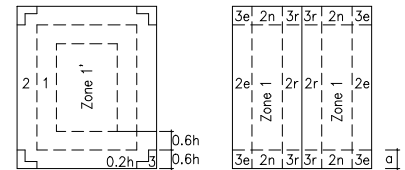
$q = 18.43$ °

$p_{overhang} = -86.84$ psf

(ASCE 7-16 28.3.3)



Walls



Roof $\theta \leq 7^\circ$

Roof $\theta > 7^\circ$

Comp. & Cladding Coeffs.	Effective Area (ft ²)	Zone 1		Zone 1'		Zone 2		Zone 2e		Zone 2n		Zone 2r	
		$G C_p$	- $G C_p$	$G C_p$	- $G C_p$	$G C_p$	- $G C_p$	$G C_p$	- $G C_p$	$G C_p$	- $G C_p$	$G C_p$	- $G C_p$
	1541	0.30	-0.80	0.30	-0.80	0.30	-2.20	0.30	-0.80	0.30	-1.00	0.30	-1.00
Effective Area (ft ²)	Zone 3		Zone 3e		Zone 3r		Zone 4		Zone 5				
	$G C_p$	- $G C_p$	$G C_p$	- $G C_p$	$G C_p$	- $G C_p$	$G C_p$	- $G C_p$	$G C_p$	- $G C_p$			
27	0.30	-2.50	0.30	-2.50	0.30	-1.80	0.99	-1.09	0.99	-1.38			

Comp. & Cladding Pressures	Zone 1		Zone 1'		Zone 2		Zone 2e		Zone 2n		Zone 2r	
	Positive	Negative	Positive	Negative	Positive	Negative	Positive	Negative	Positive	Negative	Positive	Negative
	3.02	-15.61	3.02	-15.61	3.02	-50.84	3.02	-15.61	3.02	-20.64	3.02	-20.64
	Zone 3		Zone 3e		Zone 3r		Zone 4		Zone 5		(Max Pressure 58.40 psf)	
Positive	Negative	Positive	Negative	Positive	Negative	Positive	Negative	Positive	Negative			
3.02	-58.40	3.02	-58.40	3.02	-40.78	20.38	-22.89	20.38	-30.18			

LOAD CASE 'A' FACTORED LOADS	
$0.6 * W_r = (Z_2 + Z_3) * 0.6 =$	3.3 psf
$0.6 * W_{rE} = (Z_{2E} + Z_{3E}) * 0.6 =$	6.0 psf
$0.6 * W_w = (Z_1 + Z_4) * 0.6 =$	14.1 psf
$0.6 * W_{wE} = (Z_{1E} + Z_{4E}) * 0.6 =$	21.1 psf

LOAD CASE 'B' FACTORED LOADS	
$0.6 * W_r = (Z_2 + Z_3) * 0.6 =$	4.8 psf
$0.6 * W_{rE} = (Z_{2E} + Z_{3E}) * 0.6 =$	8.2 psf
$0.6 * W_w = (Z_5 + Z_6) * 0.6 =$	10.4 psf
$0.6 * W_{wE} = (Z_{5E} + Z_{6E}) * 0.6 =$	15.7 psf

ROOF COMPONENTS FACTORED LOAD	
$0.6 * Z_{r,c\&c} =$	12.4 psf

WALL COMPONENTS FACTORED LOAD	
$0.6 * Z_{w,c\&c} =$	13.7 psf

OSB SEISMIC LOADING ANALYSIS

IBC / ASCE 7: Equivalent Lateral Force (ELF) Procedure:

INPUT DATA

Typical floor height: $h = 9$ ft
 Typical floor weight: $w_x = 93.6$ kips
 Number of floors: $n = 1$
 Importance factor (ASCE 11.5.1): $I_e = 1.00$
 Design spectral response: $S_{DS} = 0.47$ g
 $S_{D1} = 0.22$ g
 Mapped spectral resp.: $S_1 = 0.15$ g
 Period Parameter, C_t :
 (ASCE Tab 12.8-2): $C_t = 0.020$
 Resp. coefficient: (ASCE
 Tab. 12.2.1): $R = 6.5$
 Seismic design category: SDC = D
 $h_n = 25.6$ ft

DESIGN SUMMARY

$C_s = 1.2 * S_{DS} / (R / I_e) = 0.0870$ <= Applicable
 Period Parameter, $x = 0.75$, ASCE Tab 12.8-2
 Period: $T_a = C_t (h_n)^x = 0.23$ sec, ASCE 12.8.2.1
 $C_s < S_{D1} / [(R / I_e) T_a] = 0.1502$, ASCE Tab 12.8.1.1 <= Not Applicable
 $C_s > 0.044 S_{DS} I_e = 0.0207$, ASCE Tab 12.8.1.1 <= Not Applicable
 $C_s > 0.5 S_1 / (R / I_e) = 0.0117$, ASCE Tab 12.8.1.1 <= Not Applicable
 $k = 1.81$, (ASCE 12.8.3, page 91)
 $V = C_s W = 0.0870$ W
 $0.7 * V = 0.0609$ W
 $W = 94$ kips, total

SEISMIC COMPONENT & ANCHORING ANALYSIS

Out-of-plane seismic force for wall design (ASCE 7, Sec.12.11.1)

$$w_{1, seismic} = MAX(0.4 I S_{DS} W_p, 0.1 W_p) = 0.2 W_p = 0.2 \text{ psf} \quad \leq \text{USE FOR DIAPHRAGMS}$$

Where: $W_p = 1.0$ psf , $I_e = 1.00$
 (CBC / IBC Tab. 1604.5 & ASCE 7 Tab. 1.5-2)

Out-of-plane seismic force for anchorage design

For seismic design category A & B, any diaphragm (ASCE 7 Sec. 12.11.2)

$$F_{anch, seismic} = MAX \left[0.4 S_{DS} I W_p \frac{(h+h_p)^2}{2h}, 0.1 W_p \frac{(h+h_p)^2}{2h}, 400 S_{DS} I, F_{min} \right] =$$

Where: $F_{min} = 0.17$ plf, $1.77 W_p = 188$ plf (Horizontal) <= Not Applicable
 (ASCE 7 Sec. 12.11.2 & 11.7.3)

For seismic design category C and above, flexible diaphragm (ASCE 7 Sec. 12.11.2.1)

$$F_{anch, seismic} = MAX \left[0.8 S_{DS} I W_p \frac{(h+h_p)^2}{2h}, 0.1 W_p \frac{(h+h_p)^2}{2h}, 400 S_{DS} I, F_{min} \right] =$$

$= 3.54 W_p = 188$ plf (Horizontal) <= Applicable

For connections (ASCE 7 Sec. 12.11.2.1)

$$F_{conn, seismic} = MAX [0.133 S_{DS} w_p, 0.5 w_p] = 0.5 W_p = 0.5 \text{ plf (Horizontal)}$$

GYP SEISMIC LOADING ANALYSIS

IBC / ASCE 7: Equivalent Lateral Force (ELF) Procedure:

INPUT DATA

Typical floor height: $h = 9$ ft
 Typical floor weight: $w_x = 93.6$ kips
 Number of floors: $n = 1$
 Importance factor (ASCE 11.5.1): $I_e = 1.00$
 Design spectral response: $S_{DS} = 0.47$ g
 $S_{D1} = 0.22$ g
 Mapped spectral resp.: $S_1 = 0.15$ g
 Period Parameter, C_t :
 (ASCE Tab 12.8-2): $C_t = 0.020$
 Resp. coefficient: (ASCE
 Tab. 12.2.1): $R = 2$
 Seismic design category: SDC = D
 $h_n = 25.6$ ft

DESIGN SUMMARY

$C_s = 1.2 * S_{DS} / (R / I_e) = 0.2827$ <= Applicable
 Period Parameter, $x = 0.75$, ASCE Tab 12.8-2
 Period: $T_a = C_t (h_n)^x = 0.23$ sec, ASCE 12.8.2.1
 $C_s < S_{D1} / [(R / I_e) T_a] = 0.4882$, ASCE Tab 12.8.1.1 <= Not Applicable
 $C_s > 0.044 S_{DS} I_e = 0.0207$, ASCE Tab 12.8.1.1 <= Not Applicable
 $C_s > 0.5 S_1 / (R / I_e) = 0.0380$, ASCE Tab 12.8.1.1 <= Not Applicable
 $k = 1.81$, (ASCE 12.8.3, page 91)
 $V = C_s W = 0.2827$ W
 $0.7 * V = 0.1979$ W
 $W = 94$ kips, total

SEISMIC COMPONENT & ANCHORING ANALYSIS

Out-of-plane seismic force for wall design (ASCE 7, Sec.12.11.1)

$$w_{1, seismic} = MAX(0.4 I S_{DS} W_p, 0.1 W_p) = 0.2 W_p = 0.2 \text{ psf} \quad \leq \text{USE FOR DIAPHRAGMS}$$

Where: $W_p = 1.0$ psf, $I_e = 1.00$
 (CBC / IBC Tab. 1604.5 & ASCE 7 Tab. 1.5-2)

Out-of-plane seismic force for anchorage design

For seismic design category A & B, any diaphragm (ASCE 7 Sec. 12.11.2)

$$F_{anch, seismic} = MAX \left[0.4 S_{DS} I W_p \frac{(h+h_p)^2}{2h}, 0.1 W_p \frac{(h+h_p)^2}{2h}, 400 S_{DS} I, F_{min} \right] =$$

Where: $F_{min} = 0.17$ plf, $1.77 W_p = 188$ plf (Horizontal) <= Not Applicable
 (ASCE 7 Sec. 12.11.2 & 11.7.3)

For seismic design category C and above, flexible diaphragm (ASCE 7 Sec. 12.11.2.1)

$$F_{anch, seismic} = MAX \left[0.8 S_{DS} I W_p \frac{(h+h_p)^2}{2h}, 0.1 W_p \frac{(h+h_p)^2}{2h}, 400 S_{DS} I, F_{min} \right] =$$

$= 3.54 W_p = 188$ plf (Horizontal) <= Applicable

For connections (ASCE 7 Sec. 12.11.2.1)

$$F_{conn, seismic} = MAX [0.133 S_{DS} w_p, 0.5 w_p] = 0.5 W_p = 0.5 \text{ plf (Horizontal)}$$

WIND / SEISMIC SHEAR FORCE CALCULATIONS:

From ASCE 7-16 Wind & Seismic Loading Analysis

Wall Line	Roof / Floor						Wall					Load above		*C _s (W/p)	=	Loading		
	Wind Force (psf)	Diaph. Weight	Wr, We truss trib (ft)	Area W (ft)	Area L (ft)	Wind Force (psf)	Wall DL (psf)	Wall ht (ft)	wall line dist (ft)	Upr. Flr Wall ht (ft)	Wind (#)	Seismic (#)	Wind Force (kips)			Seismic Force (kips)	Lateral Control	
X1-1	9.6	55	4.3	16.0	26.0	20.1	12.0	9.0	16.0				0.06	=	1.05	0.80	Wind	
X2-1	9.6	55	4.3	16.0	79.0	20.1	12.0	9.0	16.0				0.06	=	4.38	6.06	Seismic	
	9.6	55	16.6	28.0	79.0	17.5	12.0	9.0	28.0				0.06	=				
X3-1	9.6	55	16.6	28.0	79.0	17.5	12.0	9.0	28.0				0.06	=	6.19	7.21	Seismic	
	9.6	55	13.5	24.0	79.0	18.1	12.0	12.0	24.0				0.06	=				
X4-1	9.6	55	13.5	24.0	24.0	18.1	12.0	12.0	24.0				0.06	=	2.86	1.17	Wind	
Y1-1	9.6	55	12.5	23.0	28.0	18.2	12.0	9.0	23.0				0.06	=	2.32	1.22	Wind	
Y2-1	9.6	55	12.5	23.0	68.0	18.2	12.0	9.0	23.0				0.06	=	4.97	5.61	Seismic	
	9.6	55	14.5	24.0	68.0	18.1	12.0	9.0	24.0				0.06	=				
Y3-1	9.6	55	14.5	24.0	68.0	18.1	12.0	9.0	24.0				0.06	=	6.40	6.96	Seismic	
	9.6	55	13.8	34.0	68.0	16.9	12.0	10.5	34.0				0.06	=				
Y4-1	9.6	55	13.8	34.0	28.0	16.9	12.0	10.5	34.0				0.06	=	3.75	1.84	Wind	
X1-S	9.6	55	11.0	22.0	50.0	18.4	12.0	16.4	22.0	0.0	0	0	0.06	=	2.83	2.09	Wind	
X2-S	9.6	55	11.0	22.0	50.0	18.4	12.0	16.4	22.0	0.0	0	0	0.06	=	2.83	2.09	Wind	
Y1-S	9.6	55	11.0	50.0	22.0	16.0	12.0	16.4	50.0	0	0	0	0.06	=	5.92	2.43	Wind	
Y2-S	9.6	55	11.0	50.0	22.0	16.0	12.0	16.4	50.0	0	0	0	0.06	=	5.92	2.43	Wind	

SHEAR WALL CALCULATIONS:

		X1-1	X2-1	X2-1	X3-1	X3-1	X4-1
Shear Wall Forces							
Number of Panels		1	1	1	1	1	2
Total length of wall		26.00 ft	25.00 ft	53.50 ft	24.00 ft	23.00 ft	24.00 ft
Total length of shear wall	L =	26.00 ft	25.00 ft	13.83 ft	24.00 ft	11.25 ft	3.50 ft
Total length of full ht seg.	L _w =	8.00 ft	19.08 ft	13.83 ft	21.00 ft	11.25 ft	3.50 ft
height of shear wall	H =	9.00 ft	10.50 ft	9.00 ft	10.50 ft	9.00 ft	11.83 ft
Maximum opening height	H' =	5.00 ft	5.00 ft	0.00 ft	5.00 ft	0.00 ft	0.00 ft
Total force at top of wall	V ₁ =	1049 lbs	3512 lbs	2545 lbs	4695 lbs	2515 lbs	1428 lbs
Self weight	W _{DL self} =	108 plf	126 plf	108 plf	126 plf	108 plf	142 plf
Applied dead load	W _{DL above} =	51 plf	51 plf	272 plf	272 plf	272 plf	51 plf
Prefered OSB thickness	in	7/16	7/16	7/16	7/16	7/16	7/16
Prefered Gyp thickness	in	1/2	1/2	1/2	1/2	1/2	1/2
Wall Connected to Concrete	y/n =	Y	Y	Y	Y	Y	Y
Shear Wall Segments							
		4.00	6.75	13.83	6.75	11.25	3.50
		4.00	6.00		14.25		
			6.33				
Shear Transfer to Concrete							
T =		Not Req'd	389 lbs	80 lbs	Not Req'd	730 lbs	4624 lbs
1/2 Anchor Bolts @		72 " O.C.	72 " O.C.	72 " O.C.	72 " O.C.	60 " O.C.	72 " O.C.
Provide:		Code Min.	Code Min.	Code Min.	Code Min.	A5	Code Min.
Min # of 1/2 Anchor Bolts		(2) Min	(4) Min	(3) Min	(5) Min	(3) Min	(2) Min
Load From Above		0.00	0.00	0.00	0.00	0.00	0.00
			Perp. Wall	Perp. Wall		HD1	HD3
Shear Resisting System							
Force Calculated		191.57	202.72	184.04	235.57	223.59	407.98
		OSB	OSB	OSB	OSB	OSB	OSB
Min Shear Wall Segment:		2.57 ft	3.00 ft	2.57 ft	3.00 ft	2.57 ft	3.38 ft
Provide:	V _a =	SW1	SW1	SW1	SW1	SW1	SW2
Min Shear Wall Segment:							
Provide:	V _a =						
Blocking / Nailing Framing Attachment							
Blocking Unit Shear		40 plf	140 plf	48 plf	196 plf	109 plf	119 plf
Blocking		NONE	NONE	NONE	B1	NONE	NONE
Nailing		See SCHED	See SCHED	See SCHED	T1	See SCHED	See SCHED
Unit Base Shear							
% of full height segments	%fh = L _w /L =	0.308	0.763	1.000	0.875	1.000	1.000
% of maximum opening height	%oh = H'/H =	0.556	0.476	0.000	0.476	0.000	0.000
Shear cap adj factor	SCAF =	0.68	0.91	1.00	0.95	1.00	1.00
Unit base shear	v _{base} V ₁ /L _w =	131 plf	184 plf	184 plf	224 plf	224 plf	408 plf
Effective unit base shear	v _{req} = v _{base} /SCAF =	192 plf	203 plf	184 plf	236 plf	224 plf	408 plf
Ovrtrn. mo. Ttl. length of wall	OTM =	13.8 k-ft	40.6 k-ft	22.9 k-ft	51.9 k-ft	22.6 k-ft	16.9 k-ft
Shear wall adjustment factor							
Resist moment total L. of wall	RM =	53.7 k-ft	55.3 k-ft	36.3 k-ft	114.6 k-ft	24.0 k-ft	1.2 k-ft
	r =	0.4444	0.8713	1.0000	0.9363	1.0000	1.0000
	C ₀ =	0.6842	0.9079	1.0000	0.9492	1.0000	1.0000

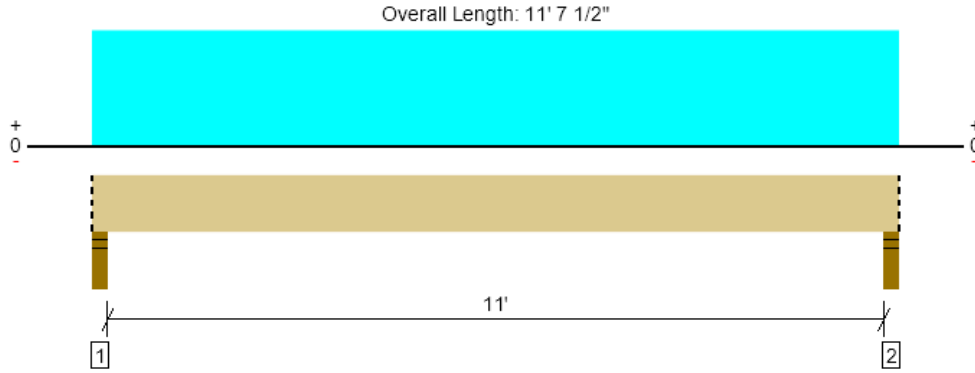
SHEAR WALL CALCULATIONS:

		Y1-1	Y2-1	Y2-1	Y3-1	Y3-1	Y4-1
Shear Wall Forces							
Number of Panels		1	1	1	1	1	2
Total length of wall		28.00 ft	40.33 ft	27.00 ft	40.50 ft	16.00 ft	28.00 ft
Total length of shear wall	L =	24.00 ft	19.75 ft	27.00 ft	40.50 ft	16.00 ft	3.00 ft
Total length of full ht seg.	L _w =	14.50 ft	19.75 ft	9.49 ft	25.80 ft	9.58 ft	3.00 ft
height of shear wall	H =	9.00 ft	12.00 ft	9.00 ft	12.00 ft	9.00 ft	9.00 ft
Maximum opening height	H' =	9.00 ft	0.00 ft	2.00 ft	8.00 ft	2.00 ft	0.00 ft
Total force at top of wall	V ₁ =	2324 lbs	3791 lbs	1821 lbs	5077 lbs	1885 lbs	1876 lbs
Self weight	W _{DL self} =	108 plf	144 plf	108 plf	144 plf	108 plf	108 plf
Applied dead load	W _{DL above} =	51 plf	357 plf	51 plf	51 plf	51 plf	51 plf
Prefered OSB thickness	in	7/16	7/16	7/16	7/16	7/16	7/16
Prefered Gyp thickness	in	1/2	1/2	1/2	1/2	1/2	1/2
Wall Connected to Concrete	y/n =	Y	Y	Y	Y	Y	Y
Shear Wall Segments							
		3.25	19.75	3.16	3.90	3.25	3.00
		3.25		6.33	3.90	6.33	
		8.00			18.00		
Shear Transfer to Concrete							
	T =	689 lbs	Not Req'd	Not Req'd	Not Req'd	497 lbs	3500 lbs
1/2 Anchor Bolts @		72" O.C.	72" O.C.	72" O.C.	72" O.C.	72" O.C.	
Provide:		Code Min.	Code Min.	Code Min.	Code Min.	Code Min.	
Min # of 1/2 Anchor Bolts		(3) Min	(4) Min	(2) Min	(5) Min	(2) Min	
Load From Above		0.00	0.00	0.00	0.00	0.00	0.00
Holddown		HD1				Perp. Wall	HD3
Shear Resisting System							
Force Calculated		287.14	191.93	191.93	268.23	196.80	625.25
		OSB	OSB	OSB	OSB	OSB	P.F.
Min Shear Wall Segment:		2.57 ft	3.43 ft	2.57 ft	3.43 ft	2.57 ft	1.33 ft
Provide:	V _a =	SW1	SW1	SW1	SW1	SW1	3853
Min Shear Wall Segment:							
Provide:	V _a =						
Blocking / Nailing Framing Attachment							
Blocking Unit Shear		83 plf	94 plf	67 plf	125 plf	118 plf	134 plf
Blocking		NONE	NONE	NONE	NONE	NONE	NONE
Nailing		See SCHED	See SCHED	See SCHED	See SCHED	See SCHED	See SCHED
Unit Base Shear							
% of full height segments	%fh = L _w /L =	0.604	1.000	0.351	0.637	0.599	1.000
% of maximum opening height	%oh = H'/H =	1.000	0.000	0.222	0.667	0.222	0.000
Shear cap adj factor	SCAF =	0.56	1.00	1.00	0.73	1.00	1.00
Unit base shear	v _{base} V ₁ /L _w =	160 plf	192 plf	192 plf	197 plf	197 plf	625 plf
Effective unit base shear	v _{req} = v _{base} /SCAF =	287 plf	192 plf	192 plf	268 plf	197 plf	625 plf
Ovrtrn. mo. Ttl. length of wall	OTM =	37.5 k-ft	45.5 k-ft	16.4 k-ft	83.0 k-ft	17.0 k-ft	16.9 k-ft
Shear wall adjustment factor							
Resist moment total L. of wall	RM =	45.8 k-ft	97.7 k-ft	58.0 k-ft	159.9 k-ft	20.4 k-ft	0.7 k-ft
	r =	0.6042	1.0000	0.7092	0.7247	0.8704	1.0000
	C ₀ =	0.5581	1.0000	1.2758	0.7337	1.1544	1.0000

SHEAR WALL CALCULATIONS:						
		X1-S	X2-S	Y1-S	Y2-S	
Shear Wall Forces						
Number of Panels		1	1	2	1	
Total length of wall		50.00 ft	50.00 ft	22.00 ft	22.00 ft	
Total length of shear wall	L =	43.00 ft	50.00 ft	5.00 ft	22.00 ft	
Total length of full ht seg.	L _w =	16.00 ft	16.00 ft	5.00 ft	12.00 ft	
height of shear wall	H =	16.42 ft	16.42 ft	16.42 ft	16.42 ft	
Maximum opening height	H' =	0.00 ft	5.00 ft	0.00 ft	5.00 ft	
Total force at top of wall	V ₁ =	2826 lbs	2826 lbs	2961 lbs	5922 lbs	
Self weight	w _{DL self} =	197 plf	197 plf	197 plf	197 plf	
Applied dead load	w _{DL above} =	51 plf	51 plf	51 plf	51 plf	
Prefered OSB thickness	in	7/16	7/16	7/16	7/16	
Prefered Gyp thickness	in	1/2	1/2	1/2	1/2	
Wall Connected to Concrete	y/n =	Y	Y	Y	Y	
Shear Wall Segments						
		8.00	8.00	5.00	6.00	
		8.00	8.00		6.00	
Shear Transfer to Concrete						
T =		Not Req'd	Not Req'd	9351 lbs	5102 lbs	
1/2 Anchor Bolts @		72 " O.C.	72 " O.C.	72 " O.C.	48 " O.C.	
Provide:		Code Min.	Code Min.	Code Min.	A4	
Min # of 1/2 Anchor Bolts		(3) Min	(3) Min	(3) Min	(6) Min	
Load From Above		0.00	0.00	0.00	0.00	
				HD6	HD3	
Shear Resisting System						
Force Calculated		176.61	176.61	592.17	493.48	
		OSB	OSB	OSB	OSB	
Min Shear Wall Segment:		4.69 ft	4.69 ft	4.69 ft	4.69 ft	
Provide:	V _a =	SW1	SW1	SW3	SW2	
Min Shear Wall Segment:						
Provide:	V _a =					
Blocking / Nailing Framing Attachment						
Blocking Unit Shear		57 plf	57 plf	269 plf	269 plf	
Blocking		NONE	NONE	B1	B1	
Nailing		See SCHED	See SCHED	T1	T1	
Unit Base Shear						
% of full height segments	%fh = L _w /L =	0.372	0.320	1.000	0.545	
% of maximum opening height	%oh = H'/H =	0.000	0.305	0.000	0.305	
Shear cap adj factor	SCAF =	1.00	1.00	1.00	1.00	
Unit base shear	v _{base} V ₁ /L _w =	177 plf	177 plf	592 plf	493 plf	
Effective unit base shear	v _{req} = v _{base} /SCAF =	177 plf	177 plf	592 plf	493 plf	
Ovrtrn. mo. Ttl. length of wall	OTM =	46.4 k-ft	46.4 k-ft	48.6 k-ft	97.2 k-ft	
Shear wall adjustment factor						
Resist moment total L. of wall	RM =	229.3 k-ft	310.1 k-ft	3.1 k-ft	60.0 k-ft	
	r =	0.9999	0.6071	1.0000	0.7976	
	C ₀ =	2.6867	1.0625	1.0000	1.0409	

Shop, RB1

1 piece(s) 6 3/4" x 10 1/2" 24F-V4 DF Glulam



Drawing is Conceptual. All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	8027 @ 2 1/4"	15820 (3.75")	Passed (51%)	--	1.0 D + 1.0 S (All Spans)
Shear (lbs)	6387 @ 1' 2 1/4"	14399	Passed (44%)	1.15	1.0 D + 1.0 S (All Spans)
Pos Moment (Ft-lbs)	21849 @ 5' 9 3/4"	28527	Passed (77%)	1.15	1.0 D + 1.0 S (All Spans)
Live Load Defl. (in)	0.377 @ 5' 9 3/4"	0.563	Passed (L/358)	--	1.0 D + 1.0 S (All Spans)
Total Load Defl. (in)	0.425 @ 5' 9 3/4"	0.750	Passed (L/318)	--	1.0 D + 1.0 S (All Spans)

Member Length : 11' 7 1/2"
 System : Roof
 Member Type : Drop Beam
 Building Use : Residential
 Building Code : IBC 2018
 Design Methodology : ASD
 Member Pitch : 0/12

- Deflection criteria: LL (L/240) and TL (L/180).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Critical positive moment adjusted by a volume/size factor of 1.00 that was calculated using length L = 11' 3".
- The effects of positive or negative camber have not been accounted for when calculating deflection.
- The specified glulam is assumed to have its strong laminations at the bottom of the beam. Install with proper side up as indicated by the manufacturer.
- Applicable calculations are based on NDS.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Snow	Factored	
1 - Stud wall - DF	3.75"	3.75"	1.90"	907	7120	8027	Blocking
2 - Stud wall - DF	3.75"	3.75"	1.90"	907	7120	8027	Blocking

• Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	11' 8" o/c	
Bottom Edge (Lu)	11' 8" o/c	

•Maximum allowable bracing intervals based on applied load.

Vertical Loads	Location (Side)	Tributary Width	Dead (0.90)	Snow (1.15)	Comments
0 - Self Weight (PLF)	0 to 11' 7 1/2"	N/A	17.2	--	
1 - Uniform (PSF)	0 to 11' 7 1/2" (Front)	8' 2"	17.0	150.0	Default Load

Weyerhaeuser Notes

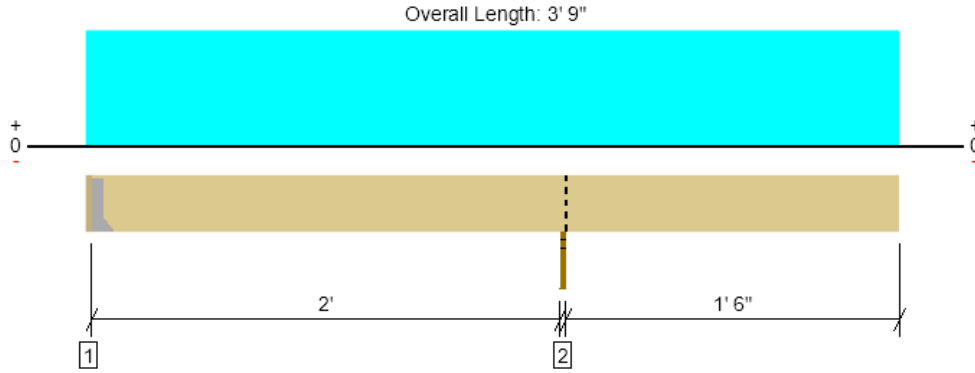
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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

ForteWEB Software Operator	Job Notes
Trevor Steelsmith Snake River Engineering (208) 453-6512 trevor@snakeriverengineering.com	



Shop, OUTLOOKERS
1 piece(s) 2 x 6 DF No.2 @ 24" OC



Drawing is Conceptual. All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	1064 @ 2' 2 1/4"	1406 (1.50")	Passed (76%)	--	1.0 D + 1.0 S (All Spans)
Shear (lbs)	368 @ 1' 8"	1139	Passed (32%)	1.15	1.0 D + 1.0 S (All Spans)
Moment (Ft-lbs)	-408 @ 2' 2 1/4"	975	Passed (42%)	1.15	1.0 D + 1.0 S (All Spans)
Live Load Defl. (in)	0.028 @ 3' 9"	0.200	Passed (2L/999+)	--	1.0 D + 1.0 S (Alt Spans)
Total Load Defl. (in)	0.030 @ 3' 9"	0.208	Passed (2L/999+)	--	1.0 D + 1.0 S (Alt Spans)

Member Length : 3' 7 1/2"
System : Roof
Member Type : Joist
Building Use : Residential
Building Code : IBC 2018
Design Methodology : ASD
Member Pitch : 0/12

- Deflection criteria: LL (L/240) and TL (L/180).
- Overhang deflection criteria: LL (0.2") and TL (2L/180).
- Right cantilever length exceeds 1/3 member length or 1/2 back span length. Additional bracing should be considered.
- Allowed moment does not reflect the adjustment for the beam stability factor.
- A 15% increase in the moment capacity has been added to account for repetitive member usage.
- Applicable calculations are based on NDS.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Snow	Factored	
1 - Hanger on 5 1/2" DF beam	1.50"	Hanger ¹	1.50"	19	258	277	See note ¹
2 - Stud wall - DF	1.50"	1.50"	1.50"	108	956	1064	Blocking

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.
- At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger
- ¹ See Connector grid below for additional information and/or requirements.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	3' 8" o/c	
Bottom Edge (Lu)	3' 8" o/c	

- Maximum allowable bracing intervals based on applied load.

Connector: Simpson Strong-Tie							
Support	Model	Seat Length	Top Fasteners	Face Fasteners	Member Fasteners	Accessories	
1 - Face Mount Hanger	LU26	1.50"	N/A	6-10dx1.5	4-10dx1.5		

- Refer to manufacturer notes and instructions for proper installation and use of all connectors.

Vertical Load	Location (Side)	Spacing	Dead (0.90)	Snow (1.15)	Comments
1 - Uniform (PSF)	0 to 3' 9"	24"	17.0	150.0	Default Load

Weyerhaeuser Notes

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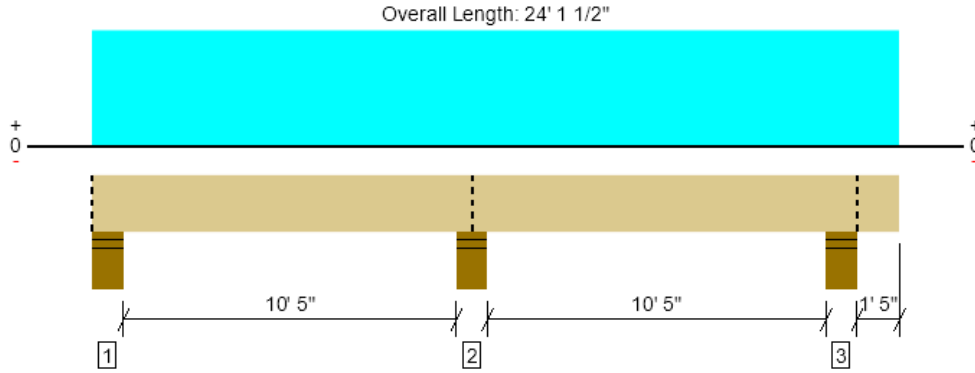
The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

ForteWEB Software Operator	Job Notes
Trevor Steelsmith Snake River Engineering (208) 453-6512 trevor@snakeriverengineering.com	



RESIDENCE, RB2

1 piece(s) 6 3/4" x 10 1/2" 24F-V4 DF Glulam



Drawing is Conceptual. All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	20633 @ 11' 4 1/4"	31641 (7.50")	Passed (65%)	--	1.0 D + 1.0 S (Adj Spans)
Shear (lbs)	8515 @ 10' 2"	14399	Passed (59%)	1.15	1.0 D + 1.0 S (Adj Spans)
Pos Moment (Ft-lbs)	14686 @ 4' 10 3/4"	28527	Passed (51%)	1.15	1.0 D + 1.0 S (Alt Spans)
Neg Moment (Ft-lbs)	-22463 @ 11' 4 1/4"	21990	Passed (102%)	1.15	1.0 D + 1.0 S (Adj Spans)
Live Load Defl. (in)	0.204 @ 5' 5 1/8"	0.543	Passed (L/637)	--	1.0 D + 1.0 S (Alt Spans)
Total Load Defl. (in)	0.223 @ 5' 4 3/4"	0.724	Passed (L/583)	--	1.0 D + 1.0 S (Alt Spans)

Member Length : 24' 1 1/2"
 System : Roof
 Member Type : Drop Beam
 Building Use : Residential
 Building Code : IBC 2018
 Design Methodology : ASD
 Member Pitch : 0/12

- Deflection criteria: LL (L/240) and TL (L/180).
- Overhang deflection criteria: LL (2L/240) and TL (2L/180).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Critical positive moment adjusted by a volume/size factor of 1.00 that was calculated using length L = 8' 9 1/2".
- Critical negative moment adjusted by a volume/size factor of 1.00 that was calculated using length L = 5' 5 3/8".
- The effects of positive or negative camber have not been accounted for when calculating deflection.
- The specified glulam is assumed to have its strong laminations at the bottom of the beam. Install with proper side up as indicated by the manufacturer.
- Applicable calculations are based on NDS.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Snow	Factored	
1 - Stud wall - DF	7.50"	7.50"	1.76"	780	6663	7442	Blocking
2 - Stud wall - DF	7.50"	7.50"	4.89"	2295	18338	20633	Blocking
3 - Stud wall - DF	7.50"	7.50"	2.29"	1032	8630	9662	Blocking

• Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	24' 2" o/c	
Bottom Edge (Lu)	6" o/c	

•Maximum allowable bracing intervals based on applied load.

Vertical Loads	Location (Side)	Tributary Width	Dead (0.90)	Snow (1.15)	Comments
0 - Self Weight (PLF)	0 to 24' 1 1/2"	N/A	17.2	--	
1 - Uniform (PSF)	0 to 24' 1 1/2" (Front)	9'	17.0	150.0	Default Load

Weyerhaeuser Notes

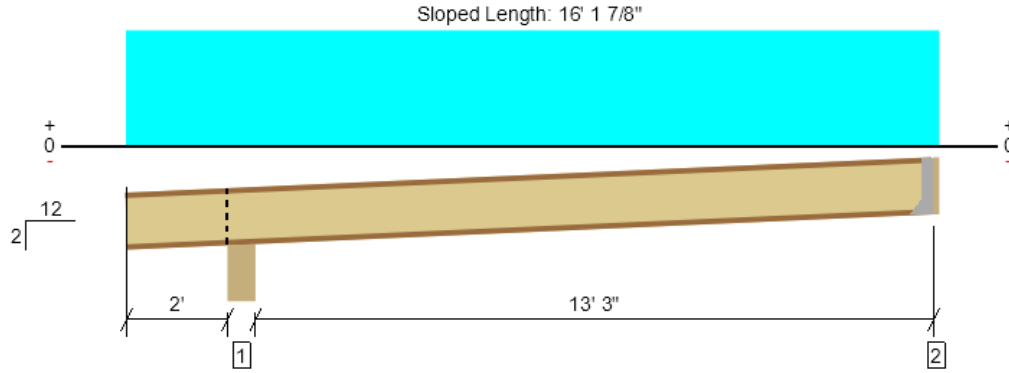
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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

ForteWEB Software Operator	Job Notes
Trevor Steelsmith 05/16/24 Snake River Engineering (208) 453-6512 trevor@snakeriverengineering.com	



RESIDENCE, Roof: Joist RIGHT DECK
1 piece(s) 11 7/8" TJI @ 360 @ 16" OC



Drawing is Conceptual. All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	1485 @ 15' 9 3/4"	1485 (2.62")	Passed (100%)	1.15	1.0 D + 1.0 S (Alt Spans)
Shear (lbs)	1485 @ 15' 9 3/4"	1961	Passed (76%)	1.15	1.0 D + 1.0 S (Alt Spans)
Moment (Ft-lbs)	4945 @ 9' 1 13/16"	7107	Passed (70%)	1.15	1.0 D + 1.0 S (Alt Spans)
Live Load Defl. (in)	0.440 @ 9' 15/16"	0.686	Passed (L/374)	--	1.0 D + 1.0 S (Alt Spans)
Total Load Defl. (in)	0.489 @ 9' 1"	0.915	Passed (L/337)	--	1.0 D + 1.0 S (Alt Spans)

Member Length : 16' 2 3/8"
System : Roof
Member Type : Joist
Building Use : Residential
Building Code : IBC 2018
Design Methodology : ASD
Member Pitch : 2/12

- Deflection criteria: LL (L/240) and TL (L/180).
- Overhang deflection criteria: LL (2L/240) and TL (2L/180).
- Allowed moment does not reflect the adjustment for the beam stability factor.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Snow	Factored	
1 - Beveled Plate - DF	6.75"	6.75"	3.50"	212	1848	2060	Blocking
2 - Hanger on 11 7/8" DF beam	1.50"	Hanger ¹	2.62" / - ²	154	1359	1513	See note ¹

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.
- At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger
- ¹ See Connector grid below for additional information and/or requirements.
- ² Required Bearing Length / Required Bearing Length with Web Stiffeners

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	4' 1" o/c	
Bottom Edge (Lu)	9' 7" o/c	

- TJI joists are only analyzed using Maximum Allowable bracing solutions.
- Maximum allowable bracing intervals based on applied load.

Connector: Simpson Strong-Tie						
Support	Model	Seat Length	Top Fasteners	Face Fasteners	Member Fasteners	Accessories
2 - Face Mount Hanger	Connector not found	N/A	N/A	N/A	N/A	

- Refer to manufacturer notes and instructions for proper installation and use of all connectors.

Vertical Load	Location	Spacing	Dead (0.90)	Snow (1.15)	Comments
1 - Uniform (PSF)	0 to 15' 11 1/4"	16"	17.0	150.0	Default Load

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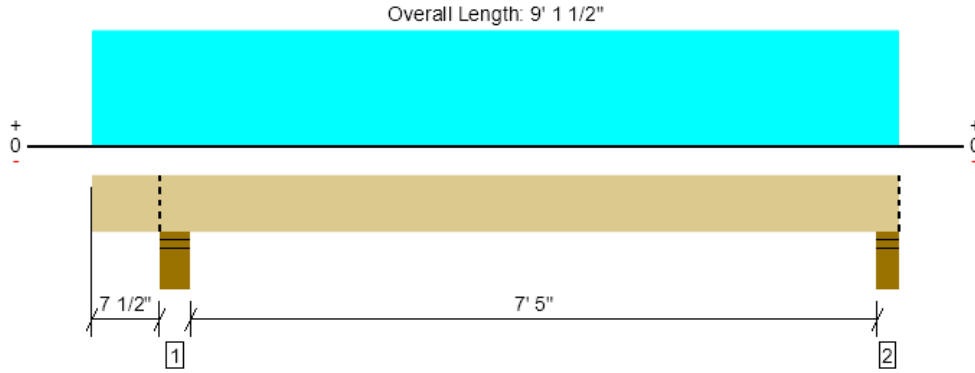
The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

ForteWEB Software Operator	Job Notes
Trevor Steelsmith Snake River Engineering (208) 453-6512 trevor@snakeriverengineering.com	



RESIDENCE, RB3

1 piece(s) 5 1/8" x 7 1/2" 24F-V4 DF Glulam



Drawing is Conceptual. All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	4984 @ 8' 9 1/2"	17617 (5.50")	Passed (28%)	--	1.0 D + 1.0 S (Alt Spans)
Shear (lbs)	3707 @ 8' 1/2"	7809	Passed (47%)	1.15	1.0 D + 1.0 S (Alt Spans)
Pos Moment (Ft-lbs)	8943 @ 4' 10 3/4"	11051	Passed (81%)	1.15	1.0 D + 1.0 S (Alt Spans)
Neg Moment (Ft-lbs)	-518 @ 11 1/4"	8518	Passed (6%)	1.15	1.0 D + 1.0 S (All Spans)
Live Load Defl. (in)	0.272 @ 4' 10 1/2"	0.393	Passed (L/346)	--	1.0 D + 1.0 S (Alt Spans)
Total Load Defl. (in)	0.305 @ 4' 10 1/2"	0.524	Passed (L/309)	--	1.0 D + 1.0 S (Alt Spans)

Member Length : 9' 1 1/2"
 System : Roof
 Member Type : Drop Beam
 Building Use : Residential
 Building Code : IBC 2018
 Design Methodology : ASD
 Member Pitch : 0/12

- Deflection criteria: LL (L/240) and TL (L/180).
- Overhang deflection criteria: LL (2L/240) and TL (2L/180).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Critical positive moment adjusted by a volume/size factor of 1.00 that was calculated using length L = 7' 9 1/2".
- Critical negative moment adjusted by a volume/size factor of 1.00 that was calculated using length L = 1' 9/16".
- The effects of positive or negative camber have not been accounted for when calculating deflection.
- The specified glulam is assumed to have its strong laminations at the bottom of the beam. Install with proper side up as indicated by the manufacturer.
- Applicable calculations are based on NDS.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Snow	Factored	
1 - Stud wall - DF	7.50"	7.50"	1.81"	632	5167	5798	Blocking
2 - Stud wall - DF	5.50"	5.50"	1.56"	540	4444	4984	Blocking

• Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	9' 2" o/c	
Bottom Edge (Lu)	9' 2" o/c	

•Maximum allowable bracing intervals based on applied load.

Vertical Loads	Location (Side)	Tributary Width	Dead (0.90)	Snow (1.15)	Comments
0 - Self Weight (PLF)	0 to 9' 1 1/2"	N/A	9.3	--	
1 - Uniform (PSF)	0 to 9' 1 1/2" (Front)	7'	17.0	150.0	Default Load

Weyerhaeuser Notes

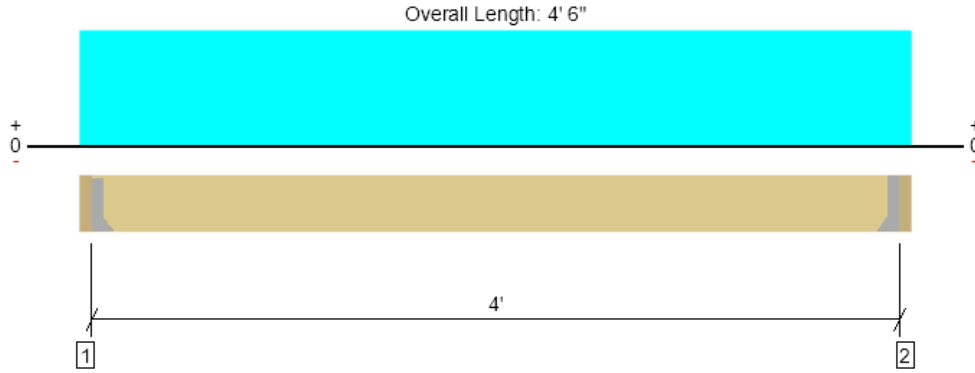
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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

ForteWEB Software Operator	Job Notes
Trevor Steelsmith Snake River Engineering (208) 453-6512 trevor@snakeriverengineering.com	



RESIDENCE, LADDER FRAMING
1 piece(s) 2 x 6 DF No.2 @ 16" OC



Drawing is Conceptual. All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	445 @ 3"	1406 (1.50")	Passed (32%)	--	1.0 D + 1.0 S (All Spans)
Shear (lbs)	343 @ 8 1/2"	1139	Passed (30%)	1.15	1.0 D + 1.0 S (All Spans)
Moment (Ft-lbs)	445 @ 2' 3"	975	Passed (46%)	1.15	1.0 D + 1.0 S (All Spans)
Live Load Defl. (in)	0.035 @ 2' 3"	0.200	Passed (L/999+)	--	1.0 D + 1.0 S (All Spans)
Total Load Defl. (in)	0.039 @ 2' 3"	0.267	Passed (L/999+)	--	1.0 D + 1.0 S (All Spans)

Member Length : 4'
System : Roof
Member Type : Joist
Building Use : Residential
Building Code : IBC 2018
Design Methodology : ASD
Member Pitch : 0/12

- Deflection criteria: LL (L/240) and TL (L/180).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- A 15% increase in the moment capacity has been added to account for repetitive member usage.
- Applicable calculations are based on NDS.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Snow	Factored	
1 - Hanger on 5 1/2" DF beam	3.00"	Hanger ¹	1.50"	51	450	501	See note ¹
2 - Hanger on 5 1/2" DF beam	3.00"	Hanger ¹	1.50"	51	450	501	See note ¹

- At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger
- ¹ See Connector grid below for additional information and/or requirements.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	4' o/c	
Bottom Edge (Lu)	4' o/c	

- Maximum allowable bracing intervals based on applied load.

Connector: Simpson Strong-Tie							
Support	Model	Seat Length	Top Fasteners	Face Fasteners	Member Fasteners	Accessories	
1 - Face Mount Hanger	LU26	1.50"	N/A	6-10dx1.5	4-10dx1.5		
2 - Face Mount Hanger	LU26	1.50"	N/A	6-10dx1.5	4-10dx1.5		

- Refer to manufacturer notes and instructions for proper installation and use of all connectors.

Vertical Load	Location (Side)	Spacing	Dead (0.90)	Snow (1.15)	Comments
1 - Uniform (PSF)	0 to 4' 6"	16"	17.0	150.0	Default Load

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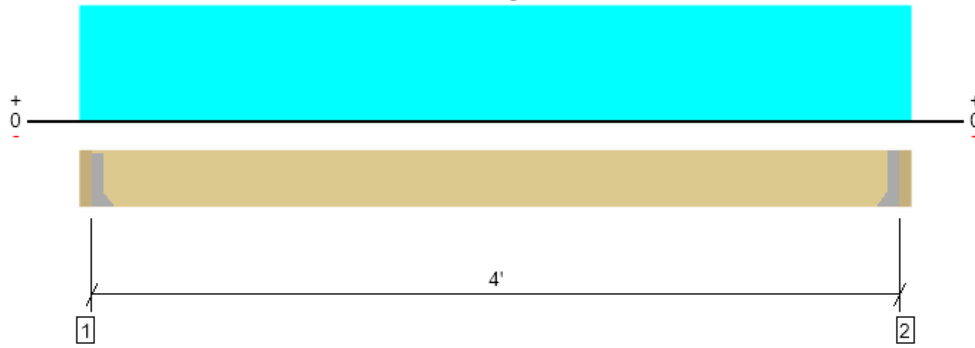
ForteWEB Software Operator	Job Notes
Trevor Steelsmith Snake River Engineering (208) 453-6512 trevor@snakeriverengineering.com	



RESIDENCE, FB1

2 piece(s) 1 3/4" x 11 7/8" 2.0E Microllam® LVL

Overall Length: 4' 6"



Drawing is Conceptual. All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	804 @ 3"	3938 (1.50")	Passed (20%)	--	1.0 D + 1.0 L (All Spans)
Shear (lbs)	406 @ 1' 2 7/8"	7897	Passed (5%)	1.00	1.0 D + 1.0 L (All Spans)
Moment (Ft-lbs)	804 @ 2' 3"	17848	Passed (5%)	1.00	1.0 D + 1.0 L (All Spans)
Live Load Defl. (in)	0.003 @ 2' 3"	0.100	Passed (L/999+)	--	1.0 D + 1.0 L (All Spans)
Total Load Defl. (in)	0.005 @ 2' 3"	0.200	Passed (L/999+)	--	1.0 D + 1.0 L (All Spans)

Member Length : 4'
 System : Floor
 Member Type : Drop Beam
 Building Use : Residential
 Building Code : IBC 2018
 Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Floor Live	Factored	
1 - Hanger on 11 7/8" DF beam	3.00"	Hanger ¹	1.50"	227	675	902	See note ¹
2 - Hanger on 11 7/8" DF beam	3.00"	Hanger ¹	1.50"	227	675	902	See note ¹

- At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger
- ¹ See Connector grid below for additional information and/or requirements.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	4' o/c	
Bottom Edge (Lu)	4' o/c	

- Maximum allowable bracing intervals based on applied load.

Connector: Simpson Strong-Tie							
Support	Model	Seat Length	Top Fasteners	Face Fasteners	Member Fasteners	Accessories	
1 - Face Mount Hanger	LUS410	2.00"	N/A	8-10dx1.5	6-10d		
2 - Face Mount Hanger	LUS410	2.00"	N/A	8-10dx1.5	6-10d		

- Refer to manufacturer notes and instructions for proper installation and use of all connectors.

Vertical Loads	Location (Side)	Tributary Width	Dead (0.90)	Floor Live (1.00)	Comments
0 - Self Weight (PLF)	3" to 4' 3"	N/A	12.1	--	
1 - Uniform (PSF)	0 to 4' 6" (Front)	7' 6"	12.0	40.0	Default Load

Weyerhaeuser Notes

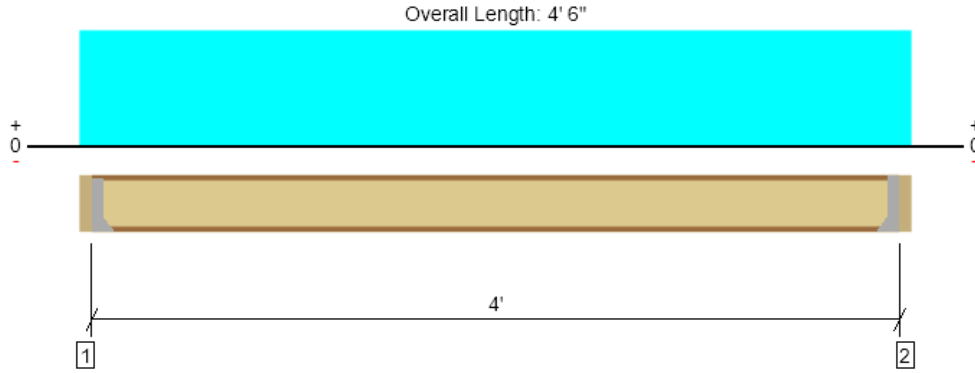
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ForteWEB Software Operator	Job Notes
Trevor Steelsmith Snake River Engineering (208) 453-6512 trevor@snakeriverengineering.com	



RESIDENCE, Floor: Joist UPPER
 1 piece(s) 11 7/8" TJI @ 110 @ 24" OC



Drawing is Conceptual. All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	208 @ 3"	910 (1.75")	Passed (23%)	1.00	1.0 D + 1.0 L (All Spans)
Shear (lbs)	208 @ 3"	1560	Passed (13%)	1.00	1.0 D + 1.0 L (All Spans)
Moment (Ft-lbs)	208 @ 2' 3"	3160	Passed (7%)	1.00	1.0 D + 1.0 L (All Spans)
Live Load Defl. (in)	0.004 @ 2' 3"	0.100	Passed (L/999+)	--	1.0 D + 1.0 L (All Spans)
Total Load Defl. (in)	0.005 @ 2' 3"	0.200	Passed (L/999+)	--	1.0 D + 1.0 L (All Spans)
TJ-Pro™ Rating	69	40	Passed	--	--

Member Length : 4'
 System : Floor
 Member Type : Joist
 Building Use : Residential
 Building Code : IBC 2018
 Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- A structural analysis of the deck has not been performed.
- Deflection analysis is based on composite action with a single layer of 23/32" Weyerhaeuser Edge™ Panel (24" Span Rating) that is glued and nailed down.
- Additional considerations for the TJ-Pro™ Rating include: None.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Floor Live	Factored	
1 - Hanger on 11 7/8" DF beam	3.00"	Hanger ¹	1.75" / - ²	54	180	234	See note ¹
2 - Hanger on 11 7/8" DF beam	3.00"	Hanger ¹	1.75" / - ²	54	180	234	See note ¹

• At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger

- ¹ See Connector grid below for additional information and/or requirements.
- ² Required Bearing Length / Required Bearing Length with Web Stiffeners

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	4' o/c	
Bottom Edge (Lu)	4' o/c	

- TJI joists are only analyzed using Maximum Allowable bracing solutions.
- Maximum allowable bracing intervals based on applied load.

Connector: Simpson Strong-Tie						
Support	Model	Seat Length	Top Fasteners	Face Fasteners	Member Fasteners	Accessories
1 - Face Mount Hanger	IUS1.81/11.88	2.00"	N/A	10-10dx1.5	2-Strong-Grip	
2 - Face Mount Hanger	IUS1.81/11.88	2.00"	N/A	10-10dx1.5	2-Strong-Grip	

- Refer to manufacturer notes and instructions for proper installation and use of all connectors.

Vertical Load	Location	Spacing	Dead (0.90)	Floor Live (1.00)	Comments
1 - Uniform (PSF)	0 to 4' 6"	24"	12.0	40.0	Default Load

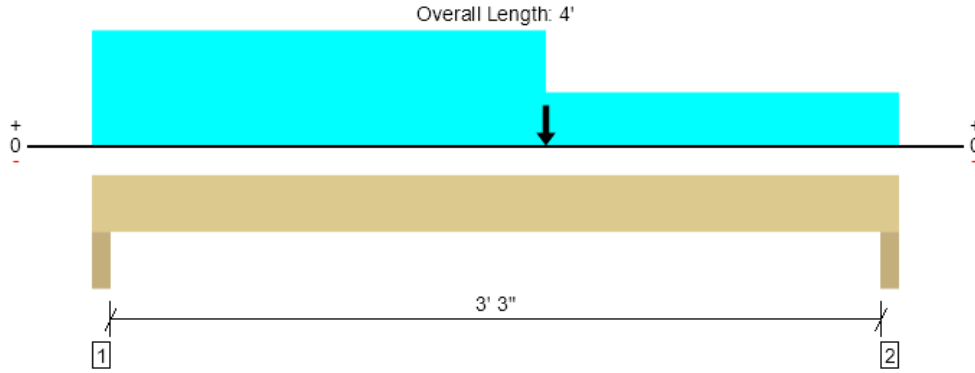
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ForteWEB Software Operator	Job Notes
Trevor Steelsmith 05/16/24 Snake River Engineering (208) 453-6512 trevor@snakeriverengineering.com	



RESIDENCE, HDR1

2 piece(s) 1 3/4" x 9 1/4" 2.0E Microllam® LVL



Drawing is Conceptual. All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	8096 @ 3"	11813 (4.50")	Passed (69%)	--	1.0 D + 1.0 S (All Spans)
Shear (lbs)	4230 @ 2' 10 1/4"	7074	Passed (60%)	1.15	1.0 D + 1.0 S (All Spans)
Moment (Ft-lbs)	6779 @ 2' 1 3/4"	12884	Passed (53%)	1.15	1.0 D + 1.0 S (All Spans)
Live Load Defl. (in)	0.049 @ 1' 11 3/4"	0.117	Passed (L/864)	--	1.0 D + 1.0 S (All Spans)
Total Load Defl. (in)	0.055 @ 1' 11 11/16"	0.175	Passed (L/765)	--	1.0 D + 1.0 S (All Spans)

Member Length : 4'
 System : Wall
 Member Type : Header
 Building Use : Residential
 Building Code : IBC 2018
 Design Methodology : ASD

- Deflection criteria: LL (L/360) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.

Supports	Bearing Length			Loads to Supports (lbs)				Accessories
	Total	Available	Required	Dead	Floor Live	Snow	Factored	
1 - Trimmer - DF	4.50"	4.50"	3.08"	977	688	7119	8096	None
2 - Trimmer - DF	4.50"	4.50"	2.44"	714	417	5679	6394	None

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	4' o/c	
Bottom Edge (Lu)	4' o/c	

•Maximum allowable bracing intervals based on applied load.

Vertical Loads	Location	Tributary Width	Dead (0.90)	Floor Live (1.00)	Snow (1.15)	Comments
0 - Self Weight (PLF)	0 to 4'	N/A	9.4	--	--	
1 - Uniform (PSF)	0 to 2' 3"	22'	17.0	-	150.0	Default Load
2 - Point (lb)	2' 3"	N/A	275	430	2420	
3 - Uniform (PSF)	2' 3" to 4'	11' 3"	17.0	-	150.0	Default Load
4 - Uniform (PSF)	0 to 2' 3"	7' 6"	12.0	40.0	-	Default Load

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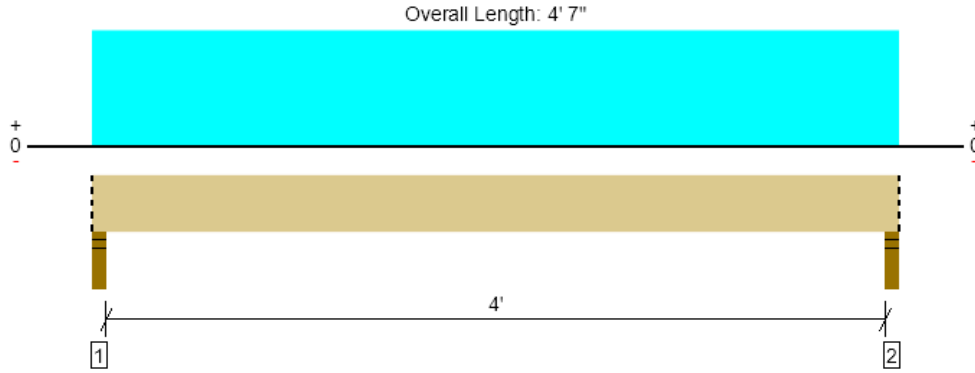
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ForteWEB Software Operator	Job Notes
Trevor Steelsmith Snake River Engineering (208) 453-6512 trevor@snakeriverengineering.com	



RESIDENCE, RB4

2 piece(s) 1 3/4" x 9 1/2" 2.0E Microllam® LVL



Drawing is Conceptual. All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	2318 @ 2"	7656 (3.50")	Passed (30%)	--	1.0 D + 1.0 S (All Spans)
Shear (lbs)	1222 @ 1' 1"	7265	Passed (17%)	1.15	1.0 D + 1.0 S (All Spans)
Moment (Ft-lbs)	2284 @ 2' 3 1/2"	13541	Passed (17%)	1.15	1.0 D + 1.0 S (All Spans)
Live Load Defl. (in)	0.020 @ 2' 3 1/2"	0.213	Passed (L/999+)	--	1.0 D + 1.0 S (All Spans)
Total Load Defl. (in)	0.023 @ 2' 3 1/2"	0.283	Passed (L/999+)	--	1.0 D + 1.0 S (All Spans)

Member Length : 4' 7"
 System : Roof
 Member Type : Drop Beam
 Building Use : Residential
 Building Code : IBC 2018
 Design Methodology : ASD
 Member Pitch : 0/12

- Deflection criteria: LL (L/240) and TL (L/180).
- Allowed moment does not reflect the adjustment for the beam stability factor.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Snow	Factored	
1 - Stud wall - DF	3.50"	3.50"	1.50"	256	2063	2318	Blocking
2 - Stud wall - DF	3.50"	3.50"	1.50"	256	2063	2318	Blocking

• Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	4' 7" o/c	
Bottom Edge (Lu)	4' 7" o/c	

•Maximum allowable bracing intervals based on applied load.

Vertical Loads	Location (Side)	Tributary Width	Dead (0.90)	Snow (1.15)	Comments
0 - Self Weight (PLF)	0 to 4' 7"	N/A	9.7	--	
1 - Uniform (PSF)	0 to 4' 7" (Front)	6'	17.0	150.0	Default Load

Weyerhaeuser Notes

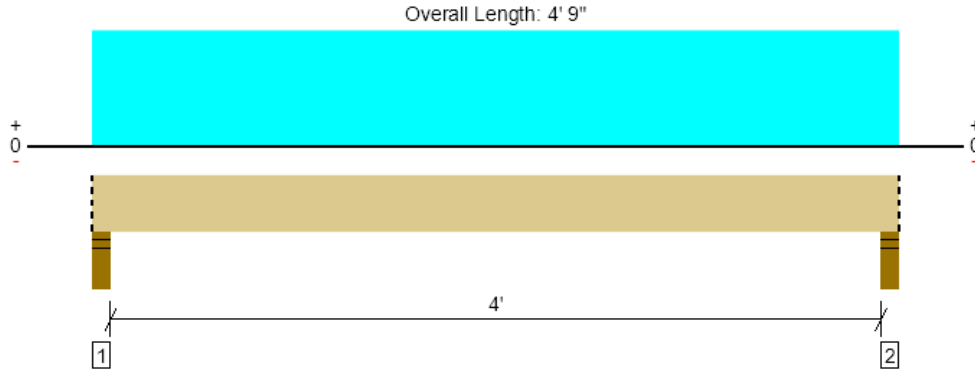
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ForteWEB Software Operator	Job Notes
Trevor Steelsmith Snake River Engineering (208) 453-6512 trevor@snakeriverengineering.com	



RESIDENCE, RB5
1 piece(s) 6 x 10 DF No.2



Drawing is Conceptual. All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	4196 @ 3"	15469 (4.50")	Passed (27%)	--	1.0 D + 1.0 S (All Spans)
Shear (lbs)	2135 @ 1' 2"	6810	Passed (31%)	1.15	1.0 D + 1.0 S (All Spans)
Moment (Ft-lbs)	3989 @ 2' 4 1/2"	6937	Passed (58%)	1.15	1.0 D + 1.0 S (All Spans)
Live Load Defl. (in)	0.023 @ 2' 4 1/2"	0.213	Passed (L/999+)	--	1.0 D + 1.0 S (All Spans)
Total Load Defl. (in)	0.025 @ 2' 4 1/2"	0.283	Passed (L/999+)	--	1.0 D + 1.0 S (All Spans)

Member Length : 4' 9"
System : Roof
Member Type : Drop Beam
Building Use : Residential
Building Code : IBC 2018
Design Methodology : ASD
Member Pitch : 0/12

- Deflection criteria: LL (L/240) and TL (L/180).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Lumber grading provisions must be extended over the length of the member per NDS 4.2.5.5.
- Applicable calculations are based on NDS.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Snow	Factored	
1 - Stud wall - DF	4.50"	4.50"	1.50"	455	3741	4196	Blocking
2 - Stud wall - DF	4.50"	4.50"	1.50"	455	3741	4196	Blocking

• Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	4' 9" o/c	
Bottom Edge (Lu)	4' 9" o/c	

•Maximum allowable bracing intervals based on applied load.

Vertical Loads	Location (Side)	Tributary Width	Dead (0.90)	Snow (1.15)	Comments
0 - Self Weight (PLF)	0 to 4' 9"	N/A	13.2	--	
1 - Uniform (PSF)	0 to 4' 9" (Front)	10' 6"	17.0	150.0	Default Load

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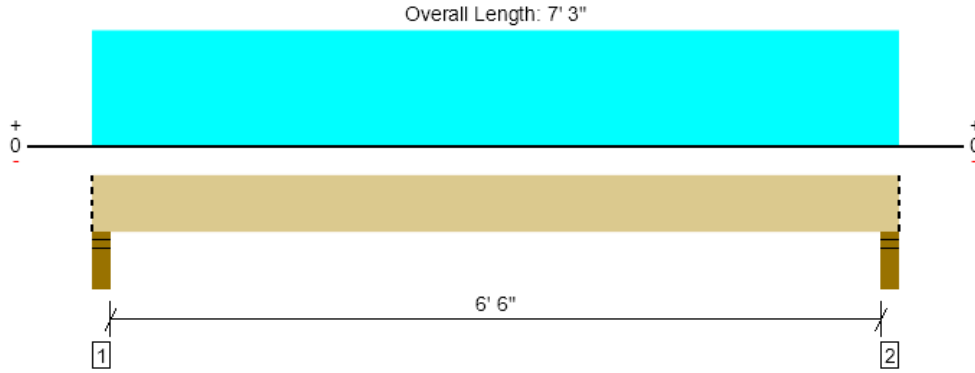
The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

ForteWEB Software Operator	Job Notes
Trevor Steelsmith Snake River Engineering (208) 453-6512 trevor@snakeriverengineering.com	



RESIDENCE, RB6

2 piece(s) 1 3/4" x 9 1/4" 2.0E Microllam® LVL



Drawing is Conceptual. All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	6391 @ 3"	9844 (4.50")	Passed (65%)	--	1.0 D + 1.0 S (All Spans)
Shear (lbs)	4371 @ 1' 1 3/4"	7074	Passed (62%)	1.15	1.0 D + 1.0 S (All Spans)
Moment (Ft-lbs)	10041 @ 3' 7 1/2"	12884	Passed (78%)	1.15	1.0 D + 1.0 S (All Spans)
Live Load Defl. (in)	0.191 @ 3' 7 1/2"	0.338	Passed (L/424)	--	1.0 D + 1.0 S (All Spans)
Total Load Defl. (in)	0.214 @ 3' 7 1/2"	0.450	Passed (L/378)	--	1.0 D + 1.0 S (All Spans)

Member Length : 7' 3"
 System : Roof
 Member Type : Drop Beam
 Building Use : Residential
 Building Code : IBC 2018
 Design Methodology : ASD
 Member Pitch : 0/12

- Deflection criteria: LL (L/240) and TL (L/180).
- Allowed moment does not reflect the adjustment for the beam stability factor.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Snow	Factored	
1 - Stud wall - DF	4.50"	4.50"	2.92"	681	5709	6391	Blocking
2 - Stud wall - DF	4.50"	4.50"	2.92"	681	5709	6391	Blocking

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	7' 3" o/c	
Bottom Edge (Lu)	7' 3" o/c	

- Maximum allowable bracing intervals based on applied load.

Vertical Loads	Location (Side)	Tributary Width	Dead (0.90)	Snow (1.15)	Comments
0 - Self Weight (PLF)	0 to 7' 3"	N/A	9.4	--	
1 - Uniform (PSF)	0 to 7' 3" (Front)	10' 6"	17.0	150.0	Default Load

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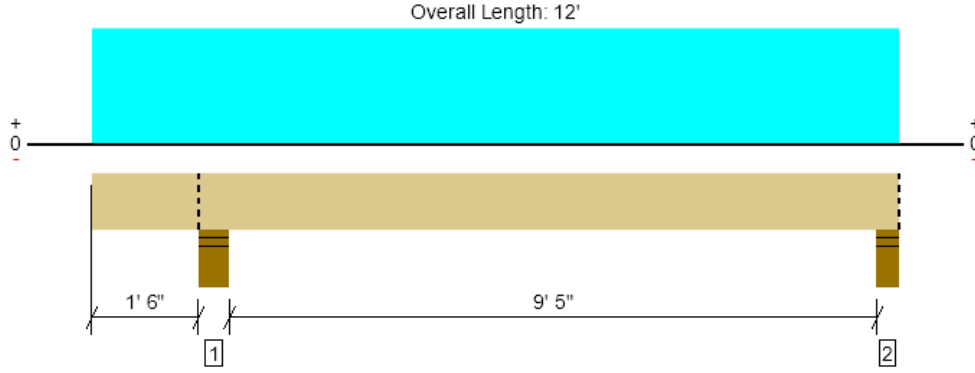
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ForteWEB Software Operator	Job Notes
Trevor Steelsmith Snake River Engineering (208) 453-6512 trevor@snakeriverengineering.com	



RESIDENCE, RB7

1 piece(s) 5 1/8" x 10 1/2" 24F-V4 DF Glulam



Drawing is Conceptual. All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	8698 @ 11' 8"	17617 (5.50")	Passed (49%)	--	1.0 D + 1.0 S (Alt Spans)
Shear (lbs)	6575 @ 3'	10933	Passed (60%)	1.15	1.0 D + 1.0 S (All Spans)
Pos Moment (Ft-lbs)	19670 @ 6' 10"	21660	Passed (91%)	1.15	1.0 D + 1.0 S (Alt Spans)
Neg Moment (Ft-lbs)	-2765 @ 1' 9 3/4"	16696	Passed (17%)	1.15	1.0 D + 1.0 S (All Spans)
Live Load Defl. (in)	0.343 @ 6' 9 1/4"	0.493	Passed (L/345)	--	1.0 D + 1.0 S (Alt Spans)
Total Load Defl. (in)	0.383 @ 6' 9 1/4"	0.657	Passed (L/309)	--	1.0 D + 1.0 S (Alt Spans)

Member Length : 12'
 System : Roof
 Member Type : Drop Beam
 Building Use : Residential
 Building Code : IBC 2018
 Design Methodology : ASD
 Member Pitch : 0/12

- Deflection criteria: LL (L/240) and TL (L/180).
- Overhang deflection criteria: LL (2L/240) and TL (2L/180).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Critical positive moment adjusted by a volume/size factor of 1.00 that was calculated using length L = 9' 8 1/16".
- Critical negative moment adjusted by a volume/size factor of 1.00 that was calculated using length L = 2' 1 3/4".
- The effects of positive or negative camber have not been accounted for when calculating deflection.
- The specified glulam is assumed to have its strong laminations at the bottom of the beam. Install with proper side up as indicated by the manufacturer.
- Applicable calculations are based on NDS.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Snow	Factored	
1 - Stud wall - DF	7.50"	7.50"	3.63"	1264	10359	11624	Blocking
2 - Stud wall - DF	5.50"	5.50"	2.72"	933	7766	8698	Blocking

• Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	12' o/c	
Bottom Edge (Lu)	12' o/c	

•Maximum allowable bracing intervals based on applied load.

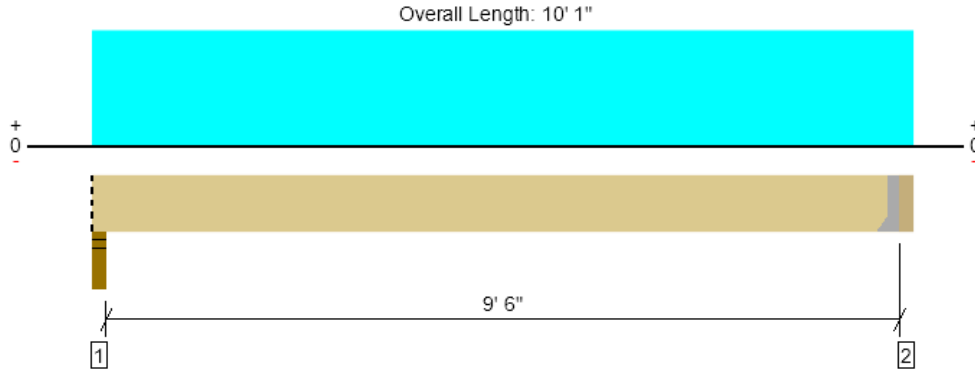
Vertical Loads	Location (Side)	Tributary Width	Dead (0.90)	Snow (1.15)	Comments
0 - Self Weight (PLF)	0 to 12'	N/A	13.1	--	
1 - Uniform (PSF)	0 to 12' (Front)	10'	17.0	150.0	Default Load

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ForteWEB Software Operator	Job Notes
Trevor Steelsmith Snake River Engineering (208) 453-6512 trevor@snakeriverengineering.com	



RESIDENCE, FB2
1 piece(s) 6 x 10 DF No.2



Drawing is Conceptual. All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	1738 @ 9' 9 1/2"	5156 (1.50")	Passed (34%)	--	1.0 D + 1.0 S (All Spans)
Shear (lbs)	1452 @ 9'	6810	Passed (21%)	1.15	1.0 D + 1.0 S (All Spans)
Moment (Ft-lbs)	4183 @ 4' 11 3/4"	6937	Passed (60%)	1.15	1.0 D + 1.0 S (All Spans)
Live Load Defl. (in)	0.113 @ 4' 11 3/4"	0.241	Passed (L/999+)	--	1.0 D + 1.0 S (All Spans)
Total Load Defl. (in)	0.137 @ 4' 11 3/4"	0.481	Passed (L/846)	--	1.0 D + 1.0 S (All Spans)

Member Length : 9' 9 1/2"
System : Floor
Member Type : Drop Beam
Building Use : Residential
Building Code : IBC 2018
Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Lumber grading provisions must be extended over the length of the member per NDS 4.2.5.5.
- Applicable calculations are based on NDS.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Snow	Factored	
1 - Stud wall - DF	3.50"	3.50"	1.50"	305	1494	1799	Blocking
2 - Hanger on 9 1/2" DF beam	3.50"	Hanger ¹	1.50"	309	1531	1840	See note ¹

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.
- At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger
- ¹ See Connector grid below for additional information and/or requirements.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	9' 10" o/c	
Bottom Edge (Lu)	9' 10" o/c	

- Maximum allowable bracing intervals based on applied load.

Connector: Simpson Strong-Tie							
Support	Model	Seat Length	Top Fasteners	Face Fasteners	Member Fasteners	Accessories	
2 - Face Mount Hanger	HU68	2.50"	N/A	14-10d	6-10d		

- Refer to manufacturer notes and instructions for proper installation and use of all connectors.

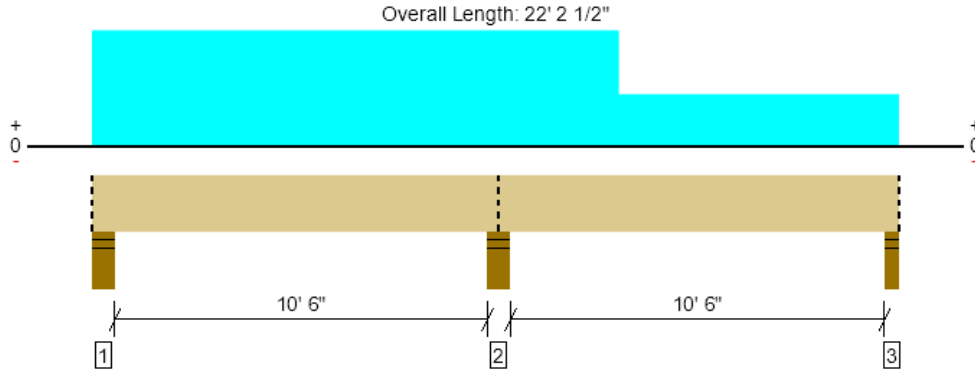
Vertical Loads	Location (Side)	Tributary Width	Dead (0.90)	Snow (1.15)	Comments
0 - Self Weight (PLF)	0 to 9' 9 1/2"	N/A	13.2	--	
1 - Uniform (PSF)	0 to 10' 1" (Front)	4'	12.0	75.0	Default Load

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ForteWEB Software Operator	Job Notes
Trevor Steelsmith Snake River Engineering (208) 453-6512 trevor@snakeriverengineering.com	



RESIDENCE, FB3
1 piece(s) 6 x 12 DF No.2



Drawing is Conceptual. All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	7262 @ 11' 2 1/4"	12856 (5.50")	Passed (56%)	--	1.0 D + 1.0 S (All Spans)
Shear (lbs)	3330 @ 10'	8244	Passed (40%)	1.15	1.0 D + 1.0 S (All Spans)
Moment (Ft-lbs)	-7386 @ 11' 2 1/4"	10166	Passed (73%)	1.15	1.0 D + 1.0 S (All Spans)
Live Load Defl. (in)	0.111 @ 5' 4 1/16"	0.271	Passed (L/999+)	--	1.0 D + 1.0 S (Alt Spans)
Total Load Defl. (in)	0.129 @ 5' 3 3/4"	0.543	Passed (L/999+)	--	1.0 D + 1.0 S (Alt Spans)

Member Length : 22' 2 1/2"
System : Floor
Member Type : Drop Beam
Building Use : Residential
Building Code : IBC 2018
Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Lumber grading provisions must be extended over the length of the member per NDS 4.2.5.5.
- Applicable calculations are based on NDS.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Snow	Factored	
1 - Stud wall - DF	5.50"	5.50"	1.50"	464	2562	3026	Blocking
2 - Stud wall - SPF	5.50"	5.50"	3.11"	1189	6073	7262	Blocking
3 - Stud wall - DF	3.50"	3.50"	1.50"	210	1068	1278	Blocking

• Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	22' 3" o/c	
Bottom Edge (Lu)	22' 3" o/c	

•Maximum allowable bracing intervals based on applied load.

Vertical Loads	Location (Side)	Tributary Width	Dead (0.90)	Snow (1.15)	Comments
0 - Self Weight (PLF)	0 to 22' 2 1/2"	N/A	16.0	--	
1 - Uniform (PSF)	0 to 14' 6" (Front)	7'	12.0	75.0	Default Load
2 - Uniform (PSF)	14' 6" to 22' 2 1/2" (Front)	3' 1 1/2"	12.0	75.0	Default Load

Weyerhaeuser Notes

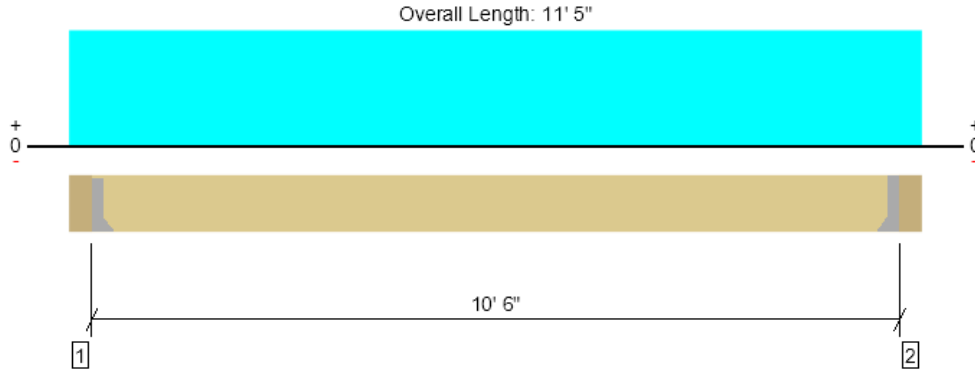
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ForteWEB Software Operator	Job Notes
Trevor Steelsmith Snake River Engineering (208) 453-6512 trevor@snakeriverengineering.com	



RESIDENCE, FB4
1 piece(s) 6 x 10 DF No.2



Drawing is Conceptual. All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	2011 @ 5' 1/2"	5156 (1.50")	Passed (39%)	--	1.0 D + 1.0 S (All Spans)
Shear (lbs)	1707 @ 1' 3"	6810	Passed (25%)	1.15	1.0 D + 1.0 S (All Spans)
Moment (Ft-lbs)	5278 @ 5' 8 1/2"	6937	Passed (76%)	1.15	1.0 D + 1.0 S (All Spans)
Live Load Defl. (in)	0.171 @ 5' 8 1/2"	0.262	Passed (L/738)	--	1.0 D + 1.0 S (All Spans)
Total Load Defl. (in)	0.205 @ 5' 8 1/2"	0.525	Passed (L/615)	--	1.0 D + 1.0 S (All Spans)

Member Length : 10' 6"
System : Floor
Member Type : Drop Beam
Building Use : Residential
Building Code : IBC 2018
Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Lumber grading provisions must be extended over the length of the member per NDS 4.2.5.5.
- Applicable calculations are based on NDS.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Snow	Factored	
1 - Hanger on 9 1/2" DF beam	5.50"	Hanger ¹	1.50"	361	1820	2180	See note ¹
2 - Hanger on 9 1/2" DF beam	5.50"	Hanger ¹	1.50"	361	1820	2180	See note ¹

- At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger
- ¹ See Connector grid below for additional information and/or requirements.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	10' 6" o/c	
Bottom Edge (Lu)	10' 6" o/c	

- Maximum allowable bracing intervals based on applied load.

Connector: Simpson Strong-Tie							
Support	Model	Seat Length	Top Fasteners	Face Fasteners	Member Fasteners	Accessories	
1 - Face Mount Hanger	HU610	2.50"	N/A	18-10dx1.5	8-10d		
2 - Face Mount Hanger	HU68	2.50"	N/A	14-16d	6-16d		

- Refer to manufacturer notes and instructions for proper installation and use of all connectors.

Vertical Loads	Location (Side)	Tributary Width	Dead (0.90)	Snow (1.15)	Comments
0 - Self Weight (PLF)	5 1/2" to 10' 11 1/2"	N/A	13.2	--	
1 - Uniform (PSF)	0 to 11' 5" (Front)	4' 3"	12.0	75.0	Default Load

Weyerhaeuser Notes

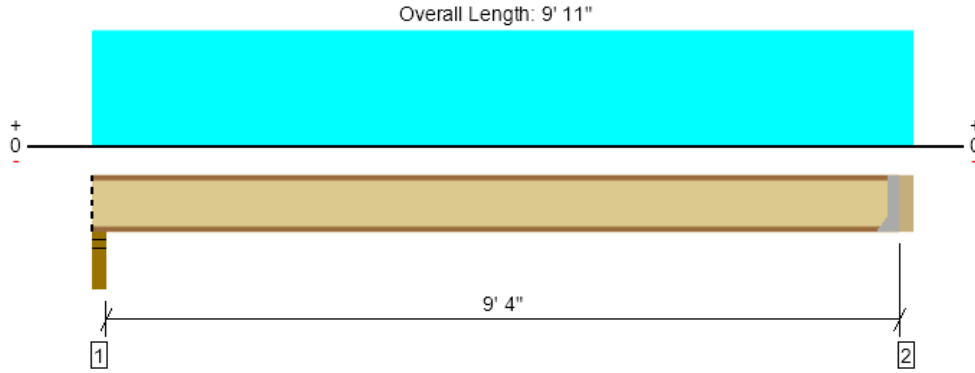
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ForteWEB Software Operator	Job Notes
Trevor Steelsmith Snake River Engineering (208) 453-6512 trevor@snakeriverengineering.com	



RESIDENCE, Floor: Joist MAIN
1 piece(s) 9 1/2" TJI® 110 @ 24" OC



Drawing is Conceptual. All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	490 @ 9' 7 1/2"	910 (1.75")	Passed (54%)	1.00	1.0 D + 1.0 L (All Spans)
Shear (lbs)	490 @ 9' 7 1/2"	1220	Passed (40%)	1.00	1.0 D + 1.0 L (All Spans)
Moment (Ft-lbs)	1153 @ 4' 11"	2500	Passed (46%)	1.00	1.0 D + 1.0 L (All Spans)
Live Load Defl. (in)	0.086 @ 4' 11"	0.235	Passed (L/999+)	--	1.0 D + 1.0 L (All Spans)
Total Load Defl. (in)	0.112 @ 4' 11"	0.471	Passed (L/999+)	--	1.0 D + 1.0 L (All Spans)
TJ-Pro™ Rating	47	40	Passed	--	--

Member Length : 9' 7 1/2"
System : Floor
Member Type : Joist
Building Use : Residential
Building Code : IBC 2018
Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- A structural analysis of the deck has not been performed.
- Deflection analysis is based on composite action with a single layer of 23/32" Weyerhaeuser Edge™ Panel (24" Span Rating) that is glued and nailed down.
- Additional considerations for the TJ-Pro™ Rating include: None.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Floor Live	Factored	
1 - Stud wall - DF	3.50"	3.50"	1.75"	118	393	511	Blocking
2 - Hanger on 9 1/2" DF beam	3.50"	Hanger ¹	1.75" / - ²	120	400	520	See note ¹

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.
- At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger
- ¹ See Connector grid below for additional information and/or requirements.
- ² Required Bearing Length / Required Bearing Length with Web Stiffeners

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	4' 8" o/c	
Bottom Edge (Lu)	9' 8" o/c	

- TJI joists are only analyzed using Maximum Allowable bracing solutions.
- Maximum allowable bracing intervals based on applied load.

Connector: Simpson Strong-Tie

Support	Model	Seat Length	Top Fasteners	Face Fasteners	Member Fasteners	Accessories
2 - Face Mount Hanger	IUS1.81/9.5	2.00"	N/A	8-10dx1.5	2-Strong-Grip	

- Refer to manufacturer notes and instructions for proper installation and use of all connectors.

Vertical Load	Location	Spacing	Dead (0.90)	Floor Live (1.00)	Comments
1 - Uniform (PSF)	0 to 9' 11"	24"	12.0	40.0	Default Load

Weyerhaeuser Notes

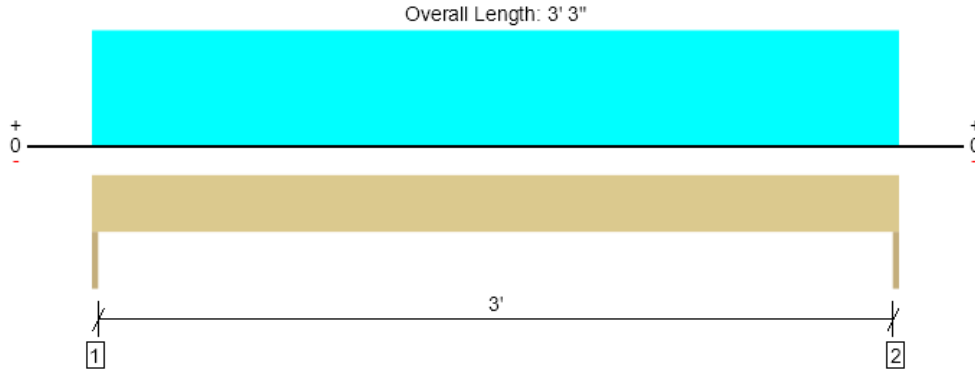
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ForteWEB Software Operator	Job Notes
Trevor Steelsmith 05/16/24 Snake River Engineering (208) 453-6512 trevor@snakeriverengineering.com	



RESIDENCE, CRAWL HDR
1 piece(s) 4 x 10 DF No.2



Drawing is Conceptual. All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	802 @ 0	3281 (1.50")	Passed (24%)	--	1.0 D + 1.0 L (All Spans)
Shear (lbs)	360 @ 10 3/4"	3885	Passed (9%)	1.00	1.0 D + 1.0 L (All Spans)
Moment (Ft-lbs)	652 @ 1' 7 1/2"	4492	Passed (15%)	1.00	1.0 D + 1.0 L (All Spans)
Live Load Defl. (in)	0.003 @ 1' 7 1/2"	0.108	Passed (L/999+)	--	1.0 D + 1.0 L (All Spans)
Total Load Defl. (in)	0.003 @ 1' 7 1/2"	0.162	Passed (L/999+)	--	1.0 D + 1.0 L (All Spans)

Member Length : 3' 3"
System : Wall
Member Type : Header
Building Use : Residential
Building Code : IBC 2018
Design Methodology : ASD

- Deflection criteria: LL (L/360) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Applicable calculations are based on NDS.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Floor Live	Factored	
1 - Trimmer - DF	1.50"	1.50"	1.50"	195	607	802	None
2 - Trimmer - DF	1.50"	1.50"	1.50"	195	607	802	None

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	3' 3" o/c	
Bottom Edge (Lu)	3' 3" o/c	

•Maximum allowable bracing intervals based on applied load.

Vertical Loads	Location	Tributary Width	Dead (0.90)	Floor Live (1.00)	Comments
0 - Self Weight (PLF)	0 to 3' 3"	N/A	8.2	--	
1 - Uniform (PSF)	0 to 3' 3"	9' 4"	12.0	40.0	Default Load

Weyerhaeuser Notes

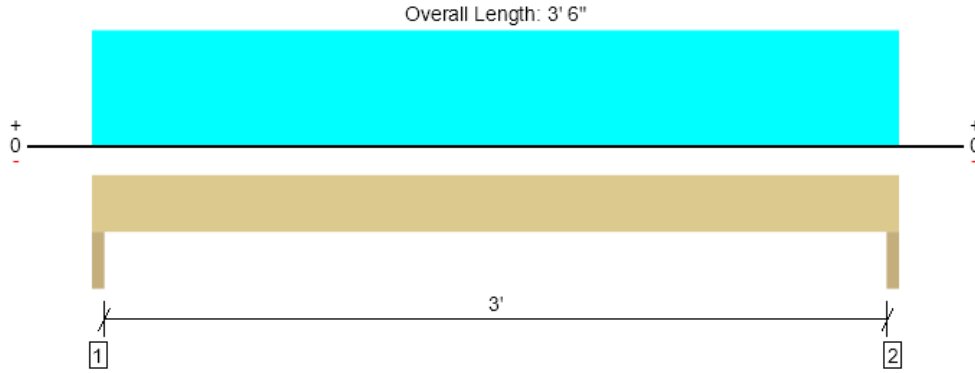
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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

ForteWEB Software Operator	Job Notes
Trevor Steelsmith Snake River Engineering (208) 453-6512 trevor@snakeriverengineering.com	



RESIDENCE, CRAWL HDR BRG. WALL
1 piece(s) 4 x 10 DF No.2



Drawing is Conceptual. All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	4302 @ 1' 1/2"	6563 (3.00")	Passed (66%)	--	1.0 D + 1.0 S (All Spans)
Shear (lbs)	1792 @ 1' 1/4"	4468	Passed (40%)	1.15	1.0 D + 1.0 S (All Spans)
Moment (Ft-lbs)	3246 @ 1' 9"	5166	Passed (63%)	1.15	1.0 D + 1.0 S (All Spans)
Live Load Defl. (in)	0.014 @ 1' 9"	0.108	Passed (L/999+)	--	1.0 D + 1.0 S (All Spans)
Total Load Defl. (in)	0.017 @ 1' 9"	0.162	Passed (L/999+)	--	1.0 D + 1.0 S (All Spans)

Member Length : 3' 6"
System : Wall
Member Type : Header
Building Use : Residential
Building Code : IBC 2018
Design Methodology : ASD

- Deflection criteria: LL (L/360) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Applicable calculations are based on NDS.

Supports	Bearing Length			Loads to Supports (lbs)				Accessories
	Total	Available	Required	Dead	Floor Live	Snow	Factored	
1 - Trimmer - DF	3.00"	3.00"	1.97"	627	653	3675	4302	None
2 - Trimmer - DF	3.00"	3.00"	1.97"	627	653	3675	4302	None

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	3' 6" o/c	
Bottom Edge (Lu)	3' 6" o/c	

•Maximum allowable bracing intervals based on applied load.

Vertical Loads	Location	Tributary Width	Dead (0.90)	Floor Live (1.00)	Snow (1.15)	Comments
0 - Self Weight (PLF)	0 to 3' 6"	N/A	8.2	--	--	
1 - Uniform (PSF)	0 to 3' 6"	9' 4"	12.0	40.0	-	Default Load
2 - Uniform (PSF)	0 to 3' 6"	14'	17.0	-	150.0	Default Load

Weyerhaeuser Notes

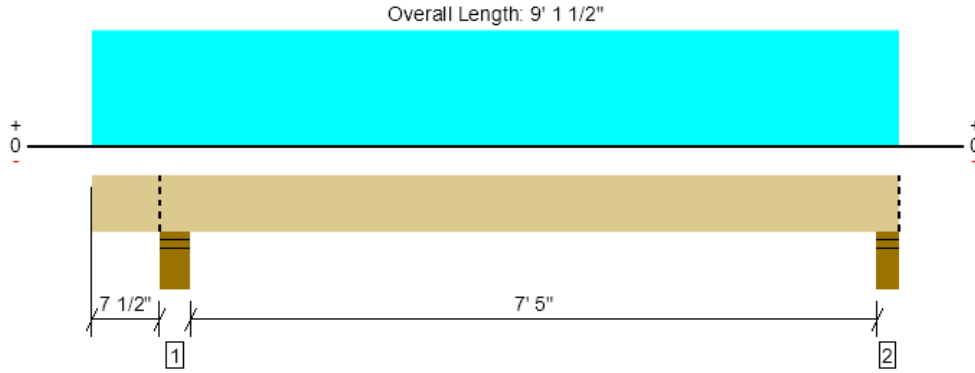
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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

ForteWEB Software Operator	Job Notes
Trevor Steelsmith Snake River Engineering (208) 453-6512 trevor@snakeriverengineering.com	



RESIDENCE, RB3 DF
1 piece(s) 6 x 12 DF No.2



Drawing is Conceptual. All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	5012 @ 8' 9 1/2"	18906 (5.50")	Passed (27%)	--	1.0 D + 1.0 S (Alt Spans)
Shear (lbs)	3333 @ 7' 8 1/2"	8244	Passed (40%)	1.15	1.0 D + 1.0 S (Alt Spans)
Moment (Ft-lbs)	8993 @ 4' 10 3/4"	10166	Passed (88%)	1.15	1.0 D + 1.0 S (Alt Spans)
Live Load Defl. (in)	0.098 @ 4' 10 1/2"	0.393	Passed (L/967)	--	1.0 D + 1.0 S (Alt Spans)
Total Load Defl. (in)	0.110 @ 4' 10 1/2"	0.524	Passed (L/858)	--	1.0 D + 1.0 S (Alt Spans)

Member Length : 9' 1 1/2"
System : Roof
Member Type : Drop Beam
Building Use : Residential
Building Code : IBC 2018
Design Methodology : ASD
Member Pitch : 0/12

- Deflection criteria: LL (L/240) and TL (L/180).
- Overhang deflection criteria: LL (2L/240) and TL (2L/180).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Lumber grading provisions must be extended over the length of the member per NDS 4.2.5.5.
- Applicable calculations are based on NDS.

Supports	Bearing Length			Loads to Supports (lbs)			Accessories
	Total	Available	Required	Dead	Snow	Factored	
1 - Stud wall - DF	7.50"	7.50"	1.70"	664	5167	5831	Blocking
2 - Stud wall - DF	5.50"	5.50"	1.50"	568	4444	5012	Blocking

• Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	9' 2" o/c	
Bottom Edge (Lu)	9' 2" o/c	

•Maximum allowable bracing intervals based on applied load.

Vertical Loads	Location (Side)	Tributary Width	Dead (0.90)	Snow (1.15)	Comments
0 - Self Weight (PLF)	0 to 9' 1 1/2"	N/A	16.0	--	
1 - Uniform (PSF)	0 to 9' 1 1/2" (Front)	7'	17.0	150.0	Default Load

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ForteWEB Software Operator	Job Notes
Trevor Steelsmith Snake River Engineering (208) 453-6512 trevor@snakeriverengineering.com	



WOOD HEADER ALLOWABLE LOADS (kips/ft)

Load Duration Factor: 1.15
LVL Grade: 2.0E

Top Chord Bracing: 2'-0" O.C.
Max TL Deflection: L/240, 0.75in
Repetitive Stress Increase: No

Header Type	Header Span										
	2'	3'	4'	5'	6'	8'	10'	12'	14'	16'	18'
(2) 2x4 DF Stud	1.15	0.69	0.29	0.22	0.12	NA	NA	NA	NA	NA	NA
(3) 2x4 DF Stud	1.84	1.04	0.46	0.35	0.18	NA	NA	NA	NA	NA	NA
(2) 2x6 DF #2	3.34	1.44	0.83	0.48	0.36	0.20	0.12	NA	NA	NA	NA
(3) 2x6 DF #2	5.06	2.19	1.27	0.72	0.55	0.30	0.18	0.13	NA	NA	NA
(2) 2x8 DF #2	5.41	2.30	1.27	0.80	0.59	0.32	0.20	0.14	0.09	NA	NA
(3) 2x8 DF #2	8.74	3.39	2.19	1.18	0.97	0.53	0.33	0.23	0.16	0.12	NA
(2) 2x10 DF #2	8.05	3.39	1.96	1.18	0.89	0.48	0.31	0.21	0.15	0.10	NA
(3) 2x10 DF #2	13.23	5.18	3.22	1.80	1.38	0.82	0.52	0.36	0.25	0.20	0.15
(2) 2x12 DF #2	10.81	4.83	2.65	1.60	1.15	0.67	0.41	0.29	0.21	0.15	0.12
(3) 2x12 DF #2	17.94	7.02	4.49	2.40	1.96	1.10	0.70	0.48	0.35	0.26	0.21
(2) 1-3/4x7-1/4 LVL	13.80	6.79	3.80	2.40	1.61	0.94	0.52	0.30	0.18	0.12	NA
(3) 1-3/4x7-1/4 LVL	20.70	10.47	5.64	3.50	2.53	1.38	0.79	0.45	0.28	0.17	NA
(2) 1-3/4x9-1/2 LVL	24.73	10.47	5.64	3.75	2.65	1.50	0.92	0.63	0.39	0.24	0.15
(3) 1-3/4x9-1/2 LVL	37.15	17.25	8.51	6.00	4.03	2.30	1.38	0.95	0.60	0.37	0.22
(2) 1-3/4x11-7/8 LVL	40.71	17.25	8.86	6.00	4.49	2.53	1.61	1.12	0.82	0.53	0.32
(3) 1-3/4x11-7/8 LVL	61.30	24.15	13.23	8.75	6.67	3.80	2.42	1.61	1.15	0.79	0.48
(2) 1-3/4x14 LVL	56.47	24.15	12.54	8.00	5.75	3.45	2.19	1.50	1.13	0.86	0.54
(3) 1-3/4x14 LVL	85.10	28.75	18.86	12.00	8.63	5.29	3.34	2.30	1.61	1.27	0.81

Header Calculations (H10)

	Additional Drift	Roof	Floor	Deck	Wall	Total Load	Total Load
Trib	0.0	10	0	0	2.83		1,704.0 plf
Dead Load	-	170.0	0.0	0.0	34.0	204.0 plf	
Live / Snow Load	0	1500.0	0.0	0.0	-	1,500.0 plf	

Description:	3.0 ft Opening						
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Header Callout	(2)2x8 DF-L No. 2						
Trimmers	(1) 2x6 DF-L No. 2						
King Studs	(1) 2x6 DF-L No. 2						

Wood Design							
Species	DF-L						
Grade	No. 2						
Width	3.00 in						
Depth	7.25 in						

Reaction							
Dead Load	306 lbs						
Live Load	2,250 lbs						

Load							
l _u	3.0 ft						
l _e	6.2 ft						

Adjustment Factors							
C _d	1.15						
C _F	1.2						

Material Properties							
F _b	900 psi						
F _v	180 psi						
E	1,600,000 psi						
E _{min}	580,000 psi						

Calculated Prop.							
A	21.75 in ²						
I	95.27 in ⁴						
S	26.28 in ³						
RB	7.73						
E _{min'}	580,000 psi						
F _{bE}	11,650 psi						
F _{b*}	1,242 psi						
C _L	1						

Shear and Moment							
M	23,003 lb-in						
V	2,556 lbs						

Stress							
fb	875 psi						
Fb'	1,235 psi						
fb/Fb'	0.71						
fv	176 psi						
Fv'	207 psi						
fv/Fv'	0.85						
Max Ratio	0.85						
	Pass						

Deflection							
Δ _{T_L}	0.02 in						
	L/1,767						
Δ _{L_L}	0.02 in						
	L/2,007						
	Pass						

Header Calculations (H9)

	Additional Drift	Roof	Floor	Deck	Wall	Total Load	Total Load
Trib	0.0	11	0	0	2.83		1,871.0 plf
Dead Load	-	187.0	0.0	0.0	34.0	221.0 plf	
Live / Snow Load	0	1650.0	0.0	0.0	-	1,650.0 plf	

Description:	2.3 ft Opening						
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Header Callout	(2)2x6 DF-L No. 2						
Trimmers	(1) 2x6 DF-L No. 2						
King Studs	(1) 2x6 DF-L No. 2						

Wood Design							
Species	DF-L						
Grade	No. 2						
Width	3.00 in						
Depth	5.50 in						

Reaction							
Dead Load	257 lbs						
Live Load	1,922 lbs						

Load							
l _u	2.3 ft						
l _e	4.8 ft						

Adjustment Factors							
C _d	1.15						
C _F	1.3						

Material Properties							
F _b	900 psi						
F _v	180 psi						
E	1,600,000 psi						
E _{min}	580,000 psi						

Calculated Prop.							
A	16.50 in ²						
I	41.59 in ⁴						
S	15.13 in ³						
RB	5.93						
E _{min'}	580,000 psi						
F _{bE}	19,774 psi						
F _{b*}	1,346 psi						
C _L	1						

Shear and Moment							
M	15,236 lb-in						
V	2,180 lbs						

Stress							
f _b	1,007 psi						
F _{b'}	1,341 psi						
f _b /F _{b'}	0.75						
f _v	198 psi						
F _{v'}	207 psi						
f _v /F _{v'}	0.96						
Max Ratio	0.96						
	Pass						

Deflection							
Δ _{T_L}	0.02 in						
	L/1,500						
Δ _{LL}	0.02 in						
	L/1,701						
	Pass						

Header Calculations (H8)

	Additional Drift	Roof	Floor	Deck	Wall	Total Load	Total Load
Trib	0.0	19	7.5	0	2.83		3,597.0 plf
Dead Load	-	323.0	90.0	0.0	34.0	447.0 plf	
Live / Snow Load	0	2850.0	300.0	0.0	-	3,150.0 plf	

Description:	3.3 ft Opening							
Header Callout	(2)9.5 LVL 2.0E							
Trimmers	(2) 2x6 DF-L No. 2							
King Studs	(1) 2x6 DF-L No. 2							

Wood Design								
Species	LVL							
Grade	2.0E							
Width	3.50 in							
Depth	9.50 in							

Reaction								
Dead Load	726 lbs							
Live Load	5,119 lbs							

Load								
lu	3.3 ft							
le	6.7 ft							

Adjustment Factors								
Cd	1.15							
CF	1.1							

Material Properties								
Fb	2,900 psi							
Fv	285 psi							
E	2,000,000 psi							
Emin	1,016,535 psi							

Calculated Prop.								
A	33.25 in ²							
I	250.07 in ⁴							
S	52.65 in ³							
RB	7.89							
Emin'	1,016,535 psi							
FbE	19,579 psi							
Fb*	3,669 psi							
CL	1							

Shear and Moment								
M	56,989 lb-in							
V	5,845 lbs							

Stress								
fb	1,083 psi							
Fb'	3,627 psi							
fb/Fb'	0.30							
fv	264 psi							
Fv'	328 psi							
fv/Fv'	0.80							
Max Ratio	0.80							
	Pass							

Deflection								
ΔTL	0.02 in							
	L/2,160							
ΔLL	0.02 in							
	L/2,467							
	Pass							

Header Calculations (H7)

	Additional Drift	Roof	Floor	Deck	Wall	Total Load	Total Load
Trib	0.0	2.5	1	0	2.83		503.5 plf
Dead Load	-	42.5	12.0	0.0	34.0	88.5 plf	
Live / Snow Load	0	375.0	40.0	0.0	-	415.0 plf	

Description:	10.0 ft Opening						
Header Callout	(2)9.5 LVL 2.0E						
Trimmers	(1) 2x6 DF-L No. 2						
King Studs	(2) 2x6 DF-L No. 2						

Wood Design							
Species	LVL						
Grade	2.0E						
Width	3.50 in						
Depth	9.50 in						

Reaction							
Dead Load	442 lbs						
Live Load	2,075 lbs						

Load							
l _u	10.0 ft						
l _e	18.7 ft						

Adjustment Factors							
C _d	1.15						
C _F	1.1						

Material Properties							
F _b	2,900 psi						
F _v	285 psi						
E	2,000,000 psi						
E _{min}	1,016,535 psi						

Calculated Prop.							
A	33.25 in ²						
I	250.07 in ⁴						
S	52.65 in ³						
RB	13.18						
E _{min} '	1,016,535 psi						
F _{bE}	7,019 psi						
F _b *	3,669 psi						
C _L	1						

Shear and Moment							
M	75,519 lb-in						
V	2,517 lbs						

Stress							
f _b	1,434 psi						
F _b '	3,495 psi						
f _b /F _b '	0.41						
f _v	114 psi						
F _v '	328 psi						
f _v /F _v '	0.35						
Max Ratio	0.41						
	Pass						

Deflection							
Δ _{T_L}	0.23 in						
	L/530						
Δ _{L_L}	0.19 in						
	L/643						
	Pass						

Header Calculations (H6)

	Additional Drift	Roof	Floor	Deck	Wall	Total Load	Total Load
Trib	0.0	16	7.335	0	2.83		3,087.4 plf
Dead Load	-	272.0	88.0	0.0	34.0	394.0 plf	
Live / Snow Load	0	2400.0	293.4	0.0	-	2,693.4 plf	

Description:	3.0 ft Opening						
Header Callout	(2)9.5 LVL 2.0E						
Trimmers	(2) 2x6 DF-L No. 2						
King Studs	(1) 2x6 DF-L No. 2						

Wood Design							
Species	LVL						
Grade	2.0E						
Width	3.50 in						
Depth	9.50 in						

Reaction							
Dead Load	591 lbs						
Live Load	4,040 lbs						

Load							
l _u	3.0 ft						
l _e	6.2 ft						

Adjustment Factors							
C _d	1.15						
CF	1.1						

Material Properties							
F _b	2,900 psi						
F _v	285 psi						
E	2,000,000 psi						
E _{min}	1,016,535 psi						

Calculated Prop.							
A	33.25 in ²						
I	250.07 in ⁴						
S	52.65 in ³						
RB	7.58						
E _{min'}	1,016,535 psi						
F _{bE}	21,210 psi						
F _{b*}	3,669 psi						
CL	1						

Shear and Moment							
M	41,680 lb-in						
V	4,631 lbs						

Stress							
f _b	792 psi						
F _{b'}	3,631 psi						
f _b /F _{b'}	0.22						
f _v	209 psi						
F _{v'}	328 psi						
f _v /F _{v'}	0.64						
Max Ratio	0.64						
	Pass						

Deflection							
Δ _{T_L}	0.01 in						
	L/3,200						
Δ _{L_L}	0.01 in						
	L/3,668						
	Pass						

Header Calculations (H5)

	Additional Drift	Roof	Floor	Deck	Wall	Total Load	Total Load
Trib	0.0	7	0	0	1.33		1,185.0 plf
Dead Load	-	119.0	0.0	0.0	16.0	135.0 plf	
Live / Snow Load	0	1050.0	0.0	0.0	-	1,050.0 plf	

Description:	5.3 ft Opening						
Header Callout	(2)9.5 LVL 2.0E						
Trimmers	(1) 2x6 DF-L No. 2						
King Studs	(1) 2x6 DF-L No. 2						

Wood Design							
Species	LVL						
Grade	2.0E						
Width	3.50 in						
Depth	9.50 in						

Reaction							
Dead Load	354 lbs						
Live Load	2,756 lbs						

Load							
l _u	5.3 ft						
l _e	10.8 ft						

Adjustment Factors							
C _d	1.15						
C _F	1.1						

Material Properties							
F _b	2,900 psi						
F _v	285 psi						
E	2,000,000 psi						
E _{min}	1,016,535 psi						

Calculated Prop.							
A	33.25 in ²						
I	250.07 in ⁴						
S	52.65 in ³						
RB	10.03						
E _{min} '	1,016,535 psi						
F _{bE}	12,120 psi						
F _b *	3,669 psi						
C _L	1						

Shear and Moment							
M	48,991 lb-in						
V	3,111 lbs						

Stress							
f _b	931 psi						
F _b '	3,593 psi						
f _b /F _b '	0.26						
f _v	140 psi						
F _v '	328 psi						
f _v /F _v '	0.43						
Max Ratio	0.43						
	Pass						

Deflection							
Δ _L	0.04 in						
	L/1,556						
Δ _{LL}	0.04 in						
	L/1,756						
	Pass						

Header Calculations (H4)

	Additional Drift	Roof	Floor	Deck	Wall	Total Load	Total Load
Trib	0.0	21	0	0	1.33		3,523.0 plf
Dead Load	-	357.0	0.0	0.0	16.0	373.0 plf	
Live / Snow Load	0	3150.0	0.0	0.0	-	3,150.0 plf	

Description:	3.0 ft Opening	3.5 ft Opening					
Header Callout	(3)9.5 LVL 2.0E	(3)9.5 LVL 2.0E					
Trimmers	(2) 2x6 DF-L No. 2	(2) 2x6 DF-L No. 2					
King Studs	(1) 2x6 DF-L No. 2	(1) 2x6 DF-L No. 2					

Wood Design							
Species	LVL	LVL					
Grade	2.0E	2.0E					
Width	5.25 in	5.25 in					
Depth	9.50 in	9.50 in					

Reaction							
Dead Load	559 lbs	653 lbs					
Live Load	4,725 lbs	5,513 lbs					

Load							
lu	3.0 ft	3.5 ft					
le	6.2 ft	7.2 ft					

Adjustment Factors							
Cd	1.15	1.15					
CF	1.1	1.1					

Material Properties							
Fb	2,900 psi	2,900 psi					
Fv	285 psi	285 psi					
E	2,000,000 psi	2,000,000 psi					
Emin	1,016,535 psi	1,016,535 psi					

Calculated Prop.							
A	49.88 in ²	49.88 in ²					
I	375.10 in ⁴	375.10 in ⁴					
S	78.97 in ³	78.97 in ³					
RB	5.06	5.46					
Emin'	1,016,535 psi	1,016,535 psi					
FbE	47,723 psi	40,906 psi					
Fb*	3,669 psi	3,669 psi					
CL	1	1					

Shear and Moment							
M	47,560 lb-in	64,734 lb-in					
V	5,284 lbs	6,165 lbs					

Stress							
fb	602 psi	820 psi					
Fb'	3,653 psi	3,651 psi					
fb/Fb'	0.16	0.22					
fv	159 psi	185 psi					
Fv'	328 psi	328 psi					
fv/Fv'	0.48	0.57					
Max Ratio	0.48	0.57					
	Pass	Pass					

Deflection							
ΔTL	0.01 in	0.02 in					
	L/4,206	L/2,649					
ΔLL	0.01 in	0.01 in					
	L/4,704	L/2,963					
	Pass	Pass					

Header Calculations (H3)

	Additional Drift	Roof	Floor	Deck	Wall	Total Load	Total Load
Trib	0.0	14	0	0	1.33		2,354.0 plf
Dead Load	-	238.0	0.0	0.0	16.0	254.0 plf	
Live / Snow Load	0	2100.0	0.0	0.0	-	2,100.0 plf	

Description:	3.0 ft Opening	6.3 ft Opening					
Header Callout	(2)2x10 DF-L No. 2	(3)9.5 LVL 2.0E					
Trimmers	(2) 2x6 DF-L No. 2	(2) 2x6 DF-L No. 2					
King Studs	(1) 2x6 DF-L No. 2	(1) 2x6 DF-L No. 2					

Wood Design							
Species	DF-L	LVL					
Grade	No. 2	2.0E					
Width	3.00 in	5.25 in					
Depth	9.25 in	9.50 in					

Reaction							
Dead Load	381 lbs	794 lbs					
Live Load	3,150 lbs	6,563 lbs					

Load							
lu	3.0 ft	6.3 ft					
le	6.2 ft	12.6 ft					

Adjustment Factors							
Cd	1.15	1.15					
CF	1.1	1.1					

Material Properties							
Fb	900 psi	2,900 psi					
Fv	180 psi	285 psi					
E	1,600,000 psi	2,000,000 psi					
Emin	580,000 psi	1,016,535 psi					

Calculated Prop.							
A	27.75 in ²	49.88 in ²					
I	197.86 in ⁴	375.10 in ⁴					
S	42.78 in ³	78.97 in ³					
RB	8.73	7.21					
Emin'	580,000 psi	1,016,535 psi					
FbE	9,131 psi	23,477 psi					
Fb*	1,139 psi	3,669 psi					
CL	1	1					

Shear and Moment							
M	31,778 lb-in	137,927 lb-in					
V	3,531 lbs	7,356 lbs					

Stress							
fb	743 psi	1,747 psi					
Fb'	1,131 psi	3,635 psi					
fb/Fb'	0.66	0.48					
fv	191 psi	221 psi					
Fv'	207 psi	328 psi					
fv/Fv'	0.92	0.68					
Max Ratio	0.92	0.68					
	Pass	Pass					

Deflection							
ΔTL	0.01 in	0.11 in					
	L/2,657	L/696					
ΔLL	0.01 in	0.10 in					
	L/2,978	L/780					
	Pass	Pass					

Header Calculations (H2)

	Additional Drift	Roof	Floor	Deck	Wall	Total Load	Total Load
Trib	0.0	15.5	0	0	1.33		2,604.5 plf
Dead Load	-	263.5	0.0	0.0	16.0	279.5 plf	
Live / Snow Load	0	2325.0	0.0	0.0	-	2,325.0 plf	

Description:	6.3 ft Opening	3.0 ft Opening					
Header Callout	(3)9.5 LVL 2.0E	(2)2x12 DF-L No. 2					
Trimmers	(2) 2x6 DF-L No. 2	(2) 2x6 DF-L No. 2					
King Studs	(1) 2x6 DF-L No. 2	(1) 2x6 DF-L No. 2					

Wood Design							
Species	LVL	DF-L					
Grade	2.0E	No. 2					
Width	5.25 in	3.00 in					
Depth	9.50 in	11.25 in					

Reaction							
Dead Load	873 lbs	419 lbs					
Live Load	7,266 lbs	3,488 lbs					

Load							
lu	6.3 ft	3.0 ft					
le	12.6 ft	6.2 ft					

Adjustment Factors							
Cd	1.15	1.15					
CF	1.1	1					

Material Properties							
Fb	2,900 psi	900 psi					
Fv	285 psi	180 psi					
E	2,000,000 psi	1,600,000 psi					
Emin	1,016,535 psi	580,000 psi					

Calculated Prop.							
A	49.88 in ²	33.75 in ²					
I	375.10 in ⁴	355.96 in ⁴					
S	78.97 in ³	63.28 in ³					
RB	7.21	9.63					
Emin'	1,016,535 psi	580,000 psi					
FbE	23,477 psi	7,508 psi					
Fb*	3,669 psi	1,035 psi					
CL	1	1					

Shear and Moment							
M	152,605 lb-in	35,160 lb-in					
V	8,139 lbs	3,907 lbs					

Stress							
fb	1,932 psi	556 psi					
Fb'	3,635 psi	1,027 psi					
fb/Fb'	0.53	0.54					
fv	245 psi	174 psi					
Fv'	328 psi	207 psi					
fv/Fv'	0.75	0.84					
Max Ratio	0.75	0.84					
	Pass	Pass					

Deflection							
Δ _L	0.12 in	0.01 in					
	L/629	L/4,320					
Δ _{LL}	0.11 in	0.01 in					
	L/705	L/4,839					
	Pass	Pass					

Header Calculations (H1)

	Additional Drift	Roof	Floor	Deck	Wall	Total Load	Total Load
Trib	0.0	2.5	0	0	1.33		433.5 plf
Dead Load	-	42.5	0.0	0.0	16.0	58.5 plf	
Live / Snow Load	0	375.0	0.0	0.0	-	375.0 plf	

Description:	3.0 ft Opening	6.5 ft Opening	9.5 ft Opening	10.0 ft Opening			
Header Callout	(2)2x6 DF-L No. 2	(2)2x8 DF-L No. 2	(2)2x12 DF-L No. 2	(2)9.5 LVL 2.0E			
Trimmers	(1) 2x6 DF-L No. 2	(1) 2x6 DF-L No. 2	(1) 2x6 DF-L No. 2	(1) 2x6 DF-L No. 2			
King Studs	(1) 2x6 DF-L No. 2	(1) 2x6 DF-L No. 2	(1) 2x6 DF-L No. 2	(1) 2x6 DF-L No. 2			

Wood Design	Species	DF-L	DF-L	DF-L	LVL		
	Grade	No. 2	No. 2	No. 2	2.0E		
	Width	3.00 in	3.00 in	3.00 in	3.50 in		
	Depth	5.50 in	7.25 in	11.25 in	9.50 in		

Reaction	Dead Load	88 lbs	190 lbs	278 lbs	292 lbs		
	Live Load	563 lbs	1,219 lbs	1,781 lbs	1,875 lbs		

Load	lu	3.0 ft	6.5 ft	9.5 ft	10.0 ft		
	le	6.2 ft	12.4 ft	18.3 ft	18.7 ft		

Adjustment Factors	Cd	1.15	1.15	1.15	1.15		
	CF	1.3	1.2	1	1.1		

Material Properties	Fb	900 psi	900 psi	900 psi	2,900 psi		
	Fv	180 psi	180 psi	180 psi	285 psi		
	E	1,600,000 psi	1,600,000 psi	1,600,000 psi	2,000,000 psi		
	Emin	580,000 psi	580,000 psi	580,000 psi	1,016,535 psi		

Calculated Prop.	A	16.50 in^2	21.75 in^2	33.75 in^2	33.25 in^2		
	I	41.59 in^4	95.27 in^4	355.96 in^4	250.07 in^4		
	S	15.13 in^3	26.28 in^3	63.28 in^3	52.65 in^3		
	RB	6.73	10.95	16.57	13.18		
	Emin'	580,000 psi	580,000 psi	580,000 psi	1,016,535 psi		
	FbE	15,357 psi	5,803 psi	2,536 psi	7,019 psi		
	Fb*	1,346 psi	1,242 psi	1,035 psi	3,669 psi		
	CL	1	1	1	1		

Shear and Moment	M	5,852 lb-in	27,471 lb-in	58,680 lb-in	65,019 lb-in		
	V	650 lbs	1,409 lbs	2,059 lbs	2,167 lbs		

Stress	fb	387 psi	1,045 psi	927 psi	1,235 psi		
	Fb'	1,339 psi	1,226 psi	1,002 psi	3,495 psi		
	fb/Fb'	0.29	0.85	0.93	0.35		
	fv	59 psi	97 psi	92 psi	98 psi		
	Fv'	207 psi	207 psi	207 psi	328 psi		
	fv/Fv'	0.29	0.47	0.44	0.30		
	Max Ratio	0.29	0.85	0.93	0.35		
		Pass	Pass	Pass	Pass		

Deflection	ΔTL	0.01 in	0.11 in	0.14 in	0.20 in		
		L/3,033	L/683	L/817	L/615		
	ΔTL	0.01 in	0.10 in	0.12 in	0.17 in		
		L/3,506	L/789	L/945	L/711		
		Pass	Pass	Pass	Pass		

Beam Calculations (SHOP (3))

	Additional Drift	Roof	Floor	Deck	Wall	Total Load	Total Load
Trib	0.0	19.25	0	0	9.75		3,331.8 plf
Dead Load	-	327.3	0.0	0.0	117.0	444.3 plf	
Live / Snow Load	0	2887.5	0.0	0.0	-	2,887.5 plf	

Description:	3.0 ft Opening						
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Header Callout	(3)2x10 DF-L No. 2						
Trimmers	(2) 2x6 DF-L No. 2						
King Studs	(2) 2x6 DF-L No. 2						

Wood Design							
Species	DF-L						
Grade	No. 2						
Width	4.50 in						
Depth	9.25 in						

Reaction							
Dead Load	666 lbs						
Live Load	4,331 lbs						

Load							
l _u	3.0 ft						
l _e	6.2 ft						

Adjustment Factors							
C _d	1.15						
C _F	1.1						

Material Properties							
F _b	900 psi						
F _v	180 psi						
E	1,600,000 psi						
E _{min}	580,000 psi						

Calculated Prop.							
A	41.63 in ²						
I	296.79 in ⁴						
S	64.17 in ³						
RB	5.82						
E _{min'}	580,000 psi						
F _{bE}	20,546 psi						
F _{b*}	1,139 psi						
C _L	1						

Shear and Moment							
M	44,979 lb-in						
V	4,998 lbs						

Stress							
f _b	701 psi						
F _{b'}	1,135 psi						
f _b /F _{b'}	0.62						
f _v	180 psi						
F _{v'}	207 psi						
f _v /F _{v'}	0.87						
Max Ratio	0.87						
	Pass						

Deflection							
Δ _{T_L}	0.01 in						
	L/2,815						
Δ _{L_L}	0.01 in						
	L/3,249						
	Pass						

Beam Calculations (SHOP (2))

	Additional Drift	Roof	Floor	Deck	Wall	Total Load	Total Load
Trib	0.0	13	0	0	9.75		2,288.0 plf
Dead Load	-	221.0	0.0	0.0	117.0	338.0 plf	
Live / Snow Load	0	1950.0	0.0	0.0	-	1,950.0 plf	

Description:	3.0 ft Opening						
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Header Callout	(2)2x10 DF-L No. 2						
Trimmers	(2) 2x6 DF-L No. 2						
King Studs	(2) 2x6 DF-L No. 2						

Wood Design							
Species	DF-L						
Grade	No. 2						
Width	3.00 in						
Depth	9.25 in						

Reaction							
Dead Load	507 lbs						
Live Load	2,925 lbs						

Load							
l _u	3.0 ft						
l _e	6.2 ft						

Adjustment Factors							
C _d	1.15						
C _F	1.1						

Material Properties							
F _b	900 psi						
F _v	180 psi						
E	1,600,000 psi						
E _{min}	580,000 psi						

Calculated Prop.							
A	27.75 in ²						
I	197.86 in ⁴						
S	42.78 in ³						
RB	8.73						
E _{min'}	580,000 psi						
F _{bE}	9,131 psi						
F _{b*}	1,139 psi						
C _L	1						

Shear and Moment							
M	30,888 lb-in						
V	3,432 lbs						

Stress							
f _b	722 psi						
F _{b'}	1,131 psi						
f _b /F _{b'}	0.64						
f _v	186 psi						
F _{v'}	207 psi						
f _v /F _{v'}	0.90						
Max Ratio	0.90						
	Pass						

Deflection							
Δ _{T_L}	0.01 in						
	L/2,733						
Δ _{L_L}	0.01 in						
	L/3,207						
	Pass						

Beam Calculations (SHOP)

	Additional Drift	Roof	Floor	Deck	Wall	Total Load	Total Load
Trib	0.0	3	0	0	9.75		618.0 plf
Dead Load	-	51.0	0.0	0.0	117.0	168.0 plf	
Live / Snow Load	0	450.0	0.0	0.0	-	450.0 plf	

Description:	3.0 ft Opening	12.0 ft Opening					
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Header Callout	(2)2x6 DF-L No. 2	(2)11.875 LVL 2.0E					
Trimmers	(1) 2x6 DF-L No. 2	(2) 2x6 DF-L No. 2					
King Studs	(2) 2x6 DF-L No. 2	(5) 2x6 DF-L No. 2					

Wood Design							
Species	DF-L	LVL					
Grade	No. 2	2.0E					
Width	3.00 in	3.50 in					
Depth	5.50 in	11.88 in					

Reaction							
Dead Load	252 lbs	1,008 lbs					
Live Load	675 lbs	2,700 lbs					

Load							
lu	3.0 ft	12.0 ft					
le	6.2 ft	22.5 ft					

Adjustment Factors							
Cd	1.15	1.15					
CF	1.3	1					

Material Properties							
Fb	900 psi	2,900 psi					
Fv	180 psi	285 psi					
E	1,600,000 psi	2,000,000 psi					
Emin	580,000 psi	1,016,535 psi					

Calculated Prop.							
A	16.50 in^2	41.56 in^2					
I	41.59 in^4	488.41 in^4					
S	15.13 in^3	82.26 in^3					
RB	6.73	16.19					
Emin'	580,000 psi	1,016,535 psi					
FbE	15,357 psi	4,655 psi					
Fb*	1,346 psi	3,335 psi					
CL	1	1					

Shear and Moment							
M	8,343 lb-in	133,488 lb-in					
V	927 lbs	3,708 lbs					

Stress							
fb	552 psi	1,623 psi					
Fb'	1,339 psi	3,046 psi					
fb/Fb'	0.41	0.53					
fv	84 psi	134 psi					
Fv'	207 psi	328 psi					
fv/Fv'	0.41	0.41					
Max Ratio	0.41	0.53					
	Pass	Pass					

Deflection							
ΔTL	0.02 in	0.30 in					
	L/2,127	L/488					
ΔLL	0.01 in	0.21 in					
	L/2,921	L/670					
	Pass	Pass					

Wood Beam

Project File: 05 Beams.ec6

LIC# : KW-06013353, Build:20.23.08.30

SNAKE RIVER ENGINEERING

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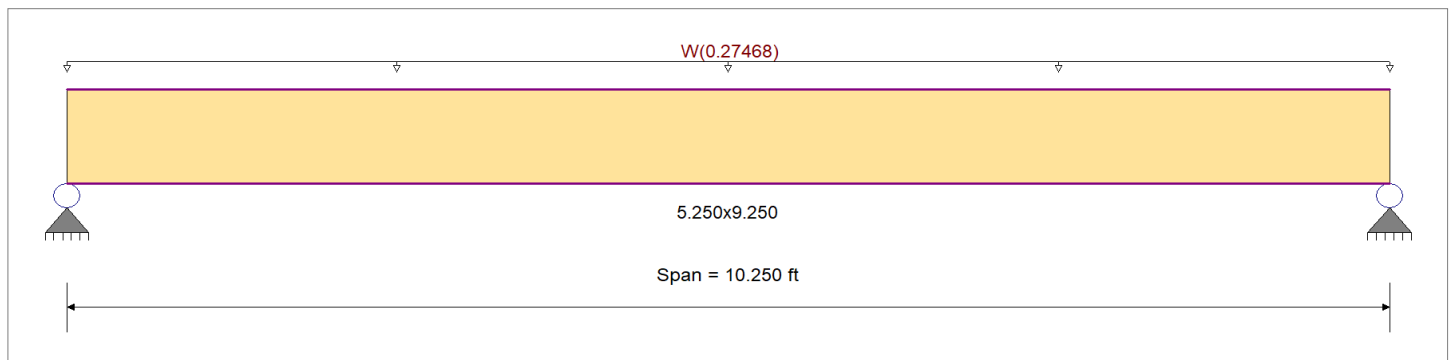
DESCRIPTION: WIND BEAM

CODE REFERENCES

Calculations per NDS 2018, IBC 2018, CBC 2019, ASCE 7-16
 Load Combination Set : IBC 2018

Material Properties

Analysis Method : Allowable Stress Design	Fb +	2,600.0 psi	E : Modulus of Elasticity
Load Combination : IBC 2018	Fb -	2,600.0 psi	Ebend- xx
	Fc - Prll	2,510.0 psi	Eminbend - xx
Wood Species : iLevel Truss Joist	Fc - Perp	750.0 psi	
Wood Grade : MicroLam LVL 1.9 E	Fv	285.0 psi	
	Ft	1,555.0 psi	Density
Beam Bracing : Beam is Fully Braced against lateral-torsional buckling			42.010pcf



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight NOT internally calculated and added
 Uniform Load : W = 0.02289 ksf, Tributary Width = 12.0 ft

DESIGN SUMMARY

Design OK

Maximum Bending Stress Ratio	=	0.143 : 1	Maximum Shear Stress Ratio	=	0.049 : 1
Section used for this span	=	5.250x9.250	Section used for this span	=	5.250x9.250
fb: Actual	=	611.23 psi	fv: Actual	=	22.28 psi
F'b	=	4,282.07 psi	F'v	=	456.00 psi
Load Combination	=	+0.60W	Load Combination	=	+0.60W
Location of maximum on span	=	5.125 ft	Location of maximum on span	=	0.000 ft
Span # where maximum occurs	=	Span # 1	Span # where maximum occurs	=	Span # 1
Maximum Deflection					
Max Downward Transient Deflection	0.324 in	Ratio = 379 >=360	Span: 1 : W Only		
Max Upward Transient Deflection	0 in	Ratio = 0 <360	n/a		
Max Downward Total Deflection	0.194 in	Ratio = 633 >=240	Span: 1 : +0.60W		
Max Upward Total Deflection	0 in	Ratio = 0 <240	n/a		

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Span #	Max Stress Ratios										Moment Values			Shear Values		
			M	V	CD	CM	C _t	CLx	C _F	C _{fu}	C _i	C _r	M	fb	F'b	V	fv	F'v
	Length = 10.250 ft	1			0.90	1.00	1.00	1.00	1.029	1.00	1.00	1.00			0.0	0.00	0.0	0.0
+0.60W						1.00	1.00	1.00	1.029	1.00	1.00	1.00			2,408.7	0.00	0.0	256.5
	Length = 10.250 ft	1	0.143	0.049	1.60	1.00	1.00	1.00	1.029	1.00	1.00	1.00	2.16	611.2	4,282.1	0.72	22.3	456.0
+0.450W						1.00	1.00	1.00	1.029	1.00	1.00	1.00			0.0	0.00	0.0	0.0
	Length = 10.250 ft	1	0.107	0.037	1.60	1.00	1.00	1.00	1.029	1.00	1.00	1.00	1.62	458.4	4,282.1	0.54	16.7	456.0

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
W Only	1	0.3238	5.162		0.0000	0.000

Project Title:
Engineer:
Project ID:
Project Descr:

Wood Beam

Project File: 05 Beams.ec6

LIC# : KW-06013353, Build:20.23.08.30

SNAKE RIVER ENGINEERING

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DESCRIPTION: WIND BEAM

Vertical Reactions

Support notation : Far left is #1

Values in KIPS

Load Combination	Support 1	Support 2
Max Upward from all Load Conditions	1.408	1.408
Max Upward from Load Combinations	0.845	0.845
Max Upward from Load Cases	1.408	1.408
+0.60W	0.845	0.845
+0.450W	0.633	0.633
W Only	1.408	1.408

WOOD TALL WALL & KING STUD ALLOWABLE LOADS (plf):

Load Duration Factor: 1.6
Max Vert. Load: 50 lbs

Max Deflection: L/180

King Stud	Height						
	12'	14'	16'	18'	20'	22'	24'
(1) 2x4 Stud	12.8	NA	NA	NA	NA	NA	NA
(2) 2x4 Stud	25.6	NA	NA	NA	NA	NA	NA
(3) 2x4 Stud	38.4	NA	NA	NA	NA	NA	NA
(1) 2x6 DF #2	57.0	35.8	24.1	16.9	NA	NA	NA
(2) 2x6 DF #2	114.0	71.6	48.2	33.8	NA	NA	NA
(3) 2x6 DF #2	171.0	107.4	72.3	50.7	NA	NA	NA
(1) 2x8 DF #2	130.0	81.7	55.0	38.7	28.2	21.2	16.3
(2) 2x8 DF #2	260.0	163.4	110.0	77.4	56.4	42.4	32.6
(3) 2x8 DF #2	390.0	245.1	165.0	116.1	84.6	63.6	48.9
(1) 2x6 LSL	67.8	42.7	28.5	20.0	14.7	NA	NA
(2) 2x6 LSL	135.6	85.4	57.0	40.0	29.4	NA	NA
(3) 2x6 LSL	203.4	128.1	85.5	60.0	44.1	NA	NA
(1) 2x8 LSL	155.0	98.3	65.5	46.0	33.5	25.2	19.5
(2) 2x8 LSL	310.0	196.6	131.0	92.0	67.0	50.4	39.0
(3) 2x8 LSL	465.0	294.9	196.5	138.0	100.5	75.6	58.5

*NOTE 1: this table combined with trimmer table to determine combined stress on each common wall stud.
*NOTE 2: allowable loads are interpolated at heights not in 2' increments.

WOOD TRIMMER ALLOWABLE LOADS (kips):

Load Duration Factor: 1.0
Eccentricity: 0"

Weak Axis Braced: Y

Trimmer Type	Height						
	8'	10'	12'	14'	16'	18'	20'
(1) 2x4 Stud	2.4	1.7	1.2	NA	NA	NA	NA
(2) 2x4 Stud	4.9	3.4	2.4	NA	NA	NA	NA
(3) 2x4 Stud	7.1	5.0	3.6	NA	NA	NA	NA
(1) 2x6 DF #2	5.1	5.1	5.0	3.8	3.0	NA	NA
(2) 2x6 DF #2	10.3	10.3	10.1	7.7	6.0	NA	NA
(3) 2x6 DF #2	15.4	15.4	15.1	11.6	9.1	NA	NA
(1) 2x8 DF #2	6.7	6.7	6.7	6.7	6.4	5.3	4.4
(2) 2x8 DF #2	13.5	13.5	13.5	13.5	12.9	10.6	8.8
(3) 2x8 DF #2	20.3	20.3	20.3	20.3	19.4	15.9	13.2

*NOTE 1: this table combined with king stud table to determine combined stress on each common wall stud.
*NOTE 2: allowable loads are interpolated at heights not in 2' increments.

TALL WALL CALCULATIONS:

This spreadsheet is used for designing a stud wall according to the NDS.

Description:	10.5' Tall Wall	9' Tall Wall			
Type:	2x Lumber (2"-4")	2x Lumber (2"-4")			
Species:	DF-L	DF-L			
Grade:	No. 2	No. 2			
Nominal width, t =	(1) 2	(1) 2			
Actual width =	1.50 in	1.50 in			
Nominal depth, d =	6	6			
Actual depth =	5.50 in	5.50 in			
Span, L =	10.500 ft	9.000 ft			
w/o Plates	10.250 ft	8.750 ft			
Stud spacing, s =	16 in	16 in			
Lat. Pressure, w _{wind} =	13.74 psf	13.74 psf			
Axial load, P =	4751 lbs	3563 lbs			
Eccentricity, e =	0 in	0 in			
K _{c,E} =	0.3	0.3			
c =	0.8	0.8			
w =	18.3 plf	18.3 plf			
F _b	900 psi	900 psi			
F _v	180 psi	180 psi			
F _{c-prll}	1,350 psi	1,350 psi			
F _{c-perp}	625 psi	625 psi			
C _d	1.60	1.60			
C _{F,Fb}	1.30	1.30			
C _{F,Fcprll}	1.10	1.10			
C _r	1.15	1.15			
C _p	0.36	0.47			
C _H	1.00	1.00			
C _b	1.07	1.07			
E	1,600,000 psi	1,600,000 psi			
E _{min}	580,000 psi	580,000 psi			
Allowable Stress:					
F' _b = F _b C _d C _F C _r =	2153 psi	2153 psi			
F' _v = F _v C _d C _H =	288 psi	288 psi			
F* _c = F _c C _d C _F =	2376 psi	2376 psi			
F _{CE} = (K _{cE} E')/(l/d) ² =	960 psi	1317 psi			
F' _c = F _c C _d C _F C _p =	862 psi	1118 psi			
F' _{c-perp} = F _{c-perp} C _b =	668 psi	668 psi			
E'	E = 1600000 psi	1600000 psi			
F _{bE}	2315 psi	2712 psi			
Slenderness Ratio:	< 50 OK	< 50 OK			
R _g	17	16			
Bending:	< F'_b OK	< F'_b OK			
M = w L ² /8 + P e/12 =	241 ft-lbs	175 ft-lbs			
f _b = M/S =	382 psi	278 psi			
S =	8 in ³	8 in ³			
Shear:	< F'_v OK	< F'_v OK			
V = w L/2 =	94 lbs	80 lbs			
f _v = 1.5 V/A =	17 psi	15 psi			
A =	8 in ²	8 in ²			
Compression:	< F'_c OK	< F'_c OK			
f _c = P/A =	576 psi	432 psi			
Compression (perp.):	< F'_c OK	< F'_c OK			
f _{c-perp} = P/A =	576 psi	432 psi			
Combined:	< 1.0 OK	< 1.0 OK			
((f _c /F _c) ² + (f _b /[F _b (1-(f _c /F _c E))]) =	0.89	0.34			
Deflection:	≥ 180 OK	≥ 180 OK			
D = 22.5 w L ⁴ /E' I =	0.14 in	0.07 in			
I =	21 in ⁴	21 in ⁴			
SPAN /	900	1446			

TALL WALL CALCULATIONS:

This spreadsheet is used for designing a stud wall according to the NDS.

Description:	14.5' Tall Wall	King Stud (8.5' Max Opening)	King Stud (10' Max Opening)	12' Tall Wall	12' Tall Wall	10.5' Tall Wall
Type:	2x Lumber (2"-4")					
Species:	DF-L					
Grade:	No. 2					
Nominal width, t =	(1) 2	(2) 2	(1) 2	(1) 2	(1) 2	(1) 2
Actual width =	1.50 in	3.00 in	1.50 in	1.50 in	1.50 in	1.50 in
Nominal depth, d =	6	6	6	6	6	6
Actual depth =	5.50 in	5.50 in	5.50 in	5.50 in	5.50 in	5.50 in
Span, L =	14.500 ft	14.500 ft	10.500 ft	12.000 ft	12.000 ft	10.500 ft
w/o Plates	14.250 ft	14.250 ft	10.250 ft	11.750 ft	11.750 ft	10.250 ft
Stud spacing, s =	16 in	53 in	62 in	12 in	16 in	12 in
Lat. Pressure, w _{wind} =	13.74 psf	13.74 psf	13.74 psf	13.74 psf	13.74 psf	13.74 psf
Axial load, P =	557 lbs	50 lbs	50 lbs	3424 lbs	3229 lbs	4064 lbs
Eccentricity, e =	0 in	0 in	0 in	0 in	0 in	0 in
K _{cE} =	0.3	0.3	0.3	0.3	0.3	0.3
c =	0.8	0.8	0.8	0.8	0.8	0.8
w =	18.3 plf	61.0 plf	71.3 plf	13.7 plf	18.3 plf	13.7 plf
F _b	900 psi	900 psi	900 psi	900 psi	900 psi	900 psi
F _v	180 psi	180 psi	180 psi	180 psi	180 psi	180 psi
F _{c-prll}	1,350 psi	1,350 psi	1,350 psi	1,350 psi	1,350 psi	1,350 psi
F _{c-perp}	625 psi	625 psi	625 psi	625 psi	625 psi	625 psi
C _d	1.60	1.60	1.60	1.60	1.60	1.60
C _{F,Fb}	1.30	1.30	1.30	1.30	1.30	1.30
C _{F,Fcprll}	1.10	1.10	1.10	1.10	1.10	1.10
C _r	1.15	1.00	1.00	1.15	1.15	1.15
C _p	0.20	0.20	0.36	0.28	0.28	0.36
C _H	1.00	1.00	1.00	1.00	1.00	6.00
C _b	1.07	1.07	1.07	1.07	1.07	1.07
E	1,600,000 psi	1,600,000 psi	1,600,000 psi	1,600,000 psi	1,600,000 psi	1,600,000 psi
E _{min}	580,000 psi	580,000 psi	580,000 psi	580,000 psi	580,000 psi	580,000 psi
Allowable Stress:						
F' _b = F _b C _d C _F C _r	2153 psi	1872 psi	1872 psi	2153 psi	2153 psi	2153 psi
F' _v = F _v C _d C _H	288 psi	288 psi	288 psi	288 psi	288 psi	1728 psi
F' _c = F _c C _d C _F	2376 psi	2376 psi	2376 psi	2376 psi	2376 psi	2376 psi
F' _{cE} = (K _{cE} E')/(l/d) ²	497 psi	497 psi	900 psi	730 psi	730 psi	960 psi
F' _c = F _c C _d C _F C _p	473 psi	473 psi	862 psi	676 psi	676 psi	862 psi
F' _{c-perp} = F _c C _b	668 psi	668 psi	668 psi	668 psi	668 psi	668 psi
E'	1600000 psi	1600000 psi	1600000 psi	1600000 psi	1600000 psi	1600000 psi
F _{bE}	1665 psi	6660 psi	2315 psi	2019 psi	2019 psi	2315 psi
Slenderness Ratio:	< 50 OK	< 50 OK	< 50 OK	< 50 OK	< 50 OK	< 50 OK
R _g	20	10	17	19	19	17
Bending:	< F'_b OK	< F'_b OK	< F'_b OK	< F'_b OK	< F'_b OK	< F'_b OK
M = w L ² /8 + P e/12	465 ft-lbs	1547 ft-lbs	936 ft-lbs	237 ft-lbs	316 ft-lbs	180 ft-lbs
f _b = M/S	738 psi	1228 psi	1485 psi	376 psi	502 psi	286 psi
S =	8 in ³	15 in ³	8 in ³	8 in ³	8 in ³	8 in ³
Shear:	< F'_v OK	< F'_v OK	< F'_v OK	< F'_v OK	< F'_v OK	< F'_v OK
V = w L/2	131 lbs	434 lbs	365 lbs	81 lbs	108 lbs	70 lbs
f _v = 1.5 V/A	24 psi	39 psi	66 psi	15 psi	20 psi	13 psi
A =	8 in ²	17 in ²	8 in ²	8 in ²	8 in ²	8 in ²
Compression:	< F'_c OK	< F'_c OK	< F'_c OK	< F'_c OK	< F'_c OK	< F'_c OK
f _c = P/A	67 psi	3 psi	6 psi	415 psi	391 psi	493 psi
Compression (perp.):	< F'_c OK	< F'_c OK	< F'_c OK	< F'_c OK	< F'_c OK	< F'_c OK
f _{c-perp} = P/A	67 psi	3 psi	6 psi	415 psi	391 psi	493 psi
Combined:	< 1.0 OK	< 1.0 OK	< 1.0 OK	< 1.0 OK	< 1.0 OK	< 1.0 OK
(f _c /F _c) ² + (f _b /F _b (1-(f _c /F _c E)))	0.42			0.78	0.84	0.60
Deflection:	≥ 180 OK	≥ 180 OK	≥ 180 OK	≥ 180 OK	≥ 180 OK	≥ 180 OK
D = 22.5 w L ⁴ /E'I =	0.51 in	0.85 in	0.53 in	0.18 in	0.24 in	0.10 in
I =	21 in ⁴	42 in ⁴	21 in ⁴	21 in ⁴	21 in ⁴	21 in ⁴
SPAN /	335	201	231	796	597	1200

TALL WALL CALCULATIONS:

This spreadsheet is used for designing a stud wall according to the NDS.

Description:	16.42' Tall Wall	King Stud (3' Max Opening)	16.42' Tall Wall	King Stud (12' Max Opening)	9' Tall Wall	
Type:	2x Lumber (2"-4")	2x Lumber (2"-4")	2x Lumber (2"-4")	2x Lumber (2"-4")	2x Lumber (2"-4")	
Species:	DF-L	DF-L	DF-L	DF-L	DF-L	
Grade:	No. 2	No. 2	No. 2	No. 2	No. 2	
Nominal width, t =	(1) 2	(2) 2	(1) 2	(5) 2	(1) 2	
Actual width =	1.50 in	3.00 in	1.50 in	7.50 in	1.50 in	
Nominal depth, d =	6	6	6	6	6	
Actual depth =	5.50 in	5.50 in	5.50 in	5.50 in	5.50 in	
Span, L =	16.420 ft	16.420 ft	16.420 ft	16.420 ft	9.000 ft	
w/o Plates	16.170 ft	16.170 ft	16.170 ft	16.170 ft	8.750 ft	
Stud spacing, s =	8 in	24 in	16 in	82 in	16 in	
Lat. Pressure, w _{wind} =	13.74 psf	13.74 psf	13.74 psf	13.74 psf	13.74 psf	
Axial load, P =	1392 lbs	50 lbs	557 lbs	50 lbs	4175 lbs	
Eccentricity, e =	0 in	0 in	0 in	0 in	0 in	
K _{cE} =	0.3	0.3	0.3	0.3	0.3	
c =	0.8	0.8	0.8	0.8	0.8	
w =	9.2 plf	27.8 plf	18.3 plf	94.2 plf	18.3 plf	
F _b	900 psi	900 psi	900 psi	900 psi	900 psi	
F _v	180 psi	180 psi	180 psi	180 psi	180 psi	
F _{c-prll}	1,350 psi	1,350 psi	1,350 psi	1,350 psi	1,350 psi	
F _{c-perp}	625 psi	625 psi	625 psi	625 psi	625 psi	
C _d	1.60	1.60	1.60	1.60	1.60	
C _{F,Fb}	1.30	1.30	1.30	1.30	1.30	
C _{F,Fcprll}	1.10	1.10	1.10	1.10	1.10	
C _r	1.15	1.00	1.15	1.00	1.15	
C _p	0.16	0.16	0.16	0.16	0.47	
C _H	1.00	1.00	1.00	1.00	1.00	
C _b	1.07	1.07	1.07	1.07	1.07	
E	1,600,000 psi	1,600,000 psi	1,600,000 psi	1,600,000 psi	1,600,000 psi	
E _{min}	580,000 psi	580,000 psi	580,000 psi	580,000 psi	580,000 psi	
Allowable Stress:						
F' _b = F _b C _d C _F C _r	2153 psi	1872 psi	2153 psi	1872 psi	2153 psi	
F' _v = F _v C _d C _H	288 psi	288 psi	288 psi	288 psi	288 psi	
F' _c = F _c C _d C _F	2376 psi	2376 psi	2376 psi	2376 psi	2376 psi	
F' _{cE} = (K _{cE} E')/(l/d)2	386 psi	386 psi	386 psi	386 psi	1317 psi	
F' _c = F _c C _d C _F C _p	372 psi	372 psi	372 psi	372 psi	1118 psi	
F' _{c-perp} = F _c C _b	668 psi	668 psi	668 psi	668 psi	668 psi	
E' = E	1600000 psi	1600000 psi	1600000 psi	1600000 psi	1600000 psi	
F _{bE} =	1467 psi	5869 psi	1467 psi	36684 psi	2712 psi	
Slenderness Ratio:	< 50 OK	< 50 OK	< 50 OK	< 50 OK	< 50 OK	
R _g =	22	11	22	4	16	
Bending:	< F' _b OK	< F' _b OK	< F' _b OK	< F' _b OK	< F' _b OK	
M = w L ² /8 + P e/12 =	299 ft-lbs	907 ft-lbs	599 ft-lbs	3077 ft-lbs	175 ft-lbs	
f _b = M/S =	475 psi	720 psi	950 psi	977 psi	278 psi	
S =	8 in ³	15 in ³	8 in ³	38 in ³	8 in ³	
Shear:	< F' _v OK	< F' _v OK	< F' _v OK	< F' _v OK	< F' _v OK	
V = w L/2 =	74 lbs	224 lbs	148 lbs	761 lbs	80 lbs	
f _v = 1.5 V/A =	13 psi	20 psi	27 psi	28 psi	15 psi	
A =	8 in ²	17 in ²	8 in ²	41 in ²	8 in ²	
Compression:	< F' _c OK	< F' _c OK	< F' _c OK	< F' _c OK	< F' _c OK	
f _c = P/A =	169 psi	3 psi	67 psi	1 psi	506 psi	
Compression (perp.):	< F' _c OK	< F' _c OK	< F' _c OK	< F' _c OK	< F' _c OK	
f _{c-perp} = P/A =	169 psi	3 psi	67 psi	1 psi	506 psi	
Combined:	< 1.0 OK	< 1.0 OK	< 1.0 OK	< 1.0 OK	< 1.0 OK	
(f _c /F _c)2 + (f _b /[F _b (1-(f _c /F _c E))]) =	0.60	0.57	0.57	0.41	0.41	
Deflection:	≥ 180 OK	≥ 180 OK	≥ 180 OK	≥ 180 OK	≥ 180 OK	
D = 22.5 w L ⁴ /E' I =	0.42 in	0.64 in	0.85 in	0.87 in	0.07 in	
I =	21 in ⁴	42 in ⁴	21 in ⁴	104 in ⁴	21 in ⁴	
SPAN /	458	302	229	223	1446	

UNBRACED WOOD COLUMN ALLOWABLE LOADS (kips)

Column Type	Unbraced Height							Compression Perp. To Grain
	8'	10'	12'	14'	16'	18'	20'	
(2) 2x4 DF #2	4.50	3.00	2.10	SR	SR	SR	SR	6.50
(3) 2x4 DF #2	8.80	5.90	4.20	3.20	SR	SR	SR	9.80
4x4 DF #2	7.00	4.60	3.30	2.40	SR	SR	SR	7.60
(2) 2x6 DF #2	7.20	4.70	3.30	SR	SR	SR	SR	10.30
(3) 2x6 DF #2	20.40	14.70	10.70	8.00	6.20	4.90	SR	15.40
6x6 DF #2	18.00	15.70	13.00	10.50	8.50	6.90	5.70	18.90
6x8 DF #2	24.50	21.40	17.80	14.30	11.60	9.40	7.80	25.70
6x10 DF #2	31.40	27.10	22.50	18.20	14.70	12.00	9.90	32.60
8x8 DF #2	36.60	34.60	31.90	28.50	24.90	21.30	18.20	35.20
8x10 DF #2	46.30	43.90	40.40	36.20	31.50	27.00	23.10	44.50
8x12 DF #2	56.20	53.10	49.00	43.80	38.10	32.70	28.00	53.40
10x10 DF #2	60.50	58.80	56.50	53.40	49.60	45.20	40.50	56.40

Wood Column

Project File: 05 Beams.ec6

LIC# : KW-06013353, Build:20.23.08.30

SNAKE RIVER ENGINEERING

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DESCRIPTION: RB1 BRG.

Code References

Calculations per NDS 2018, IBC 2018, CBC 2019, ASCE 7-16
 Load Combinations Used : IBC 2018

General Information

Analysis Method	Allowable Stress Design			Wood Section Name	8x8
End Fixities	Top & Bottom Pinned			Wood Grading/Manuf.	Graded Lumber
Overall Column Height	9 ft			Wood Member Type	Sawn
<i>(Used for non-slender calculations)</i>					
Wood Species	Douglas Fir-Larch			Exact Width	7.50 in
Wood Grade	No.2			Exact Depth	7.50 in
Fb +	750 psi	Fv	170 psi	Area	56.250 in^2
Fb -	750 psi	Ft	475 psi	Ix	263.672 in^4
Fc - Prll	700 psi	Density	31.21 pcf	Iy	263.672 in^4
Fc - Perp	625 psi			Allow Stress Modification Factors	
E : Modulus of Elasticity . . .	x-x Bending	y-y Bending	Axial	Cf or Cv for Bending 1.0	
	Basic	1300	1300	1300 ksi	Cf or Cv for Compression 1.0
	Minimum	470	470		Cf or Cv for Tension 1.0
				Column Buckling Condition:	Cm : Wet Use Factor 1.0
				ABOUT X-X Axis: Lux = 9 ft, Kx = 1.0	Ct : Temperature Fact 1.0
				ABOUT Y-Y Axis: Luy = 9 ft, Ky = 1.0	Cfu : Flat Use Factor 1.0
					Kf : Built-up columns 1.0
					Use Cr : Repetitive ? No

Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Column self weight included : 109.723 lbs * Dead Load Factor

AXIAL LOADS . . .

Axial Load at 9.0 ft, D = 16.10 k

DESIGN SUMMARY

Bending & Shear Check Results

PASS Max. Axial+Bending Stress Ratio = **0.4986 : 1**
 Load Combination D Only
 Governing NDS Formula Comp Only, fc/Fc'
 Location of max.above base 0.0 ft
 At maximum location values are .
 Applied Axial 16.210 k
 Applied Mx 0.0 k-ft
 Applied My 0.0 k-ft
 Fc : Allowable 578.01 psi

Maximum SERVICE Lateral Load Reactions . .
 Top along Y-Y 0.0 k Bottom along Y-Y 0.0 k
 Top along X-X 0.0 k Bottom along X-X 0.0 k

Maximum SERVICE Load Lateral Deflections . . .
 Along Y-Y 0.0 in at 0.0 ft above base
 for load combination : n/a
 Along X-X 0.0 in at 0.0 ft above base
 for load combination : n/a

PASS Maximum Shear Stress Ratio = **0.0 : 1**
 Load Combination +0.60D
 Location of max.above base 9.0 ft
 Applied Design Shear 0.0 psi
 Allowable Shear 272.0 psi

Other Factors used to calculate allowable stresses . . .
Bending Compression Tension

Load Combination Results

Load Combination	C _D	C _P	Maximum Axial + Bending Stress Ratios			Maximum Shear Ratios		
			Stress Ratio	Status	Location	Stress Ratio	Status	Location
D Only	0.900	0.917	0.4986	PASS	0.0 ft	0.0	PASS	9.0 ft
+0.60D	1.600	0.833	0.1853	PASS	0.0 ft	0.0	PASS	9.0 ft

Maximum Reactions

Note: Only non-zero reactions are listed.

Load Combination	X-X Axis Reaction		k	Y-Y Axis Reaction		Axial Reaction	My - End Moments		Mx - End Moments	
	@ Base	@ Top		@ Base	@ Top		@ Base	@ Top	@ Base	@ Top
D Only						16.210				
+0.60D						9.726				

Wood Column

Project File: 05 Beams.ec6

LIC# : KW-06013353, Build:20.23.08.30

SNAKE RIVER ENGINEERING

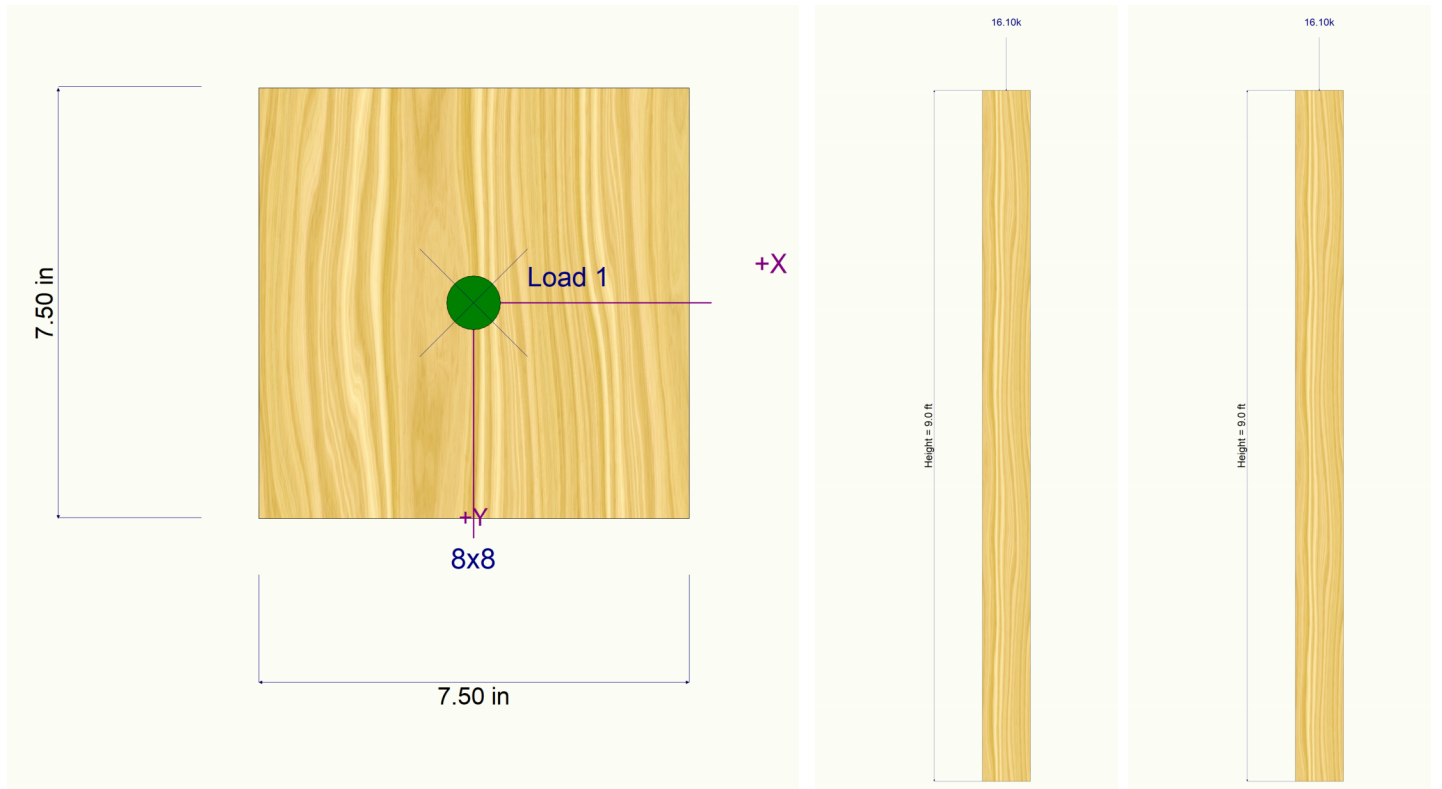
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DESCRIPTION: RB1 BRG.

Maximum Deflections for Load Combinations

Load Combination	Max. X-X Deflection	Distance	Max. Y-Y Deflection	Distance
D Only	0.0000 in	0.000ft	0.000 in	0.000 ft
+0.60D	0.0000 in	0.000ft	0.000 in	0.000 ft

Sketches



Wood Column

Project File: 05 Beams.ec6

LIC# : KW-06013353, Build:20.23.08.30

SNAKE RIVER ENGINEERING

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DESCRIPTION: RB2 BRG.

Code References

Calculations per NDS 2018, IBC 2018, CBC 2019, ASCE 7-16
 Load Combinations Used : IBC 2018

General Information

Analysis Method	Allowable Stress Design			Wood Section Name	8x8
End Fixities	Top & Bottom Pinned			Wood Grading/Manuf.	Graded Lumber
Overall Column Height	8 ft			Wood Member Type	Sawn
<i>(Used for non-slender calculations)</i>					
Wood Species	Douglas Fir-Larch			Exact Width	7.50 in
Wood Grade	No.2			Exact Depth	7.50 in
Fb +	750.0 psi	Fv	170.0 psi	Area	56.250 in^2
Fb -	750.0 psi	Ft	475.0 psi	Ix	263.672 in^4
Fc - Prll	700.0 psi	Density	31.210 pcf	Iy	263.672 in^4
Fc - Perp	625.0 psi			Allow Stress Modification Factors	
E : Modulus of Elasticity . . .	x-x Bending	y-y Bending	Axial	Cf or Cv for Bending 1.0	
	Basic	1,300.0	1,300.0	1,300.0 ksi	Cf or Cv for Compression 1.0
	Minimum	470.0	470.0		Cf or Cv for Tension 1.0
					Cm : Wet Use Factor 1.0
					Ct : Temperature Fact 1.0
					Cfu : Flat Use Factor 1.0
					Kf : Built-up columns 1.0
					Use Cr : Repetitive ? No
				Column Buckling Condition:	
				ABOUT X-X Axis: Lux = 8 ft, Kx = 1.0	
				ABOUT Y-Y Axis: Luy = 8 ft, Ky = 1.0	

Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Column self weight included : 97.531 lbs * Dead Load Factor

AXIAL LOADS . . .

Axial Load at 8.0 ft, D = 20.633 k

DESIGN SUMMARY

Bending & Shear Check Results

PASS Max. Axial+Bending Stress Ratio = **0.6241 : 1**
 Load Combination D Only
 Governing NDS Formula Comp Only, fc/Fc'
 Location of max.above base 0.0 ft
 At maximum location values are .
 Applied Axial 20.731 k
 Applied Mx 0.0 k-ft
 Applied My 0.0 k-ft
 Fc : Allowable 590.54 psi

Maximum SERVICE Lateral Load Reactions . .
 Top along Y-Y 0.0 k Bottom along Y-Y 0.0 k
 Top along X-X 0.0 k Bottom along X-X 0.0 k

Maximum SERVICE Load Lateral Deflections . . .
 Along Y-Y 0.0 in at 0.0 ft above base
 for load combination : n/a
 Along X-X 0.0 in at 0.0 ft above base
 for load combination : n/a

PASS Maximum Shear Stress Ratio = **0.0 : 1**
 Load Combination +0.60D
 Location of max.above base 8.0 ft
 Applied Design Shear 0.0 psi
 Allowable Shear 272.0 psi

Other Factors used to calculate allowable stresses . . .
Bending Compression Tension

Load Combination Results

Load Combination	C _D	C _P	Maximum Axial + Bending Stress Ratios			Maximum Shear Ratios		
			Stress Ratio	Status	Location	Stress Ratio	Status	Location
D Only	0.900	0.937	0.6241	PASS	0.0 ft	0.0	PASS	8.0 ft
+0.60D	1.600	0.875	0.2255	PASS	0.0 ft	0.0	PASS	8.0 ft

Maximum Reactions

Note: Only non-zero reactions are listed.

Load Combination	X-X Axis Reaction		k	Y-Y Axis Reaction		Axial Reaction	My - End Moments		k-ft		Mx - End Moments	
	@ Base	@ Top		@ Base	@ Top		@ Base	@ Top	@ Base	@ Top		
D Only						20.731						
+0.60D						12.438						

Wood Column

Project File: 05 Beams.ec6

LIC# : KW-06013353, Build:20.23.08.30

SNAKE RIVER ENGINEERING

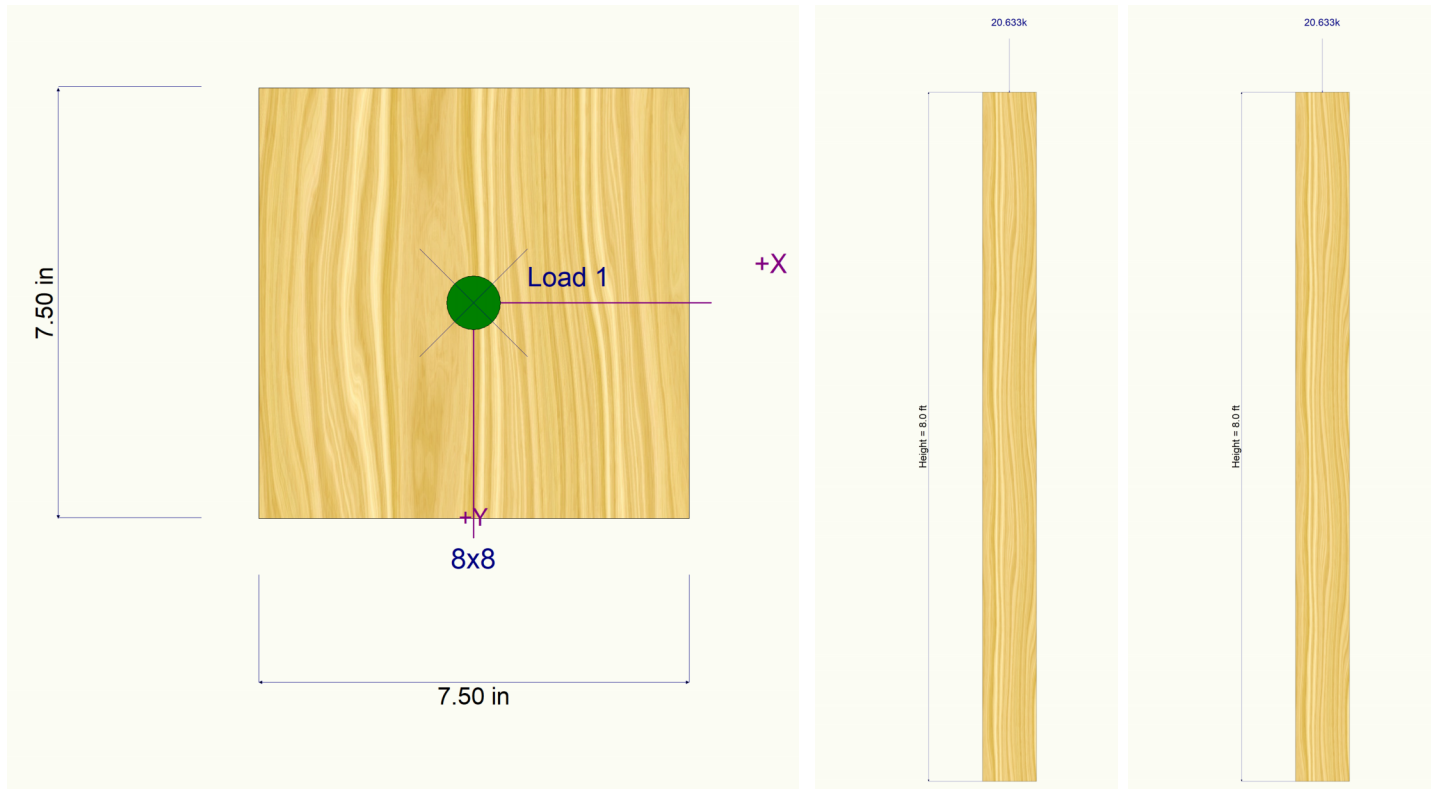
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DESCRIPTION: RB2 BRG.

Maximum Deflections for Load Combinations

Load Combination	Max. X-X Deflection	Distance	Max. Y-Y Deflection	Distance
D Only	0.0000 in	0.000ft	0.000 in	0.000 ft
+0.60D	0.0000 in	0.000ft	0.000 in	0.000 ft

Sketches



Wood Column

Project File: 05 Beams.ec6

LIC# : KW-06013353, Build:20.23.08.30

SNAKE RIVER ENGINEERING

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DESCRIPTION: LIVING MIDDLE KING STUD

Code References

Calculations per NDS 2018, IBC 2018, CBC 2019, ASCE 7-16
 Load Combinations Used : IBC 2018

General Information

Analysis Method	Allowable Stress Design	Wood Section Name	6x6
End Fixities	Top & Bottom Pinned	Wood Grading/Manuf.	Graded Lumber
Overall Column Height	20.67 ft	Wood Member Type	Sawn
<i>(Used for non-slender calculations)</i>			
Wood Species	Douglas Fir-Larch	Exact Width	5.50 in
Wood Grade	No.2	Exact Depth	5.50 in
Fb +	750 psi	Fv	170 psi
Fb -	750 psi	Ft	475 psi
Fc - Prll	700 psi	Density	31.21 pcf
Fc - Perp	625 psi		
E : Modulus of Elasticity . . .	x-x Bending	y-y Bending	Axial
	Basic	1300	1300
	Minimum	470	470
			1300 ksi
			Column Buckling Condition:
			Fully braced against buckling ABOUT X-X Axis
			ABOUT Y-Y Axis: Luy = 19.0 ft, Ky = 1.0
			Allow Stress Modification Factors
			Cf or Cv for Bending 1.0
			Cf or Cv for Compression 1.0
			Cf or Cv for Tension 1.0
			Cm : Wet Use Factor 1.0
			Ct : Temperature Fact 1.0
			Cfu : Flat Use Factor 1.0
			Kf : Built-up columns 1.0
			Use Cr : Repetitive ? No

Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Column self weight included : 135.518 lbs * Dead Load Factor

AXIAL LOADS . . .

Axial Load at 20.670 ft, D = 0.5840, S = 3.750 k

BENDING LOADS . . .

Lat. Point Load at 19.0 ft creating Mx-x, W = 2.0 k

DESIGN SUMMARY

Bending & Shear Check Results

PASS Max. Axial+Bending Stress Ratio = **0.7926 : 1**
 Load Combination +D+0.750S+0.450W
 Governing NDS Formula Comp + Mxx, NDS Eq. 3.9-3
 Location of max.above base 19.005 ft
 At maximum location values are .
 Applied Axial 3.532 k
 Applied Mx 1.377 k-ft
 Applied My 0.0 k-ft
 Fc : Allowable 214.638 psi

Maximum SERVICE Lateral Load Reactions . .
 Top along Y-Y 1.838 k Bottom along Y-Y 0.1616 k
 Top along X-X 0.0 k Bottom along X-X 0.0 k

Maximum SERVICE Load Lateral Deflections . . .
 Along Y-Y 1.594 in at 11.930 ft above base
 for load combination : W Only
 Along X-X 0.0 in at 0.0 ft above base
 for load combination : n/a

Other Factors used to calculate allowable stresses . . .
Bending Compression Tension

PASS Maximum Shear Stress Ratio = **0.2011 : 1**
 Load Combination +D+0.60W
 Location of max.above base 20.670 ft
 Applied Design Shear 82.045 psi
 Allowable Shear 272.0 psi

Load Combination Results

Load Combination	C _D	C _P	Maximum Axial + Bending Stress Ratios			Maximum Shear Ratios		
			Stress Ratio	Status	Location	Stress Ratio	Status	Location
D Only	0.900	0.325	0.1160	PASS	0.0 ft	0.0	PASS	20.670 ft
+D+S	1.150	0.261	0.7036	PASS	0.0 ft	0.0	PASS	20.670 ft
+D+0.750S	1.150	0.261	0.5560	PASS	0.0 ft	0.0	PASS	20.670 ft
+D+0.60W	1.600	0.192	0.6745	PASS	19.005 ft	0.2011	PASS	20.670 ft
+D+0.450W	1.600	0.192	0.5089	PASS	19.005 ft	0.1508	PASS	20.670 ft
+D+0.750S+0.450W	1.600	0.192	0.7926	PASS	19.005 ft	0.1508	PASS	20.670 ft
+0.60D+0.60W	1.600	0.192	0.6666	PASS	19.005 ft	0.2011	PASS	20.670 ft
+0.60D	1.600	0.192	0.06649	PASS	0.0 ft	0.0	PASS	20.670 ft

Wood Column

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DESCRIPTION: LIVING MIDDLE KING STUD

Maximum Reactions

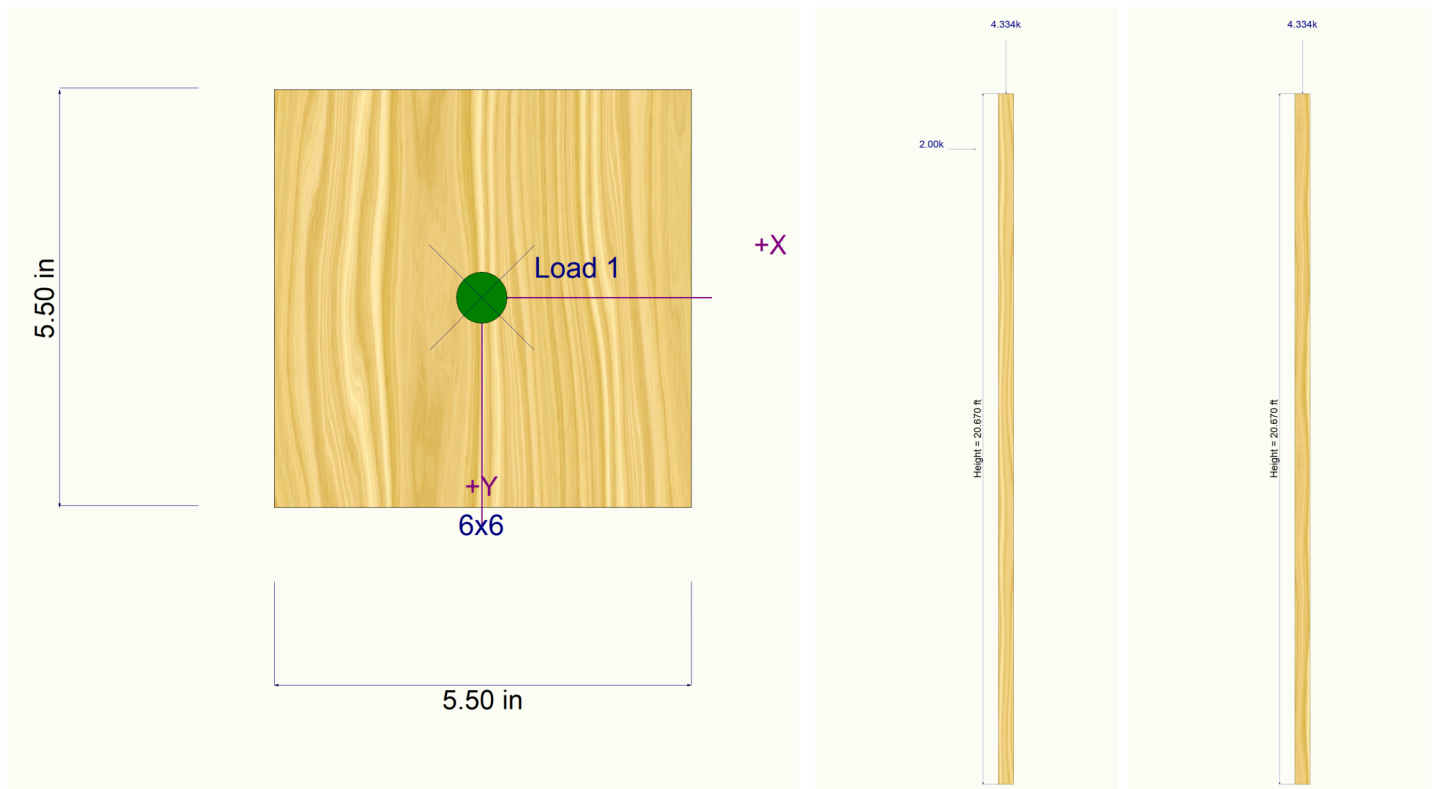
Note: Only non-zero reactions are listed.

Load Combination	X-X Axis Reaction		k	Y-Y Axis Reaction		Axial Reaction	My - End Moments		Mx - End Moments	
	@ Base	@ Top		@ Base	@ Top		@ Base	@ Top	@ Base	@ Top
D Only						0.720				
+D+S						4.470				
+D+0.750S						3.532				
+D+0.60W				0.097	1.103	0.720				
+D+0.450W				0.073	0.827	0.720				
+D+0.750S+0.450W				0.073	0.827	3.532				
+0.60D+0.60W				0.097	1.103	0.432				
+0.60D						0.432				
S Only						3.750				
W Only				0.162	1.838					

Maximum Deflections for Load Combinations

Load Combination	Max. X-X Deflection	Distance	Max. Y-Y Deflection	Distance
D Only	0.000 in	0.000ft	0.000 in	0.000 ft
+D+S	0.000 in	0.000ft	0.000 in	0.000 ft
+D+0.750S	0.000 in	0.000ft	0.000 in	0.000 ft
+D+0.60W	0.000 in	0.000ft	0.956 in	11.930 ft
+D+0.450W	0.000 in	0.000ft	0.717 in	11.930 ft
+D+0.750S+0.450W	0.000 in	0.000ft	0.717 in	11.930 ft
+0.60D+0.60W	0.000 in	0.000ft	0.956 in	11.930 ft
+0.60D	0.000 in	0.000ft	0.000 in	0.000 ft
S Only	0.000 in	0.000ft	0.000 in	0.000 ft
W Only	0.000 in	0.000ft	1.594 in	11.930 ft

Sketches



RES (9) Individual Footing Design

Program: Continuous Footing

Soil Bearing Pressure: 1500psf

Roof			
Roof Dead	(17psf)	(20.5ft)	= 349plf
Snow Live	(150psf)	(20.5ft)	= 3075plf

Upper Floor			
Floor Dead	(12psf)	(.0ft)	= plf
Floor Live	(40psf)	(.0ft)	= plf

Main Floor			
Floor Dead	(12psf)	(4.0ft)	= 48plf
Floor Live	(40psf)	(4.0ft)	= 160plf

Deck Cover			
Roof Dead	(17psf)	(.0ft)	= plf
Snow Live	(150psf)	(.0ft)	= plf

Deck Floor			
Floor Dead	(12psf)	(3.0ft)	= 36plf
Snow Live	(75psf)	(3.0ft)	= 225plf

Misc			
Wall Load:	(12psf)	(12.0ft)	= 144plf
Conc Stem:	(145pcf)	(2 x .7ft)	= 194plf
Misc Load:	(.0ft)	(.0ft) (.0ft)	= plf

4071plf

Use Footing Width:	42	x	10	in
W/		(4)	#4	Cont.

RES (7) Individual Footing Design

Program: Continuous Footing

Soil Bearing Pressure: 1500psf

Roof				
Roof Dead	(17psf)	(16.0ft)	=	272plf
Snow Live	(150psf)	(16.0ft)	=	2400plf

Upper Floor				
Floor Dead	(12psf)	(7.5ft)	=	90plf
Floor Live	(40psf)	(7.5ft)	=	300plf

Main Floor				
Floor Dead	(12psf)	(.0ft)	=	plf
Floor Live	(40psf)	(.0ft)	=	plf

Deck Cover				
Roof Dead	(17psf)	(.0ft)	=	plf
Snow Live	(150psf)	(.0ft)	=	plf

Deck Floor				
Floor Dead	(12psf)	(.0ft)	=	plf
Snow Live	(150psf)	(.0ft)	=	plf

Misc				
Wall Load:	(12psf)	(12.0ft)	=	144plf
Conc Stem:	(145pcf)	(2 x .7ft)	=	194plf
Misc Load:	(.0ft)	(.0ft)	(.0ft)	= plf

3100plf

Use Footing Width:	30	x	10	in
W/		(3)	#4	Cont.

RES (6) Individual Footing Design

Program: Continuous Footing

Soil Bearing Pressure: 1500psf

Roof				
Roof Dead	(17psf)	(22.0ft)	=	374plf
Snow Live	(150psf)	(22.0ft)	=	3300plf

Upper Floor				
Floor Dead	(12psf)	(7.5ft)	=	90plf
Floor Live	(40psf)	(7.5ft)	=	300plf

Main Floor				
Floor Dead	(12psf)	(.0ft)	=	plf
Floor Live	(40psf)	(.0ft)	=	plf

Deck Cover				
Roof Dead	(17psf)	(.0ft)	=	plf
Snow Live	(150psf)	(.0ft)	=	plf

Deck Floor				
Floor Dead	(12psf)	(.0ft)	=	plf
Snow Live	(150psf)	(.0ft)	=	plf

Misc				
Wall Load:	(12psf)	(12.0ft)	=	144plf
Conc Stem:	(145pcf)	(2 x .7ft)	=	194plf
Misc Load:	(.0ft)	(.0ft)	=	plf

4102plf

Use Footing Width:	42	x	10	in
W/		(4)	#4	Cont.

RES (5) Individual Footing Design

Program: Continuous Footing

Soil Bearing Pressure: 1500psf

Roof				
Roof Dead	(17psf)	(19.0ft)	=	323plf
Snow Live	(150psf)	(19.0ft)	=	2850plf

Upper Floor				
Floor Dead	(12psf)	(7.5ft)	=	90plf
Floor Live	(40psf)	(7.5ft)	=	300plf

Main Floor				
Floor Dead	(12psf)	(.0ft)	=	plf
Floor Live	(40psf)	(.0ft)	=	plf

Deck Cover				
Roof Dead	(17psf)	(.0ft)	=	plf
Snow Live	(150psf)	(.0ft)	=	plf

Deck Floor				
Floor Dead	(12psf)	(.0ft)	=	plf
Snow Live	(150psf)	(.0ft)	=	plf

Misc				
Wall Load:	(12psf)	(12.0ft)	=	144plf
Conc Stem:	(145pcf)	(2 x .7ft)	=	194plf
Misc Load:	(.0ft)	(.0ft)	=	plf

3601plf

Use Footing Width:	36	x	10	in
W/		(3)	#4	Cont.

RES (4) Individual Footing Design

Program: Continuous Footing

Soil Bearing Pressure: 1500psf

Roof				
Roof Dead	(17psf)	(10.0ft)	=	170plf
Snow Live	(150psf)	(10.0ft)	=	1500plf

Upper Floor				
Floor Dead	(12psf)	(.0ft)	=	plf
Floor Live	(40psf)	(.0ft)	=	plf

Main Floor				
Floor Dead	(12psf)	(1.0ft)	=	12plf
Floor Live	(40psf)	(1.0ft)	=	40plf

Deck Cover				
Roof Dead	(17psf)	(.0ft)	=	plf
Snow Live	(150psf)	(.0ft)	=	plf

Deck Floor				
Floor Dead	(12psf)	(.0ft)	=	plf
Snow Live	(150psf)	(.0ft)	=	plf

Misc				
Wall Load:	(12psf)	(12.0ft)	=	144plf
Conc Stem:	(145pcf)	(2 x .7ft)	=	194plf
Misc Load:	(.0ft)	(.0ft)	(.0ft)	= plf

2020plf

Use Footing Width:	18	x	8	in
W/		(2)	#4	Cont.

RES (3) Individual Footing Design

Program: Continuous Footing

Soil Bearing Pressure: 1500psf

Roof				
Roof Dead	(17psf)	(7.0ft)	=	119plf
Snow Live	(150psf)	(7.0ft)	=	1050plf

Upper Floor				
Floor Dead	(12psf)	(1.0ft)	=	12plf
Floor Live	(40psf)	(1.0ft)	=	40plf

Main Floor				
Floor Dead	(12psf)	(1.0ft)	=	12plf
Floor Live	(40psf)	(1.0ft)	=	40plf

Deck Cover				
Roof Dead	(17psf)	(.0ft)	=	plf
Snow Live	(150psf)	(.0ft)	=	plf

Deck Floor				
Floor Dead	(12psf)	(.0ft)	=	plf
Snow Live	(150psf)	(.0ft)	=	plf

Misc				
Wall Load:	(12psf)	(12.0ft)	=	144plf
Conc Stem:	(145pcf)	(2 x .7ft)	=	194plf
Misc Load:	(.0ft)	(.0ft)	(.0ft)	= plf

1531plf

Use Footing Width:	16	x	8	in
W/		(2)	#4	Cont.

RES (2) Individual Footing Design

Program: Continuous Footing

Soil Bearing Pressure: 1500psf

Roof				
Roof Dead	(17psf)	(.0ft)	=	plf
Snow Live	(150psf)	(.0ft)	=	plf

Upper Floor				
Floor Dead	(12psf)	(.0ft)	=	plf
Floor Live	(40psf)	(.0ft)	=	plf

Main Floor				
Floor Dead	(12psf)	(9.3ft)	=	112plf
Floor Live	(40psf)	(9.3ft)	=	373plf

Deck Cover				
Roof Dead	(17psf)	(.0ft)	=	plf
Snow Live	(150psf)	(.0ft)	=	plf

Deck Floor				
Floor Dead	(12psf)	(.0ft)	=	plf
Snow Live	(150psf)	(.0ft)	=	plf

Misc				
Wall Load:	(12psf)	(12.0ft)	=	144plf
Conc Stem:	(145pcf)	(2 x .7ft)	=	194plf
Misc Load:	(.0ft)	(.0ft)	(.0ft)	= plf

823plf

Use Footing Width:	12	x	8	in
W/		(2)	#4	Cont.

RES Individual Footing Design

Program: Continuous Footing

Soil Bearing Pressure: 1500psf

Roof				
Roof Dead	(17psf)	(2.5ft)	=	43plf
Snow Live	(150psf)	(2.5ft)	=	375plf

Upper Floor				
Floor Dead	(12psf)	(1.0ft)	=	12plf
Floor Live	(40psf)	(1.0ft)	=	40plf

Main Floor				
Floor Dead	(12psf)	(1.0ft)	=	12plf
Floor Live	(40psf)	(1.0ft)	=	40plf

Deck Cover				
Roof Dead	(17psf)	(.0ft)	=	plf
Snow Live	(150psf)	(.0ft)	=	plf

Deck Floor				
Floor Dead	(12psf)	(.0ft)	=	plf
Snow Live	(150psf)	(.0ft)	=	plf

Misc				
Wall Load:	(12psf)	(12.0ft)	=	144plf
Conc Stem:	(145pcf)	(2 x .7ft)	=	194plf
Misc Load:	(.0ft)	(.0ft)	(.0ft)	= plf

780plf

Use Footing Width:	12	x	8	in
W/		(2)	#4	Cont.

SHOP (3) Individual Footing Design

Program: Continuous Footing

Soil Bearing Pressure: 1500psf

<i>Roof</i>			
Roof Dead	(17psf)	(18.8ft)	= 319plf
Snow Live	(150psf)	(18.8ft)	= 2813plf

<i>Misc</i>			
Wall Load:	(12psf)	(16.4ft)	= 197plf
Conc Stem:	(145pcf)	(2 x .7ft)	= 194plf
Misc Load:	(.0ft)	(.0ft)	(.0ft) = plf

3522plf

Use Footing Width:	36	x	10	in
W/	(3)		#4	Cont.

SHOP (2) Individual Footing Design

Program: Continuous Footing

Soil Bearing Pressure: 1500psf

<i>Roof</i>				
Roof Dead	(17psf)	(12.5ft)	=	213plf
Snow Live	(150psf)	(12.5ft)	=	1875plf

<i>Misc</i>				
Wall Load:	(12psf)	(16.4ft)	=	197plf
Conc Stem:	(145pcf)	(2 x .7ft)	=	194plf
Misc Load:	(.0ft)	(.0ft)	(.0ft)	= plf

2479plf

Use Footing Width:	24	x	8	in
W/	(2)	#4	Cont.	

SHOP Individual Footing Design

Program: Continuous Footing

Soil Bearing Pressure: 1500psf

<i>Roof</i>			
Roof Dead	(17psf)	(3.5ft)	= 60plf
Snow Live	(150psf)	(3.5ft)	= 525plf

<i>Misc</i>			
Wall Load:	(12psf)	(16.4ft)	= 197plf
Conc Stem:	(145pcf)	(2 x .7ft)	= 194plf
Misc Load:	(.0ft)	(.0ft)	(.0ft) = plf

976plf

Use Footing Width:	12	x	8	in
W/	(2)		#4	Cont.

PAD FOOTING DESIGN CAPACITIES:

Soil Bearing (1500 psf)							
Dimensions (Inches)			Capacity	# of Bars	Min. Col. Size		
72	x	72	x	12	47,500 lbs	10	3.5 sq.
66	x	66	x	12	39,750 lbs	8	3.5 sq.
60	x	60	x	10	33,450 lbs	6	3.5 sq.
54	x	54	x	10	27,000 lbs	5	3.5 sq.
48	x	48	x	8	21,500 lbs	4	3.5 sq.
42	x	42	x	8	16,500 lbs	4	3.5 sq.
36	x	36	x	8	12,000 lbs	4	3.5 sq.
30	x	30	x	8	8,350 lbs	3	3.5 sq.
24	x	24	x	8	5,300 lbs	2	3.5 sq.
18	x	18	x	8	2,900 lbs	2	3.5 sq.

Bars to be 3 1/2" from bottom of pad. Evenly space in both directions.

CONT. FOOTING DESIGN CAPACITIES:

Soil Bearing (1500 psf)				
Dimensions (Inches)			Capacity	# of Bars
60	x	10	6,850 plf	6
54	x	10	6,200 plf	5
48	x	10	5,500 plf	4
42	x	10	4,750 plf	4
36	x	10	4,000 plf	3
30	x	10	3,400 plf	3
24	x	8	2,800 plf	2
18	x	8	2,100 plf	2
16	x	8	1,850 plf	2
12	x	8	1,350 plf	2

Bars to be 3 1/2" from bottom of footing.